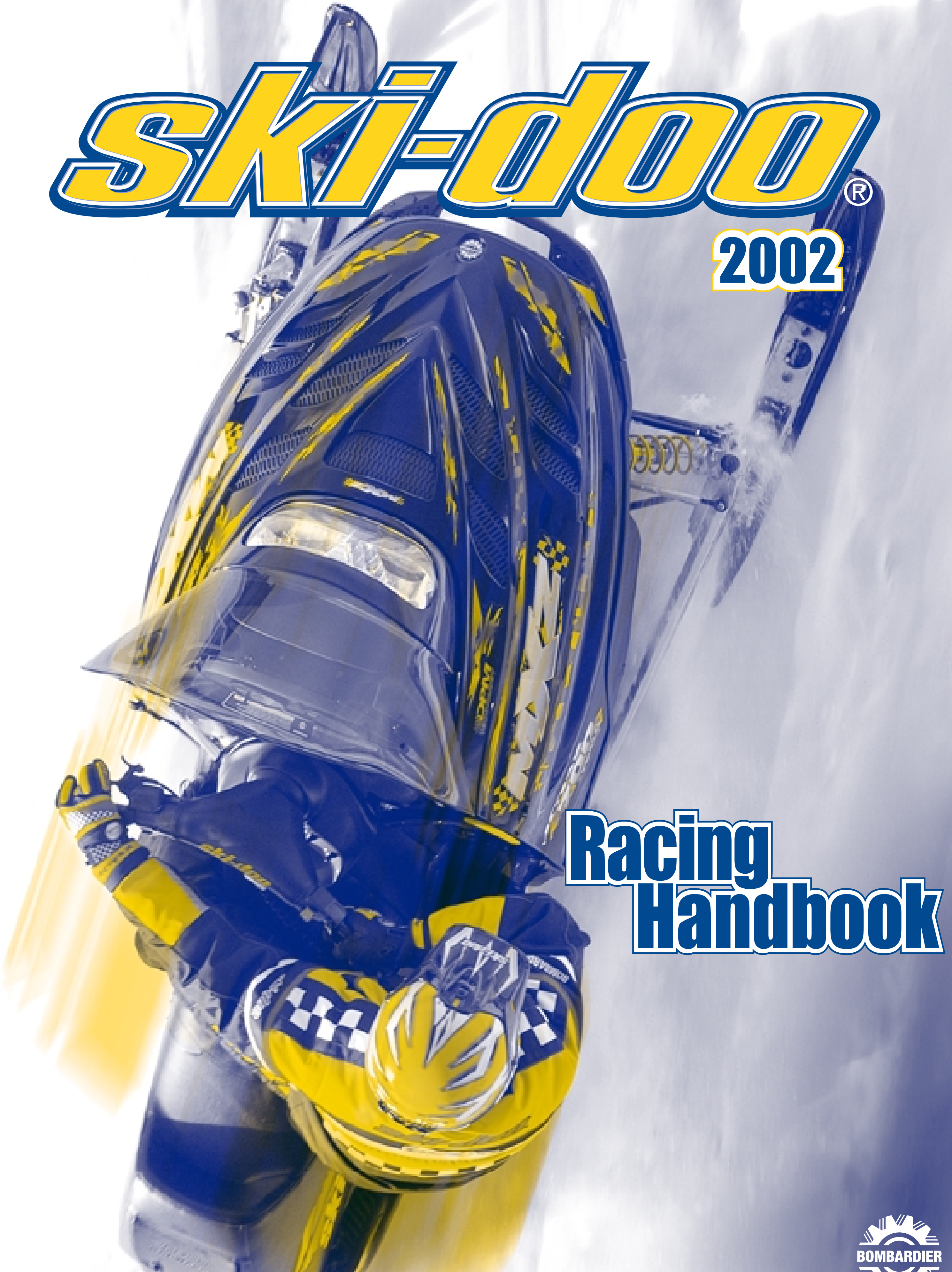

ski-doo® 2002

Racing Handbook

484 200 038

2002 RACER HANDBOOK

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⚠ WARNING

This information relates to the preparation and use of snowmobiles in competitive events. Bombardier Inc. disclaims liability for all damages and/or injuries resulting from the improper use of the contents. We strongly recommend that these modifications be carried out and/or verified by a highly-skilled professional racing mechanic. It is understood that racing or modifications of any Bombardier-made snowmobile voids the vehicle warranty and that such modifications may render use of the vehicle illegal in other than sanctioned racing events under existing federal, provincial and state regulations.

KEEPING YOUR MACHINE LEGAL IS YOUR RESPONSIBILITY

Read and know your rule books.

GENERAL

If you have any suggestions on new information and ideas to improve next year's handbook, including any errors or omissions, please mail or fax to;

Ski-Doo Race Department
Bombardier Motor Corp of America
7575 Bombardier Court
Wausau, Wisconsin
54401.

For additional information or to pass on your feedback and suggestions please contact the following people using the racer report format.

Your information is important to us.

Technical assistance for snocross, grass drag, oval, cross country hillclimb and asphalt racing

Contact Tom Lawrence:	Phone	715-848-4971
	Fax	715-847-6879
	E-mail	tom.lawrence@recreation.bombardier.com

To order parts through Valcourt race department, use *Parts order form.*

Fax: 450-532-5076

A wide range of excellent publications and special tools are available to support your racing activities.

See Section 06-1, Competition bulletins-racing parts, useful publications.

Parts numbers with a 486 prefix must be ordered from the Valcourt Race Dept. All others must be ordered from your local Ski-Doo dealer.

Race program, sponsorship, contingency programs

Contact Steve Cowing:	Phone	651-452-3340
	Fax	651-452-3341
	E-mail	steve.cowing@recreation.bombardier.com

PARTS ORDER

SKI-DOO RACING DEPT.

	DATE:	PAGE of
ORDER DESK: *PARTS & CLOTHING*	**Robert Bourgeois** Racing Parts Coordinator	**Fax # (450) 532-5076**

FROM:	***if you are a dealer:***
	DEALER #:
	FED. ID #: (US dealers only)
PHONE #:	**FAX #:**
FROM:	***if you are a racer:***
	SOCIAL SECURITY #:
	(we need your SS # for custom regulations)
PHONE #:	**FAX #:**

PAYMENT: VISA ___ MASTER CARD ___ # ________________________ Exp. Date ________

SHIPPING CONDITIONS: RED ______ GROUND ______ BLUE ______

(*Shipping fees will be charged to you)*

DESCRIPTION	PART # OR CLOTHING PART #	QUANTITY

Part numbers with a 486 prefix must be ordered from the Valcourt Race Dept. All others must be ordered from your local Ski-Doo dealer.

PHONE ORDERS WILL NOT BE ACCEPTED

T.I.P. SHEET APPLICATION

TECHNICAL INFORMATION POSTING

Dear Ski-Doo X-Team

Please add my name to your list of recipients for the T.I.P. sheets to be distributed during the 2001-02 race season.

Name:

Address:

City: St./Prov: Zip/Code:

Phone: Day: Evening:

Please send my T.I.P. sheets to the following:

Please print !

Priority (please circle one)

Fax: 1 2

Email: 1 2

Personal Information:

Race Circuits you compete in:

Number of years racing:

Type and class you currently race:

Model and year of race sled:

Please return this completed form by Fax to (715) 847-6869

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SECTION 02 - 2002 MODELS TECHNICAL DATA

VEHICLES

ENGINES

VEHICLE MODEL			MX Zx 440 RACING (CAN./U.S.)	MX Z 500 SPORT (CAN./U.S.)	MX Z 500 R SPORT (CAN./U.S.)
ENGINE TYPE			**453**	**493**	**493**
Number of Cylinders			2	2	2
Bore		mm (in)	65.00 (2.559)	69.50 (2.736)	69.50 (2.736)
Stroke		mm (in)	65.80 (2.591)	65.80 (2.591)	65.80 (2.591)
Displacement		cm^3 (in^3)	436.69 (26.65)	499.30 (30.47)	499.30 (30.47)
Compression Ratio (corrected)		± 0.5	14.8 ± 0.25	12.0	12.0
Maximum Power Engine Speed ①		± 100 RPM	8400	8000	8000
Piston Ring Type		1st/2nd	ST/N.A.	ST/N.A.	ST/N.A.
Ring End Gap	New	mm (in)	0.2 (.008)	0.4 (.016)	0.4 (.016)
	Wear Limit	mm (in)	1.0 (.039)	1.0 (.039)	1.0 (.039)
Ring/Piston Groove Clearance	New	mm (in)	0.04 (.0016)	0.04 (.0016)	0.04 (.0016)
	Wear Limit	mm (in)	0.2 (.0079)	0.2 (.0079)	0.2 (.0079)
Piston/Cylinder Wall Clearance	New	mm (in)	0.113 ± 0.013 (.0044 ± .0005)	0.100 ± 0.016 (.0039 ± .0006)	0.100 ± 0.016 (.0039 ± .0006)
	Wear Limit	mm (in)	0.18 (.0071)	0.20 (.0079)	0.20 (.0079)
Connecting Rod Big End Axial Play	New	mm (in)	0.39 (.0154)	0.39 (.0154)	0.39 (.0154)
	Wear Limit	mm (in)	1.2 (.0472)	1.2 (.0472)	1.2 (.0472)
Maximum Crankshaft End-play ②		mm (in)	0.3 (.012)	0.3 (.012)	0.3 (.012)
Maximum Crankshaft Deflection at PTO		mm (in)	0.06 (.0024)	0.06 (.0024)	0.06 (.0024)
Magneto Generator Output		W	290	290	290
Ignition Type			CDI	CDI	CDI
Spark Plug Make and Type			NGK BR9ES	NGK BR9ECS	NGK BR9ECS
Spark Plug Gap		± 0.05 mm (± .002 in)	0.45 (.018)	0.45 (.018)	0.45 (.018)
Ignition Timing BTDC ③		mm (in)	3.14 (.124)	3.00 (.118)	3.00 (.118)
Trigger Coil ④		Ω	190 – 300	190 – 300	190 – 300
Generating Coil ④	Low Speed	Ω	17.5 – 42.5	17.5 – 42.5	17.5 – 42.5
	High Speed	Ω	2.4 – 5.8	2.4 – 5.8	2.4 – 5.8
Lighting Coil ④		Ω	0.1 – 0.4	0.1 – 0.4	0.1 – 0.4
High Tension Coil ④	Primary	Ω	0.3 – 0.7	0.3 – 0.7	0.3 – 0.7
	Secondary	kΩ	8.0 – 16.0	8.0 – 16.0	8.0 – 16.0
Carburetor Type		PTO/MAG	TMX 34-18	TM 40-B151	TM 40-B151
Main Jet		PTO/MAG	260/260	500/500	500/500
Needle Jet			P-0 ⑤	P-0 ⑤	P-0 ⑤
Pilot Jet			25	17.5	17.5
Needle Identification — Clip Position			6FNY04/51 — 3	9HGY1/58 ⑥	9HGY1/58 ⑥
Slide Cut-Away			4.0	2.0	2.0
Float Adjustment		± 1 mm (± .040 in)	N.A.	N.A.	N.A.
Air or Pilot Screw Adjustment		± 1/16 Turn	N.A.	1	1
Idle Speed		± 200 RPM	1600	1600	1600
Gas Type/Pump Octane Number			Unleaded/87	Unleaded/87	Unleaded/87
Gas/Oil Ratio			33:1	Injection	Injection
Type			Liquid	Liquid	Liquid
Axial Fan Belt Adjustment	Deflection	mm (in)	N.A.	N.A.	N.A.
	Force	kg (lbf)	N.A.	N.A.	N.A.
Thermostat Opening Temperature		°C (°F)	42 (108)	42 (108)	42 (108)
Radiator Cap Opening Pressure		kPa (PSI)	90 (13)	90 (13)	90 (13)
ENGINE COLD N•m (lbf•ft)	Drive Pulley Retaining Screw		⑦	⑦	⑦
	Exhaust Manifold Nuts or Bolts		22 (16)	22 (16)	22 (16)
	Magneto Ring Nut		125 (92)	125 (92)	125 (92)
	Crankcase Nuts or Screws	M6	9 (7)	9 (7)	9 (7)
		M8	29 (21)	29 (21)	29 (21)
	Crankcase/Engine Support Nuts or Screws		35 (26)	35 (26)	35 (26)
	Cylinder Head Screws		29 (21)	29 (21)	29 (21)
	Crankcase/Cylinder Nuts or Screws		29 (21)	29 (21)	29 (21)
	Axial Fan Shaft Nut		N.A.	N.A.	N.A.

	VEHICLE MODEL			MX Z 500 TRAIL (CAN./U.S.)	MX Z 600 SPORT (CAN./U.S.)	MX Z 600 R SPORT (CAN./U.S.)
	ENGINE TYPE			**493**	**593**	**593**
	Number of Cylinders			2	2	2
	Bore		mm (in)	69.50 (2.736)	76.00 (2.992)	76.00 (2.992)
	Stroke		mm (in)	65.80 (2.591)	65.80 (2.591)	65.80 (2.591)
	Displacement		cm^3 (in^3)	499.30 (30.47)	597.00 (36.43)	597.00 (36.43)
	Compression Ratio (corrected)		± 0.5	12.0	12.0	12.0
	Maximum Power Engine Speed ①		± 100 RPM	8000	8000	8000
	Piston Ring Type		1st/2nd	ST/N.A.	ST/N.A.	ST/N.A.
	Ring End Gap	New Wear Limit	mm (in) mm (in)	0.4 (.016) 1.0 (.039)	0.4 (.016) 1.0 (.039)	0.4 (.016) 1.0 (.039)
	Ring/Piston Groove Clearance	New Wear Limit	mm (in) mm (in)	0.04 (.0016) 0.2 (.0079)	0.04 (.0016) 0.2 (.0079)	0.04 (.0016) 0.2 (.0079)
	Piston/Cylinder Wall Clearance	New Wear Limit	mm (in) mm (in)	0.100 ± 0.016 (.0039 ± .0006) 0.20 (.0079)	0.120 ± 0.016 (.0047 ± .0006) 0.20 (.0079)	0.120 ± 0.016 (.0047 ± .0006) 0.20 (.0079)
	Connecting Rod Big End Axial Play	New Wear Limit	mm (in) mm (in)	0.39 (.0154) 1.2 (.0472)	0.39 (.0154) 1.2 (.0472)	0.39 (.0154) 1.2 (.0472)
	Maximum Crankshaft End-play ②		mm (in)	0.3 (.012)	0.3 (.012)	0.3 (.012)
	Maximum Crankshaft Deflection at PTO		mm (in)	0.06 (.0024)	0.06 (.0024)	0.06 (.0024)
	Magneto Generator Output		W	290	290	290
	Ignition Type			CDI	CDI	CDI
	Spark Plug Make and Type			NGK BR9ECS	NGK BR9ECS	NGK BR9ECS
	Spark Plug Gap		± 0.05 mm (± .002 in)	0.45 (.018)	0.45 (.018)	0.45 (.018)
	Ignition Timing BTDC ③		mm (in)	3.00 (.118)	3.00 (.118)	3.00 (.118)
	Trigger Coil ④		Ω	190 – 300	190 – 300	190 – 300
	Generating Coil ④	Low Speed	Ω	17.5 – 42.5	17.5 – 42.5	17.5 – 42.5
		High Speed	Ω	2.4 – 5.8	2.4 – 5.8	2.4 – 5.8
	Lighting Coil ④		Ω	0.1 – 0.4	0.1 – 0.4	0.1 – 0.4
	High Tension Coil ④	Primary	Ω	0.3 – 0.7	0.3 – 0.7	0.3 – 0.7
		Secondary	kΩ	8.0 – 16.0	8.0 – 16.0	8.0 – 16.0
	Carburetor Type		PTO/MAG	TM 40-B151	TM 40-B154	TM 40-B154
	Main Jet		PTO/MAG	500/500	500/500	500/500
	Needle Jet			P-0 ⑤	P-0 ⑤	P-0 ⑤
	Pilot Jet			17.5	20	20
	Needle Identification — Clip Position			9HGY1/58 ⑥	9HGY1/58 ⑥	9HGY1/58 ⑥
	Slide Cut-Away			2.0	2.0	2.0
	Float Adjustment		± 1 mm (± .040 in)	N.A.	N.A.	N.A.
	Air or Pilot Screw Adjustment		± 1/16 Turn	1.0	1-1/2	1-1/2
	Idle Speed		± 200 RPM	1600	1600	1600
	Gas Type/Pump Octane Number			Unleaded/87	Unleaded/87	Unleaded/87
	Gas/Oil Ratio			Injection	Injection	Injection
	Type			Liquid	Liquid	Liquid
	Axial Fan Belt Adjustment	Deflection	mm (in)	N.A.	N.A.	N.A.
		Force	kg (lbf)	N.A.	N.A.	N.A.
	Thermostat Opening Temperature		°C (°F)	42 (108)	42 (108)	42 (108)
	Radiator Cap Opening Pressure		kPa (PSI)	90 (13)	90 (13)	90 (13)
ENGINE COLD N•m (lbf•ft)	Drive Pulley Retaining Screw			⑦	⑦	⑦
	Exhaust Manifold Nuts or Bolts			22 (16)	22 (16)	22 (16)
	Magneto Ring Nut			125 (92)	125 (92)	125 (92)
	Crankcase Nuts or Screws		M6 M8	9 (7) 29 (21)	9 (7) 29 (21)	9 (7) 29 (21)
	Crankcase/Engine Support Nuts or Screws			35 (26)	35 (26)	35 (26)
	Cylinder Head Screws			29 (21)	29 (21)	29 (21)
	Crankcase/Cylinder Nuts or Screws			29 (21)	29 (21)	29 (21)
	Axial Fan Shaft Nut			N.A.	N.A.	N.A.

	VEHICLE MODEL			MX Z 600 TRAIL (CAN./U.S.)	MX Z 600 R ADRENALINE (CAN./U.S.)	MX Z 600 R RENEGADE (CAN./U.S.)
	ENGINE TYPE			**593**	**593**	**593**
	Number of Cylinders			2	2	2
	Bore		mm (in)	76.00 (2.992)	76.00 (2.992)	76.00 (2.992)
	Stroke		mm (in)	65.80 (2.591)	65.8 (2.591)	65.8 (2.591)
	Displacement		cm^3 (in^3)	597.00 (36.43)	597.00 (36.43)	597.00 (36.43)
	Compression Ratio (corrected)		± 0.5	12.0	12.0	12.0
	Maximum Power Engine Speed ①		± 100 RPM	8000	8000	8000
	Piston Ring Type		$1^{st}/2^{nd}$	ST/N.A.	ST/N.A.	ST/N.A.
	Ring End Gap	New Wear Limit	mm (in) mm (in)	0.4 (.016) 1.0 (.039)	0.4 (.016) 1.0 (.039)	0.4 (.016) 1.0 (.039)
	Ring/Piston Groove Clearance	New Wear Limit	mm (in) mm (in)	0.04 (.0016) 0.2 (.0079)	0.040 (.0016) 0.2 (.0079)	0.40 (.0157) 0.2 (.0079)
	Piston/Cylinder Wall Clearance	New Wear Limit	mm (in) mm (in)	0.120 ± 0.016 (.0047 ± .0006) 0.20 (.0079)	0.120 ± 0.016 (.0047 ± .0006) 0.20 (.0079)	0.120 ± 0.016 (.0047 ± .0006) 0.20 (.0079)
	Connecting Rod Big End Axial Play	New Wear Limit	mm (in) mm (in)	0.39 (.0154) 1.2 (.0472)	0.39 (.0154) 1.2 (.0472)	0.39 (.0154) 1.2 (.0472)
	Maximum Crankshaft End-play ②		mm (in)	0.3 (.012)	0.3 (.012)	0.3 (.012)
	Maximum Crankshaft Deflection at PTO		mm (in)	0.06 (.0024)	0.06 (.0024)	0.06 (.0024)
	Magneto Generator Output		W	290	290	290
	Ignition Type			CDI	CDI	CDI
	Spark Plug Make and Type			NGK BR9ECS	NGK BR9ECS	NGK BR9ECS
	Spark Plug Gap		± 0.05 mm (± .002 in)	0.45 (.018)	0.45 (.018)	0.45 (.018)
	Ignition Timing BTDC ③		mm (in)	3.00 (.118)	3.00 (.118)	3.00 (.118)
	Trigger Coil ④		Ω	190 – 300	190 – 300	190 – 300
	Generating Coil ④	Low Speed	Ω	17.5 – 42.5	17.5 – 42.5	17.5 – 42.5
		High Speed	Ω	2.4 – 5.8	2.4 – 5.8	2.4 – 5.8
	Lighting Coil ④		Ω	0.1 – 0.4	0.1 – 0.4	0.1 – 0.4
	High Tension Coil ④	Primary	Ω	0.3 – 0.7	0.3 – 0.7	0.3 – 0.7
		Secondary	kΩ	8.0 – 16.0	8.0 – 16.0	8.0 – 16.0
	Carburetor Type		PTO/MAG	TM 40-B154	TM 40-B154	TM 40-B154
	Main Jet		PTO/MAG	500/500	500/500	500/500
	Needle Jet			P-0 ⑤	P-0 ⑤	P-0 ⑤
	Pilot Jet			20	20	20
	Needle Identification — Clip Position			9HGY1/58 ⑥	9HGY1/58 ⑥	9ZLY3/58 ⑥
	Slide Cut-Away			2.0	2.0	2.0
	Float Adjustment		± 1 mm (± .040 in)	N.A.	N.A.	N.A.
	Air or Pilot Screw Adjustment		± 1/16 Turn	1.5	1-1/2	1-1/2
	Idle Speed		± 200 RPM	1600	1600	1600
	Gas Type/Pump Octane Number			Unleaded/87	Unleaded/87	Unleaded/87
	Gas/Oil Ratio			Injection	Injection	Injection
	Type			Liquid	Liquid	Liquid
	Axial Fan Belt Adjustment	Deflection	mm (in)	N.A.	N.A.	N.A.
		Force	kg (lbf)	N.A.	N.A.	N.A.
	Thermostat Opening Temperature		°C (°F)	42 (108)	42 (108)	42 (108)
	Radiator Cap Opening Pressure		kPa (PSI)	90 (13)	90 (13)	90 (13)
ENGINE COLD N•m (lbf•ft)	Drive Pulley Retaining Screw			⑦	⑦	⑦
	Exhaust Manifold Nuts or Bolts			22 (16)	22 (16)	22 (16)
	Magneto Ring Nut			125 (92)	125 (92)	125 (92)
	Crankcase Nuts or Screws		M6 M8	9 (7) 29 (21)	9 (7) 29 (21)	9 (7) 29 (21)
	Crankcase/Engine Support Nuts or Screws			35 (26)	35 (26)	35 (26)
	Cylinder Head Screws			29 (21)	29 (21)	29 (21)
	Crankcase/Cylinder Nuts or Screws			29 (21)	29 (21)	29 (21)
	Axial Fan Shaft Nut			N.A.	N.A.	N.A.

VEHICLE MODEL			MX Z 600 X (CAN./U.S.)	MX Z 600 R X (CAN./U.S.)	MX Z 700 SPORT (CAN./U.S.)
ENGINE TYPE			**593**	**593**	**693**
Number of Cylinders			2	2	2
Bore		mm (in)	76.00 (2.992)	76.00 (2.992)	78.00 (3.071)
Stroke		mm (in)	65.80 (2.591)	65.80 (2.591)	73.00 (2.874)
Displacement		cm^3 (in^3)	597.00 (36.43)	597.00 (36.43)	697.70 (42.58)
Compression Ratio (corrected)		± 0.5	12.0	12.0	12.0
Maximum Power Engine Speed ①		± 100 RPM	8000	8000	8000
Piston Ring Type		1st/2nd	ST/N.A.	ST/N.A.	ST/N.A.
Ring End Gap	New	mm (in)	0.4 (.016)	0.4 (.016)	0.4 (.016)
	Wear Limit	mm (in)	1.0 (.039)	1.0 (.039)	1.0 (.039)
Ring/Piston Groove Clearance	New	mm (in)	0.04 (.0016)	0.04 (.0016)	0.04 (.0016)
	Wear Limit	mm (in)	0.2 (.0079)	0.2 (.0079)	0.2 (.0079)
Piston/Cylinder Wall Clearance	New	mm (in)	0.120 ± 0.016 (.0047 ± .0006)	0.120 ± 0.016 (.0047 ± .0006)	0.115 ± 0.013 (.0045 ± .0005)
	Wear Limit	mm (in)	0.20 (.0079)	0.20 (.0079)	0.20 (.0079)
Connecting Rod Big End Axial Play	New	mm (in)	0.39 (.0154)	0.39 (.0154)	0.39 (.0154)
	Wear Limit	mm (in)	1.2 (.0472)	1.2 (.0472)	1.2 (.0472)
Maximum Crankshaft End-play ②		mm (in)	0.3 (.012)	0.3 (.012)	0.3 (.012)
Maximum Crankshaft Deflection at PTO		mm (in)	0.06 (.0024)	0.06 (.0024)	0.06 (.0024)
Magneto Generator Output		W	290	290	290
Ignition Type			CDI	CDI	CDI
Spark Plug Make and Type			NGK BR9ECS	NGK BR9ECS	NGK BR9ECS
Spark Plug Gap		± 0.05 mm (± .002 in)	0.45 (.018)	0.45 (.018)	0.45 (.018)
Ignition Timing BTDC ③		mm (in)	3.00 (.118)	3.00 (.118)	3.36 (.132)
Trigger Coil ④		Ω	190 – 300	190 – 300	190 – 300
Generating Coil ④	Low Speed	Ω	17.5 – 42.5	17.5 – 42.5	17.5 – 42.5
	High Speed	Ω	2.4 – 5.8	2.4 – 5.8	2.4 – 5.8
Lighting Coil ④		Ω	0.1 – 0.4	0.1 – 0.4	0.1 – 0.4
High Tension Coil ④	Primary	Ω	0.3 – 0.7	0.3 – 0.7	0.3 – 0.7
	Secondary	kΩ	8.0 – 16.0	8.0 – 16.0	8.0 – 16.0
Carburetor Type		PTO/MAG	TM 40-B154	TM 40-B154	TM 40-B160
Main Jet		PTO/MAG	500/500	500/500	510N/510N
Needle Jet			P-0 ⑤	P-0 ⑤	P-0 ⑤
Pilot Jet			20	20	17.5
Needle Identification — Clip Position			9HGY1/58 ⑥	9HGY1/58 ⑥	9ZLY3/58 ⑥
Slide Cut-Away			2.0	2.0	2.0
Float Adjustment		± 1 mm (± .040 in)	N.A.	N.A.	N.A.
Air or Pilot Screw Adjustment		± 1/16 Turn	1-1/2	1-1/2	1-1/2
Idle Speed		± 200 RPM	1600	1600	1500
Gas Type/Pump Octane Number			Unleaded/87	Unleaded/87	Unleaded/87
Gas/Oil Ratio			Injection	Injection	Injection
Type			Liquid	Liquid	Liquid
Axial Fan Belt Adjustment	Deflection	mm (in)	N.A.	N.A.	N.A.
	Force	kg (lbf)	N.A.	N.A.	N.A.
Thermostat Opening Temperature		°C (°F)	42 (108)	42 (108)	42 (108)
Radiator Cap Opening Pressure		kPa (PSI)	90 (13)	90 (13)	90 (13)
ENGINE COLD N•m (lbf•ft)	Drive Pulley Retaining Screw		⑦	⑦	⑦
	Exhaust Manifold Nuts or Bolts		22 (16)	22 (16)	22 (16)
	Magneto Ring Nut		125 (92)	125 (92)	125 (92)
	Crankcase Nuts or Screws	M6	9 (7)	9 (7)	9 (7)
		M8	29 (21)	29 (21)	29 (21)
	Crankcase/Engine Support Nuts or Screws		35 (26)	35 (26)	35 (26)
	Cylinder Head Screws		29 (21)	29 (21)	29 (21)
	Crankcase/Cylinder Nuts or Screws		29 (21)	29 (21)	40 (29)
	Axial Fan Shaft Nut		N.A.	N.A.	N.A.

VEHICLE MODEL			MX Z 700 R SPORT (CAN./U.S.)	MX Z 700 TRAIL (CAN./U.S.)	MX Z 700 R ADRENALINE (CAN./U.S.)
ENGINE TYPE			**693**	**693**	**693**
Number of Cylinders			2	2	2
Bore		mm (in)	78.00 (3.071)	78.00 (3.071)	78.00 (3.071)
Stroke		mm (in)	73.00 (2.874)	73.00 (2.874)	73.00 (2.874)
Displacement		cm^3 (in^3)	697.70 (42.58)	697.70 (42.58)	697.70 (42.58)
Compression Ratio (corrected)		± 0.5	12.0	12.0	12.0
Maximum Power Engine Speed ①		± 100 RPM	8000	8000	8000
Piston Ring Type		$1^{st}/2^{nd}$	ST/N.A.	ST/N.A.	ST/N.A.
Ring End Gap	New	mm (in)	0.4 (.016)	0.4 (.016)	0.4 (.016)
	Wear Limit	mm (in)	1.0 (.039)	1.0 (.039)	1.0 (.039)
Ring/Piston Groove Clearance	New	mm (in)	0.04 (.0016)	0.04 (.0016)	0.04 (.0016)
	Wear Limit	mm (in)	0.2 (.0079)	0.2 (.0079)	0.2 (.0079)
Piston/Cylinder Wall Clearance	New	mm (in)	0.118 ± 0.016 (.0046 ± .0006)	0.115 ± 0.013 (.0045 ± .0005)	0.115 ± 0.013 (.0045 ± .0005)
	Wear Limit	mm (in)	0.20 (.0079)	0.20 (.0079)	0.20 (.0079)
Connecting Rod Big End Axial Play	New	mm (in)	0.39 (.0154)	0.39 (.0154)	0.39 (.0154)
	Wear Limit	mm (in)	1.2 (.0472)	1.2 (.0472)	1.2 (.0472)
Maximum Crankshaft End-play ②		mm (in)	0.3 (.012)	0.3 (.012)	0.3 (.012)
Maximum Crankshaft Deflection at PTO		mm (in)	0.06 (.0024)	0.06 (.0024)	0.06 (.0024)
Magneto Generator Output		W	290	290	290
Ignition Type			CDI	CDI	CDI
Spark Plug Make and Type			NGK BR9ECS	NGK BR9ECS	NGK BR9ECS
Spark Plug Gap		± 0.05 mm (± .002 in)	0.45 (.018)	0.45 (.018)	0.45 (.018)
Ignition Timing BTDC ③		mm (in)	3.36 (.132)	3.36 (.132)	3.36 (.132)
Trigger Coil ④		Ω	190 – 300	190 – 300	190 – 300
Generating Coil ④	Low Speed	Ω	17.5 – 42.5	17.5 – 42.5	17.5 – 42.5
	High Speed	Ω	2.4 – 5.8	2.4 – 5.8	2.4 – 5.8
Lighting Coil ④		Ω	0.1 – 0.4	0.1 – 0.4	0.1 – 0.4
High Tension Coil ④	Primary	Ω	0.3 – 0.7	0.3 – 0.7	0.3 – 0.7
	Secondary	kΩ	8.0 – 16.0	8.0 – 16.0	8.0 – 16.0
Carburetor Type		PTO/MAG	TM 40-B160	TM 40-B160	TM 40-B160
Main Jet		PTO/MAG	510N/510N	510N/510N	510N/510N
Needle Jet			P-0 ⑤	P-0 ⑤	P-0 ⑤
Pilot Jet			17.5	17.5	17.5
Needle Identification — Clip Position			9ZLY3/58 ⑥	9ZLY3/58 ⑥	9ZLY3/58 ⑥
Slide Cut-Away			2.0	2.0	2.0
Float Adjustment		± 1 mm (± .040 in)	N.A.	N.A.	N.A.
Air or Pilot Screw Adjustment		± 1/16 Turn	1-1/2	1-1/2	1-1/2
Idle Speed		± 200 RPM	1500	1500	1500
Gas Type/Pump Octane Number			Unleaded/87	Unleaded/87	Unleaded/87
Gas/Oil Ratio			Injection	Injection	Injection
Type			Liquid	Liquid	Liquid
Axial Fan Belt Adjustment	Deflection	mm (in)	N.A.	N.A.	N.A.
	Force	kg (lbf)	N.A.	N.A.	N.A.
Thermostat Opening Temperature		°C (°F)	42 (108)	42 (108)	42 (108)
Radiator Cap Opening Pressure		kPa (PSI)	90 (13)	90 (13)	90 (13)
ENGINE COLD N•m (lbf•ft): Drive Pulley Retaining Screw			⑦	⑦	⑦
Exhaust Manifold Nuts or Bolts			22 (16)	22 (16)	22 (16)
Magneto Ring Nut			125 (92)	125 (92)	125 (92)
Crankcase Nuts or Screws		M6	9 (7)	9 (7)	9 (7)
		M8	29 (21)	29 (21)	29 (21)
Crankcase/Engine Support Nuts or Screws			35 (26)	35 (26)	35 (26)
Cylinder Head Screws			29 (21)	29 (21)	29 (21)
Crankcase/Cylinder Nuts or Screws			40 (29)	40 (29)	40 (29)
Axial Fan Shaft Nut			N.A.	N.A.	N.A.

VEHICLE MODEL			MX Z 700 R RENEGADE (CAN./U.S.)	MX Z 700 X (CAN./U.S.)	MX Z 700 R X (CAN./U.S.)
ENGINE TYPE			**693**	**693**	**693**
Number of Cylinders			2	2	2
Bore		mm (in)	78.00 (3.071)	78.00 (3.071)	78.00 (3.071)
Stroke		mm (in)	73.00 (2.874)	73.00 (2.874)	73.00 (2.874)
Displacement		cm³ (in³)	697.70 (42.58)	697.70 (42.58)	697.70 (42.58)
Compression Ratio (corrected)		± 0.5	12.0	12.0	12.0
Maximum Power Engine Speed ①		± 100 RPM	8000	8000	8000
Piston Ring Type		1st/2nd	ST/N.A.	ST/N.A.	ST/N.A.
Ring End Gap	New Wear Limit	mm (in) mm (in)	0.4 (.016) 1.0 (.039)	0.4 (.016) 1.0 (.039)	0.4 (.016) 1.0 (.039)
Ring/Piston Groove Clearance	New Wear Limit	mm (in) mm (in)	0.04 (.0016) 0.2 (.0079)	0.04 (.0016) 0.2 (.0079)	0.04 (.0016) 0.2 (.0079)
Piston/Cylinder Wall Clearance	New Wear Limit	mm (in) mm (in)	0.115 ± 0.013 (.0045 ± .0005) 0.20 (.0079)	0.115 ± 0.013 (.0045 ± .0005) 0.20 (.0079)	0.115 ± 0.013 (.0045 ± .0005) 0.20 (.0079)
Connecting Rod Big End Axial Play	New Wear Limit	mm (in) mm (in)	0.39 (.0154) 1.2 (.0472)	0.39 (.0154) 1.2 (.0472)	0.39 (.0154) 1.2 (.0472)
Maximum Crankshaft End-play ②		mm (in)	0.3 (.012)	0.3 (.012)	0.3 (.012)
Maximum Crankshaft Deflection at PTO		mm (in)	0.06 (.0024)	0.06 (.0024)	0.06 (.0024)
Magneto Generator Output		W	290	290	290
Ignition Type			CDI	CDI	CDI
Spark Plug Make and Type			NGK BR9ECS	NGK BR9ECS	NGK BR9ECS
Spark Plug Gap		± 0.05 mm (± .002 in)	0.45 (.018)	0.45 (.018)	0.45 (.018)
Ignition Timing BTDC ③		mm (in)	3.36 (.132)	3.36 (.132)	3.36 (.132)
Trigger Coil ④		Ω	190 – 300	190 – 300	190 – 300
Generating Coil ④	Low Speed	Ω	17.5 – 42.5	17.5 – 42.5	17.5 – 42.5
	High Speed	Ω	2.4 – 5.8	2.4 – 5.8	2.4 – 5.8
Lighting Coil ④		Ω	0.1 – 0.4	0.1 – 0.4	0.1 – 0.4
High Tension Coil ④	Primary	Ω	0.3 – 0.7	0.3 – 0.7	0.3 – 0.7
	Secondary	kΩ	8.0 – 16.0	8.0 – 16.0	8.0 – 16.0
Carburetor Type		PTO/MAG	TM 40-B160	TM 40-B160	TM 40-B160
Main Jet		PTO/MAG	510N/510N	510N/510N	510N/510N
Needle Jet			P-0 ⑤	P-0 ⑤	P-0 ⑤
Pilot Jet			17.5	17.5	17.5
Needle Identification — Clip Position			9ZLY3/58 ⑥	9ZLY3/58 ⑥	9ZLY3/58 ⑥
Slide Cut-Away			2.0	2.0	2.0
Float Adjustment		± 1 mm (± .040 in)	N.A.	N.A.	N.A.
Air or Pilot Screw Adjustment		± 1/16 Turn	1-1/2	1-1/2	1-1/2
Idle Speed		± 200 RPM	1500	1500	1500
Gas Type/Pump Octane Number			Unleaded/87	Unleaded/87	Unleaded/87
Gas/Oil Ratio			Injection	Injection	Injection
Type			Liquid	Liquid	Liquid
Axial Fan Belt Adjustment	Deflection	mm (in)	N.A.	N.A.	N.A.
	Force	kg (lbf)	N.A.	N.A.	N.A.
Thermostat Opening Temperature		°C (°F)	42 (108)	42 (108)	42 (108)
Radiator Cap Opening Pressure		kPa (PSI)	90 (13)	90 (13)	90 (13)
ENGINE COLD N•m (lbf•ft)	Drive Pulley Retaining Screw		⑦	⑦	⑦
	Exhaust Manifold Nuts or Bolts		22 (16)	22 (16)	22 (16)
	Magneto Ring Nut		125 (92)	125 (92)	125 (92)
	Crankcase Nuts or Screws	M6 M8	9 (7) 29 (21)	9 (7) 29 (21)	9 (7) 29 (21)
	Crankcase/Engine Support Nuts or Screws		35 (26)	35 (26)	35 (26)
	Cylinder Head Screws		29 (21)	29 (21)	29 (21)
	Crankcase/Cylinder Nuts or Screws		40 (29)	40 (30)	40 (30)
	Axial Fan Shaft Nut		N.A.	N.A.	N.A.

VEHICLE MODEL			MX Z 800 SPORT (CAN./U.S.)	MX Z 800 R SPORT (CAN./U.S.)	MX Z 800 TRAIL (CAN./U.S.)
ENGINE TYPE			**793**	**793**	**793**
Number of Cylinders			2	2	2
Bore		mm (in)	82.00 (3.228)	82.00 (3.228)	82.00 (3.228)
Stroke		mm (in)	75.70 (2.980)	75.70 (2.980)	75.70 (2.980)
Displacement		cm^3 (in^3)	799.20 (48.77)	799.20 (48.77)	799.20 (48.77)
Compression Ratio (corrected)		± 0.5	12.0	12.0	12.0
Maximum Power Engine Speed ①		± 100 RPM	7900	7900	7900
Piston Ring Type		1st/2nd	ST/N.A.	ST/N.A.	ST/N.A.
Ring End Gap	New Wear Limit	mm (in) mm (in)	0.4 (.016) 1.0 (.039)	0.4 (.016) 1.0 (.039)	0.4 (.016) 1.0 (.039)
Ring/Piston Groove Clearance	New Wear Limit	mm (in) mm (in)	0.05 (.0020) 0.2 (.0079)	0.05 (.0020) 0.2 (.0079)	0.05 (.0020) 0.2 (.0079)
Piston/Cylinder Wall Clearance	New Wear Limit	mm (in) mm (in)	0.125 ± 0.013 (.0049 ± .0005) 0.20 (.0079)	0.125 ± 0.013 (.0049 ± .0005) 0.20 (.0079)	0.125 ± 0.013 (.0049 ± .0005) 0.20 (.0079)
Connecting Rod Big End Axial Play	New Wear Limit	mm (in) mm (in)	0.39 (.0154) 1.2 (.0472)	0.39 (.0154) 1.2 (.0472)	0.39 (.0154) 1.2 (.0472)
Maximum Crankshaft End-play ②		mm (in)	0.3 (.012)	0.3 (.012)	0.3 (.012)
Maximum Crankshaft Deflection at PTO		mm (in)	0.06 (.0024)	0.06 (.0024)	0.06 (.0024)
Magneto Generator Output		W	290	290	290
Ignition Type			CDI	CDI	CDI
Spark Plug Make and Type			NGK BR9ECS	NGK BR9ECS	NGK BR9ECS
Spark Plug Gap		± 0.05 mm (± .002 in)	0.45 (.018)	0.45 (.018)	0.45 (.018)
Ignition Timing BTDC ③		mm (in)	3.51 (.138)	3.51 (.138)	3.51 (.138)
Trigger Coil ④		Ω	190 – 300	190 – 300	190 – 300
Generating Coil ④	Low Speed	Ω	17.5 – 42.5	17.5 – 42.5	17.5 – 42.5
	High Speed	Ω	2.4 – 5.8	2.4 – 5.8	2.4 – 5.8
Lighting Coil ④		Ω	0.1 – 0.4	0.1 – 0.4	0.1 – 0.4
High Tension Coil ④	Primary	Ω	0.3 – 0.7	0.3 – 0.7	0.3 – 0.7
	Secondary	kΩ	8.0 – 16.0	8.0 – 16.0	8.0 – 16.0
Carburetor Type		PTO/MAG	TM 40-B166	TM 40-B166	TM 40-B166
Main Jet		PTO/MAG	520N/520N	520N/520N	520N/520N
Needle Jet			P-0 ⑤	P-0 ⑤	P-0 ⑤
Pilot Jet			17.5	17.5	17.5
Needle Identification — Clip Position			9ZLY2/58 ⑥	9ZLY2/58 ⑥	9ZLY2/58 ⑥
Slide Cut-Away			2.0	2.0	2.0
Float Adjustment		± 1 mm (± .040 in)	N.A.	N.A.	N.A.
Air or Pilot Screw Adjustment		± 1/16 Turn	1-1/2	1-1/2	1-1/2
Idle Speed		± 200 RPM	1500	1500	1500
Gas Type/Pump Octane Number			Unleaded/87	Unleaded/87	Unleaded/87
Gas/Oil Ratio			Injection	Injection	Injection
Type			Liquid	Liquid	Liquid
Axial Fan Belt Adjustment	Deflection	mm (in)	N.A.	N.A.	N.A.
	Force	kg (lbf)	N.A.	N.A.	N.A.
Thermostat Opening Temperature		°C (°F)	42 (108)	42 (108)	42 (108)
Radiator Cap Opening Pressure		kPa (PSI)	90 (13)	90 (13)	90 (13)
ENGINE COLD N•m (lbf•ft)	Drive Pulley Retaining Screw		⑦	⑦	⑦
	Exhaust Manifold Nuts or Bolts		22 (16)	22 (16)	22 (16)
	Magneto Ring Nut		125 (92)	125 (92)	125 (92)
	Crankcase Nuts or Screws	M6 M8	9 (7) 29 (21)	9 (7) 29 (21)	9 (7) 29 (21)
	Crankcase/Engine Support Nuts or Screws		35 (26)	35 (26)	35 (26)
	Cylinder Head Screws		29 (21)	29 (21)	29 (21)
	Crankcase/Cylinder Nuts or Screws		40 (29)	40 (29)	40 (29)
	Axial Fan Shaft Nut		N.A.	N.A.	N.A.

VEHICLE MODEL			MX Z 800 R ADRENALINE (CAN./U.S.)	MX Z 800 R RENEGADE (CAN./U.S.)	MX Z 800 X (CAN./U.S.)
ENGINE TYPE			793	793	793
Number of Cylinders			2	2	2
Bore		mm (in)	82.00 (3.228)	82.00 (3.228)	82.00 (32.228)
Stroke		mm (in)	75.70 (2.980)	75.7 (2.980)	75.70 (2.980)
Displacement		cm^3 (in^3)	799.20 (48.77)	799.20 (48.77)	799.20 (48.77)
Compression Ratio (corrected)		± 0.5	12.0	12.0	12.0
Maximum Power Engine Speed ①		± 100 RPM	7900	7900	7900
Piston Ring Type		$1^{st}/2^{nd}$	ST/N.A.	ST/N.A.	ST/N.A.
Ring End Gap	New	mm (in)	0.4 (.016)	0.4 (.016)	0.4 (.016)
	Wear Limit	mm (in)	1.0 (.039)	1.0 (.039)	1.0 (.039)
Ring/Piston Groove Clearance	New	mm (in)	0.05 (.0020)	0.05 (.0020)	0.05 (.0020)
	Wear Limit	mm (in)	0.2 (.0079)	0.2 (.0079)	0.2 (.0079)
Piston/Cylinder Wall Clearance	New	mm (in)	0.125 ± 0.013 (.0049 ± .0005)	0.125 ± 0.013 (.0049 ± .0005)	0.125 ± 0.013 (.0049 ± .0005)
	Wear Limit	mm (in)	0.20 (.0079)	0.20 (.0079)	0.20 (.0079)
Connecting Rod Big End Axial Play	New	mm (in)	0.39 (.0154)	0.39 (.0154)	0.39 (.0154)
	Wear Limit	mm (in)	1.2 (.0472)	1.2 (.0472)	1.2 (.0472)
Maximum Crankshaft End-play ②		mm (in)	0.3 (.012)	0.3 (.012)	0.3 (.012)
Maximum Crankshaft Deflection at PTO		mm (in)	0.06 (.0024)	0.06 (.0024)	0.06 (.0024)
Magneto Generator Output		W	290	290	290
Ignition Type			CDI	CDI	CDI
Spark Plug Make and Type			NGK BR9ECS	NGK BR9ECS	NGK BR9ECS
Spark Plug Gap		± 0.05 mm (± .002 in)	0.45 (.018)	0.45 (.018)	0.45 (.018)
Ignition Timing BTDC ③		mm (in)	3.51 (.138)	3.51 (.138)	3.51 (.138)
Trigger Coil ④		Ω	190 – 300	190 – 300	190 – 300
Generating Coil ④	Low Speed	Ω	17.5 – 42.5	17.5 – 42.5	17.5 – 42.5
	High Speed	Ω	2.4 – 5.8	2.4 – 5.8	2.4 – 5.8
Lighting Coil ④		Ω	0.1 – 0.4	0.1 – 0.4	0.1 – 0.4
High Tension Coil ④	Primary	Ω	0.3 – 0.7	0.3 – 0.7	0.3 – 0.7
	Secondary	kΩ	8.0 – 16.0	8.0 – 16.0	8.0 – 16.0
Carburetor Type		PTO/MAG	TM 40-B166	TM 40-B166	TM 40-B166
Main Jet		PTO/MAG	520N/520N	520N/520N	520N/520N
Needle Jet			P-0 ⑤	P-0 ⑤	P-0 ⑤
Pilot Jet			17.5	17.5	17.5
Needle Identification — Clip Position			9ZLY2/58 ⑥	9ZLY2/58 ⑥	9ZLY2/58 ⑥ 9ZLY3/58 ⑥
Slide Cut-Away			2.0	2.0	2.0
Float Adjustment		± 1 mm (± .040 in)	N.A.	N.A.	N.A.
Air or Pilot Screw Adjustment		± 1/16 Turn	1-1/2	1-1/2	1-1/2
Idle Speed		± 200 RPM	1500	1500	1500
Gas Type/Pump Octane Number			Unleaded/87	Unleaded/87	Unleaded/87
Gas/Oil Ratio			Injection	Injection	Injection
Type			Liquid	Liquid	Liquid
Axial Fan Belt Adjustment	Deflection	mm (in)	N.A.	N.A.	N.A.
	Force	kg (lbf)	N.A.	N.A.	N.A.
Thermostat Opening Temperature		°C (°F)	42 (108)	42 (108)	42 (108)
Radiator Cap Opening Pressure		kPa (PSI)	90 (13)	90 (13)	90 (13)
ENGINE COLD N•m (lbf•ft)	Drive Pulley Retaining Screw		⑦	⑦	⑦
	Exhaust Manifold Nuts or Bolts		22 (16)	22 (16)	22 (16)
	Magneto Ring Nut		125 (92)	125 (92)	125 (92)
	Crankcase Nuts or Screws	M6	9 (7)	9 (7)	9 (7)
		M8	29 (21)	29 (21)	29 (21)
	Crankcase/Engine Support Nuts or Screws		35 (26)	35 (26)	35 (26)
	Cylinder Head Screws		29 (21)	29 (21)	29 (21)
	Crankcase/Cylinder Nuts or Screws		40 (29)	40 (29)	40 (30)
	Axial Fan Shaft Nut		N.A.	N.A.	N.A.

VEHICLE MODEL			MX Z 800 R X (CAN./U.S.)	SUMMIT 600 SPORT (CAN./U.S.)	SUMMIT 600 R SPORT (CAN./U.S.)
ENGINE TYPE			**793**	**593**	**593**
Number of Cylinders			2	2	2
Bore		mm (in)	82.00 (32.228)	76.00 (2.992)	76.00 (2.992)
Stroke		mm (in)	75.70 (2.980)	65.80 (2.591)	65.80 (2.591)
Displacement		cm^3 (in^3)	799.20 (48.77)	597.00 (36.43)	597.00 (36.43)
Compression Ratio (corrected)		± 0.5	12.0	12.0	12.0
Maximum Power Engine Speed ①		± 100 RPM	7900	8000	8000
Piston Ring Type		1st/2nd	ST/N.A.	ST/N.A.	ST/N.A.
Ring End Gap	New	mm (in)	0.4 (.016)	0.4 (.016)	0.4 (.016)
	Wear Limit	mm (in)	1.0 (.039)	1.0 (.039)	1.0 (.039)
Ring/Piston Groove Clearance	New	mm (in)	0.05 (.0020)	0.045 (.0016)	0.045 (.0016)
	Wear Limit	mm (in)	0.2 (.0079)	0.2 (.0079)	0.2 (.0079)
Piston/Cylinder Wall Clearance	New	mm (in)	0.125 ± 0.013 (.0049 ± .0005)	0.120 ± 0.016(.0047 ± .0006)	0.120 ± 0.016 (.0047 ± .0006)
	Wear Limit	mm (in)	0.20 (.0079)	0.20 (.0079)	0.20 (.0079)
Connecting Rod Big End Axial Play	New	mm (in)	0.39 (.0154)	0.39 (.0154)	0.39 (.0154)
	Wear Limit	mm (in)	1.2 (.0472)	1.2 (.0472)	1.2 (.0472)
Maximum Crankshaft End-play ②		mm (in)	0.3 (.012)	0.3 (.012)	0.3 (.012)
Maximum Crankshaft Deflection at PTO		mm (in)	0.06 (.0024)	0.06 (.0024)	0.06 (.0024)
Magneto Generator Output		W	290	290	290
Ignition Type			CDI	CDI	CDI
Spark Plug Make and Type			NGK BR9ECS	NGK BR9ECS	NGK BR9ECS
Spark Plug Gap		± 0.05 mm (± .002 in)	0.45 (.018)	0.45 (.018)	0.45 (.018)
Ignition Timing BTDC ③		mm (in)	3.51 (.138)	3.00 (.118)	3.00 (.118)
Trigger Coil ④		Ω	190 – 300	190 – 300	190 – 300
Generating Coil ④	Low Speed	Ω	17.5 – 42.5	17.5 – 42.5	17.5 – 42.5
	High Speed	Ω	2.4 – 5.8	2.4 – 5.8	2.4 – 5.8
Lighting Coil ④		Ω	0.1 – 0.4	0.1 – 0.4	0.1 – 0.4
High Tension Coil ④	Primary	Ω	0.3 – 0.7	0.3 – 0.7	0.3 – 0.7
	Secondary	kΩ	8.0 – 16.0	8.0 – 16.0	8.0 – 16.0
Carburetor Type		PTO/MAG	TM 40-B166	TM 40-B157	TM 40-B157
Main Jet		PTO/MAG	520N/520N	500/500	500/500
Needle Jet			P-0 ⑤	P-0 ⑤	P-0 ⑤
Pilot Jet			17.5	20	20
Needle Identification — Clip Position			9ZLY2/58 ⑥ 9ZLY3/58 ⑥	9HGY1/58 ⑥	9HGY1/58 ⑥
Slide Cut-Away			2.0	2.0	2.0
Float Adjustment		± 1 mm (± .040 in)	N.A.	N.A.	N.A.
Air or Pilot Screw Adjustment		± 1/16 Turn	1-1/2	1-1/2	1-1/2
Idle Speed		± 200 RPM	1500	1500	1500
Gas Type/Pump Octane Number			Unleaded/87	Unleaded/87	Unleaded/87
Gas/Oil Ratio			Injection	Injection	Injection
Type			Liquid	Liquid	Liquid
Axial Fan Belt Adjustment	Deflection	mm (in)	N.A.	N.A.	N.A.
	Force	kg (lbf)	N.A.	N.A.	N.A.
Thermostat Opening Temperature		°C (°F)	42 (108)	42 (108)	42 (108)
Radiator Cap Opening Pressure		kPa (PSI)	90 (13)	90 (13)	90 (13)
ENGINE COLD N•m (lbf•ft)					
Drive Pulley Retaining Screw			⑦	⑦	⑦
Exhaust Manifold Nuts or Bolts			22 (16)	22 (16)	22 (16)
Magneto Ring Nut			125 (92)	125 (92)	125 (92)
Crankcase Nuts or Screws		M6	9 (7)	9 (7)	9 (7)
		M8	29 (21)	29 (21)	29 (21)
Crankcase/Engine Support Nuts or Screws			35 (26)	35 (26)	35 (26)
Cylinder Head Screws			29 (21)	29 (21)	29 (21)
Crankcase/Cylinder Nuts or Screws			40 (30)	29 (21)	29 (21)
Axial Fan Shaft Nut			N.A.	N.A.	N.A.

	VEHICLE MODEL			SUMMIT 700 SPORT (CAN./U.S.)	SUMMIT 700 R SPORT (CAN./U.S.)	SUMMIT 800 SPORT (CAN./U.S.)
	ENGINE TYPE			**693**	**693**	**793**
	Number of Cylinders			2	2	2
	Bore		mm (in)	78.00 (3.071)	78.00 (3.071)	82.00 (3.228)
	Stroke		mm (in)	73.0 (2.874)	73.0 (2.874)	75.70 (2.980)
	Displacement		cm^3 (in^3)	697.70 (42.58)	697.70 (42.58)	799.20 (48.77)
	Compression Ratio (corrected)		± 0.5	12.0	12.0	12.0
	Maximum Power Engine Speed ①		± 100 RPM	8000	8000	7900
	Piston Ring Type		1st/2nd	ST/N.A.	ST/N.A.	ST/N.A.
	Ring End Gap	New Wear Limit	mm (in) mm (in)	0.4 (.016) 1.0 (.039)	0.4 (.016) 1.0 (.039)	0.4 (.016) 1.0 (.039)
	Ring/Piston Groove Clearance	New Wear Limit	mm (in) mm (in)	0.04 (.0016) 0.2 (.0079)	0.04 (.0016) 0.2 (.0079)	0.05 (.0020) 0.2 (.0079)
	Piston/Cylinder Wall Clearance	New Wear Limit	mm (in) mm (in)	0.115 ± 0.013 (.0045 ± .0005) 0.20 (.0079)	0.115 ± 0.013 (.0045 ± .0005) 0.20 (.0079)	0.125 ± 0.013 (.0049 ± .0005) 0.20 (.0079)
	Connecting Rod Big End Axial Play	New Wear Limit	mm (in) mm (in)	0.39 (.0154) 1.2 (.0472)	0.39 (.0154) 1.2 (.0472)	0.39 (.0154) 1.2 (.0472)
	Maximum Crankshaft End-play ②		mm (in)	0.3 (.012)	0.3 (.012)	0.3 (.012)
	Maximum Crankshaft Deflection at PTO		mm (in)	0.06 (.0024)	0.06 (.0024)	0.06 (.0024)
	Magneto Generator Output		W	290	290	290
	Ignition Type			CDI	CDI	CDI
	Spark Plug Make and Type			NGK BR9ECS	NGK BR9ECS	NGK BR9ECS
	Spark Plug Gap		± 0.05 mm (± .002 in)	0.45 (.018)	0.45 (.018)	0.45 (.018)
	Ignition Timing BTDC ③		mm (in)	3.36 (.132)	3.36 (.132)	3.51 (.138)
	Trigger Coil ④		Ω	190 – 300	190 – 300	190 – 300
	Generating Coil ④	Low Speed	Ω	17.5 – 42.5	17.5 – 42.5	17.5 – 42.5
		High Speed	Ω	2.4 – 5.8	2.4 – 5.8	2.4 – 5.8
	Lighting Coil ④		Ω	0.1 – 0.4	0.1 – 0.4	0.1 – 0.4
	High Tension Coil ④	Primary	Ω	0.3 – 0.7	0.3 – 0.7	0.3 – 0.7
		Secondary	kΩ	8.0 – 16.0	8.0 – 16.0	8.0 – 16.0
	Carburetor Type		PTO/MAG	TM 40-B163	TM 40-B163	TM 40-B175
	Main Jet		PTO/MAG	510N/510N	510N/510N	520N/520N
	Needle Jet			P-0 ⑤	P-0 ⑤	P-0 ⑤
	Pilot Jet			17.5	17.5	17.5
	Needle Identification — Clip Position			9ZLY3/58 ⑥	9ZLY3/58 ⑥	9ZLY2/58 ⑥
	Slide Cut-Away			2.0	2.0	2.0
	Float Adjustment		± 1 mm (± .040 in)	N.A.	N.A.	N.A.
	Air or Pilot Screw Adjustment		± 1/16 Turn	1-1/2	1-1/2	1-1/2
	Idle Speed		± 200 RPM	1500	1500	1500
	Gas Type/Pump Octane Number			Unleaded/87	Unleaded/87	Unleaded/87
	Gas/Oil Ratio			Injection	Injection	Injection
	Type			Liquid	Liquid	Liquid
	Axial Fan Belt Adjustment	Deflection	mm (in)	N.A.	N.A.	N.A.
		Force	kg (lbf)	N.A.	N.A.	N.A.
	Thermostat Opening Temperature		°C (°F)	42 (108)	42 (108)	42 (108)
	Radiator Cap Opening Pressure		kPa (PSI)	90 (13)	90 (13)	90 (13)
ENGINE COLD N•m (lbf•ft)	Drive Pulley Retaining Screw			⑦	⑦	⑦
	Exhaust Manifold Nuts or Bolts			22 (16)	22 (16)	22 (16)
	Magneto Ring Nut			125 (92)	125 (92)	125 (92)
	Crankcase Nuts or Screws		M6 M8	9 (7) 29 (21)	9 (7) 29 (21)	9 (7) 29 (21)
	Crankcase/Engine Support Nuts or Screws			35 (26)	35 (26)	35 (26)
	Cylinder Head Screws			29 (21)	29 (21)	29 (21)
	Crankcase/Cylinder Nuts or Screws			40 (29)	40 (29)	40 (29)
	Axial Fan Shaft Nut			N.A.	N.A.	N.A.

	VEHICLE MODEL			SUMMIT 800 R SPORT (CAN./U.S.)	SUMMIT 800 X (CAN./U.S.)	SUMMIT 800 R X (CAN./U.S.)
	ENGINE TYPE			**793**	**793**	**793**
	Number of Cylinders			2	2	2
	Bore		mm (in)	82.00 (3.228)	82.00 (3.228)	82.00 (3.228)
	Stroke		mm (in)	75.70 (2.980)	75.70 (2.980)	75.70 (2.980)
	Displacement		cm^3 (in^3)	799.20 (48.77)	799.20 (48.77)	799.20 (48.77)
	Compression Ratio (corrected)		± 0.5	12.0	12.0	12.0
	Maximum Power Engine Speed ①		± 100 RPM	7900	7900	7900
	Piston Ring Type		1st/2nd	ST/N.A.	ST/N.A.	ST/N.A.
	Ring End Gap	New Wear Limit	mm (in) mm (in)	0.4 (.016) 1.0 (.039)	0.4 (.016) 1.0 (.039)	0.4 (.016) 1.0 (.039)
	Ring/Piston Groove Clearance	New Wear Limit	mm (in) mm (in)	0.05 (.0020) 0.2 (.0079)	0.05 (.0020) 0.2 (.0079)	0.05 (.0020) 0.2 (.0079
	Piston/Cylinder Wall Clearance	New Wear Limit	mm (in) mm (in)	0.125 ± 0.013 (.0049 ± .0005) 0.20 (.0079)	0.125 ± 0.013 (.0049 ± .0005) 0.20 (.0079)	0.125 ± 0.013 (.0049 ± .0005) 0.20 (.0079)
	Connecting Rod Big End Axial Play	New Wear Limit	mm (in) mm (in)	0.39 (.0154) 1.2 (.0472)	0.39 (.0154) 1.2 (.0472)	0.39 (.0154) 1.2 (.0472)
	Maximum Crankshaft End-play ②		mm (in)	0.3 (.012)	0.3 (.012)	0.3 (.012)
	Maximum Crankshaft Deflection at PTO		mm (in)	0.06 (.0024)	0.06 (.0024)	0.06 (.0024)
	Magneto Generator Output		W	290	290	290
	Ignition Type			CDI	CDI	CDI
	Spark Plug Make and Type			NGK BR9ECS	NGK BR9ECS	NGK BR9ECS
	Spark Plug Gap		± 0.05 mm (± .002 in)	0.45 (.018)	0.45 (.018)	0.45 (.018)
	Ignition Timing BTDC ③		mm (in)	3.51 (.138)	3.51 (.138)	3.51 (.138)
	Trigger Coil ④		Ω	190 – 300	190 – 300	190 – 300
	Generating Coil ④	Low Speed	Ω	17.5 – 42.5	17.5 – 42.5	17.5 – 42.5
		High Speed	Ω	2.4 – 5.8	2.4 – 5.8	2.4 – 5.8
	Lighting Coil ④		Ω	0.1 – 0.4	0.1 – 0.4	0.1 – 0.4
	High Tension Coil ④	Primary	Ω	0.3 – 0.7	0.3 – 0.7	0.3 – 0.7
		Secondary	kΩ	8.0 – 16.0	8.0 – 16.0	8.0 – 16.0
	Carburetor Type		PTO/MAG	TM 40-B175	TM 40-B175	TM 40-B175
	Main Jet		PTO/MAG	520N/520N	520N/520N	520N/520N
	Needle Jet			P-0 ⑤	P-0 ⑤	P-0 ⑤
	Pilot Jet			17.5	17.5	17.5
	Needle Identification — Clip Position			9ZLY2/58 ⑥	9ZLY2/58 ⑥	9ZLY2/58 ⑥
	Slide Cut-Away			2.0	2.0	2.0
	Float Adjustment		± 1 mm (± .040 in)	N.A.	N.A.	N.A.
	Air or Pilot Screw Adjustment		± 1/16 Turn	1-1/2	1-1/2	1-1/2
	Idle Speed		± 200 RPM	1500	1500	1500
	Gas Type/Pump Octane Number			Unleaded/87	Unleaded/87	Unleaded/87
	Gas/Oil Ratio			Injection	Injection	Injection
	Type			Liquid	Liquid	Liquid
	Axial Fan Belt Adjustment	Deflection	mm (in)	N.A.	N.A.	N.A.
		Force	kg (lbf)	N.A.	N.A.	N.A.
	Thermostat Opening Temperature		°C (°F)	42 (108)	42 (108)	42 (108)
	Radiator Cap Opening Pressure		kPa (PSI)	90 (13)	90 (13)	90 (13)
ENGINE COLD N•m (lbf•ft)	Drive Pulley Retaining Screw			⑦	⑦	⑦
	Exhaust Manifold Nuts or Bolts			22 (16)	22 (16)	22 (16)
	Magneto Ring Nut			125 (92)	125 (92)	125 (92)
	Crankcase Nuts or Screws		M6 M8	9 (7) 29 (21)	9 (7) 29 (21)	9 (7) 29 (21)
	Crankcase/Engine Support Nuts or Screws			35 (26)	35 (26)	35 (26)
	Cylinder Head Screws			29 (21)	29 (21)	29 (21)
	Crankcase/Cylinder Nuts or Screws			40 (29)	40 (29)	40 (29)
	Axial Fan Shaft Nut			N.A.	N.A.	N.A.

	VEHICLE MODEL			SUMMIT 800 HIGHMARK (CAN./U.S.)	SUMMIT 800 R HIGHMARK (CAN./U.S.)	SUMMIT 800 HIGHMARK X (CAN./U.S.)
	ENGINE TYPE			**793**	**793**	**793**
	Number of Cylinders			2	2	2
	Bore		mm (in)	82.00 (3.228)	82.00 (3.228)	82.00 (3.228)
	Stroke		mm (in)	75.70 (2.980)	75.70 (2.980)	75.70 (2.980)
	Displacement		cm^3 (in^3)	799.20 (48.77)	799.20 (48.77)	799.20 (48.77)
	Compression Ratio (corrected)		± 0.5	12.0	12.0	12.0
	Maximum Power Engine Speed ①		± 100 RPM	7900	7900	7900
	Piston Ring Type		1st/2nd	ST/N.A.	ST/N.A.	ST/N.A.
	Ring End Gap	New Wear Limit	mm (in) mm (in)	0.4 (.016) 1.0 (.039)	0.4 (.016) 1.0 (.039)	0.4 (.016) 1.0 (.039)
	Ring/Piston Groove Clearance	New Wear Limit	mm (in) mm (in)	0.05 (.0020) 0.2 (.0079)	0.04 (.0016) 0.2 (.0079)	0.05 (.0020) 0.2 (.0079)
	Piston/Cylinder Wall Clearance	New Wear Limit	mm (in) mm (in)	0.125 ± 0.013 (.0049 ± .0005) 0.20 (.0079)	0.115 ± 0.013 (.0045 ± .0005) 0.20 (.0079)	0.125 ± 0.013 (.0049 ± .0005) 0.20 (.0079)
	Connecting Rod Big End Axial Play	New Wear Limit	mm (in) mm (in)	0.39 (.0154) 1.2 (.0472)	0.39 (.0154) 1.2 (.0472)	0.39 (.0154) 1.2 (.0472)
	Maximum Crankshaft End-play ②		mm (in)	0.3 (.012)	0.3 (.012)	0.3 (.012)
	Maximum Crankshaft Deflection at PTO		mm (in)	0.06 (.0024)	0.06 (.0024)	0.06 (.0024)
	Magneto Generator Output		W	290	290	290
	Ignition Type			CDI	CDI	CDI
	Spark Plug Make and Type			NGK BR9ECS	NGK BR9ECS	NGK BR9ECS
	Spark Plug Gap		± 0.05 mm (± .002 in)	0.45 (.018)	0.45 (.018)	0.45 (.018)
	Ignition Timing BTDC ③		mm (in)	3.51 (.138)	3.51 (.138)	3.51 (.138)
	Trigger Coil ④		Ω	190 – 300	190 – 300	190 – 300
	Generating Coil ④	Low Speed	Ω	17.5 – 42.5	17.5 – 42.5	17.5 – 42.5
		High Speed	Ω	2.4 – 5.8	2.4 – 5.8	2.4 – 5.8
	Lighting Coil ④		Ω	0.1 – 0.4	0.1 – 0.4	0.1 – 0.4
	High Tension Coil ④	Primary	Ω	0.3 – 0.7	0.3 – 0.7	0.3 – 0.7
		Secondary	kΩ	8.0 – 16.0	8.0 – 16.0	8.0 – 16.0
	Carburetor Type		PTO/MAG	TM 40-B175	TM 40-B175	TM 40-B175
	Main Jet		PTO/MAG	520N/520N	520N/520N	520N/520N
	Needle Jet			P-0 ⑤	P-0 ⑤	P-0 ⑤
	Pilot Jet			17.5	17.5	17.5
	Needle Identification — Clip Position			9ZLY2/58 ⑥	9ZLY2/58 ⑥	9ZLY2/58 ⑥
	Slide Cut-Away			2.0	2.0	2.0
	Float Adjustment		± 1 mm (± .040 in)	N.A.	N.A.	N.A.
	Air or Pilot Screw Adjustment		± 1/16 Turn	1-1/2	1-1/2	1-1/2
	Idle Speed		± 200 RPM	1500	1500	1500
	Gas Type/Pump Octane Number			Unleaded/87	Unleaded/87	Unleaded/87
	Gas/Oil Ratio			Injection	Injection	Injection
	Type			Liquid	Liquid	Liquid
	Axial Fan Belt Adjustment	Deflection	mm (in)	N.A.	N.A.	N.A.
		Force	kg (lbf)	N.A.	N.A.	N.A.
	Thermostat Opening Temperature		°C (°F)	42 (108)	42 (108)	42 (108)
	Radiator Cap Opening Pressure		kPa (PSI)	90 (13)	90 (13)	90 (13)
ENGINE COLD N•m (lbf•ft)	Drive Pulley Retaining Screw			⑦	⑦	⑦
	Exhaust Manifold Nuts or Bolts			22 (16)	22 (16)	22 (16)
	Magneto Ring Nut			125 (92)	125 (92)	125 (92)
	Crankcase Nuts or Screws		M6 M8	9 (7) 29 (21)	9 (7) 29 (21)	9 (7) 29 (21)
	Crankcase/Engine Support Nuts or Screws			35 (26)	35 (26)	35 (26)
	Cylinder Head Screws			29 (21)	29 (21)	29 (21)
	Crankcase/Cylinder Nuts or Screws			40 (29)	40 (29)	40 (29)
	Axial Fan Shaft Nut			N.A.	N.A.	N.A.

VEHICLE MODEL			SUMMIT 800 R HIGHMARK X (CAN./U.S.)
ENGINE TYPE			**793**
Number of Cylinders			2
Bore		mm (in)	82.00 (3.228)
Stroke		mm (in)	75.70 (2.980)
Displacement		cm³ (in³)	799.20 (48.77)
Compression Ratio (corrected)		± 0.5	12.0
Maximum Power Engine Speed ①		± 100 RPM	7900
Piston Ring Type		1st/2nd	ST/N.A.
Ring End Gap	New Wear Limit	mm (in) mm (in)	0.4 (.016) 1.0 (.039)
Ring/Piston Groove Clearance	New Wear Limit	mm (in) mm (in)	0.05 (.0020) 0.2 (.0079)
Piston/Cylinder Wall Clearance	New Wear Limit	mm (in) mm (in)	0.125 ± 0.013 (.0049 ± .0005) 0.20 (.0079)
Connecting Rod Big End Axial Play	New Wear Limit	mm (in) mm (in)	0.39 (.0154) 1.2 (.0472)
Maximum Crankshaft End-play ②		mm (in)	0.3 (.012)
Maximum Crankshaft Deflection at PTO		mm (in)	0.06 (.0024)
Magneto Generator Output		W	290
Ignition Type			CDI
Spark Plug Make and Type			NGK BR9ECS
Spark Plug Gap		± 0.05 mm (± .002 in)	0.45 (.018)
Ignition Timing BTDC ③		mm (in)	3.51 (.138)
Trigger Coil ④		Ω	190 – 300
Generating Coil ④	Low Speed	Ω	17.5 – 42.5
	High Speed	Ω	2.4 – 5.8
Lighting Coil ④		Ω	0.1 – 0.4
High Tension Coil ④	Primary	Ω	0.3 – 0.7
	Secondary	kΩ	8.0 – 16.0
Carburetor Type		PTO/MAG	TM 40-B175
Main Jet		PTO/MAG	520N/520N
Needle Jet			P-0 ⑤
Pilot Jet			17.5
Needle Identification — Clip Position			9ZLY2/58 ⑥
Slide Cut-Away			2.0
Float Adjustment		± 1 mm (± .040 in)	N.A.
Air or Pilot Screw Adjustment		± 1/16 Turn	1-1/2
Idle Speed		± 200 RPM	1500
Gas Type/Pump Octane Number			Unleaded/87
Gas/Oil Ratio			Injection
Type			Liquid
Axial Fan Belt Adjustment	Deflection	mm (in)	N.A.
	Force	kg (lbf)	N.A.
Thermostat Opening Temperature		°C (°F)	42 (108)
Radiator Cap Opening Pressure		kPa (PSI)	90 (13)
ENGINE COLD N•m (lbf•ft)	Drive Pulley Retaining Screw		⑦
	Exhaust Manifold Nuts or Bolts		22 (16)
	Magneto Ring Nut		125 (92)
	Crankcase Nuts or Screws	M6 M8	9 (7) 29 (21)
	Crankcase/Engine Support Nuts or Screws		35 (26)
	Cylinder Head Screws		29 (21)
	Crankcase/Cylinder Nuts or Screws		40 (29)
	Axial Fan Shaft Nut		N.A.

VEHICLES

VEHICLE MODEL				MX Zx 440 RACING (CAN./U.S.)	MX Z 500 SPORT (CAN./U.S.)	MX Z 500 R SPORT (CAN./U.S.)
ENGINE TYPE				**453**	**493**	**493**
Chain Drive Ratio				21/43	22/43	22/43
Chain	Pitch		in	3/8	3/8	3/8
	Type/Links Qty/Plates Qty			Silent 74/15	Silent 74/11	Silent 74/11
Drive Pulley	Type of Drive Pulley			TRA	TRA	TRA
	Ramp Identification and Roller Pin Type			296 ⑧	283 ⑤	283 ⑤
	Calibration Screw Position or Calibration Disc Quantity			4	4	3
	Spring Color			Pink/White	Green/White	Green/Pink
	Spring Length		mm (in)	124.5 (4.902)	110.7 (4.36)	118.0 (4.65)
	Clutch Engagement		± 100 RPM	5000	4400	4400
Driven Pulley	Type			FORMULA	FORMULA	HPV27
	Spring Preload		± 0.7 kg (± 1.5 lb)	7.0 (15.43)	7.0 (15.4)	N.A.
	Cam Angle		Degree	48/44	42	44
Pulley Distance	Z		± 0.5 mm (± .020 in)	16.5 (.650)	16.5 (.650)	16.5 (.650)
Offset	X		± 0.5 mm (± .020 in)	35.5 (1.398)	35.5 (1.398)	35.5 (1.398)
	Y – X	MIN. – MAX.	mm (in)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)
Drive Belt Part Number (P/N)				414 860 700	414 860 700	414 860 700
Drive Belt Width (new) ①			mm (in)	35.3 (1.390)	35.30 (1.390)	35.30 (1.390)
Drive Belt Adjustment		Deflection	± 5 mm (± .197 in)	32 (1.260)	32 (1.260)	32 (1.260)
		Force ②	kg (lbf)	11.3 (25)	11.3 (25)	11.3 (25)
Track	Width		mm (in)	381 (15.0)	381 (15.0)	381 (15.0)
	Length		mm (in)	3074 (121)	3074 (121)	3074 (121)
	Profile Height		mm (in)	36.8 (1.45)	22.3 (0.9)	22.3 (0.9)
	Adjustment	Deflection	mm (in)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)
		Force ③	kg (lbf)	7.3 (16)	7.3 (16)	7.3 (16)
Suspension Type		Track		SC-10 III	SC-10 III	SC-10 III
		Ski		ADSA	ADSA	ADSA
Length			mm (in)	2801 (110)	2725 (107.3)	2725 (107.3)
Width			mm (in)	1213 (48)	1329 (52.3)	1329 (52.3)
Height			mm (in)	1130 (44)	1130 (44.5)	1130 (44.5)
Ski Stance (carbide to carbide)			mm (in)	1080 (43)	1195 (47.0)	1195 (47.0)
Toe-out and Camber			mm (in) degree	0 (0) 0	0 (0) 0	0 (0) 0
Mass (dry)			kg (lb)	210 (463)	213 (468)	213 (468)
Ground Contact Area			cm^2 (in^2)	6671 (1034)	6836 (1060)	6836 (1060)
Ground Contact Pressure			kPa (PSI)	3.09 (.448)	3.06 (.444)	3.06 (.444)
Frame Material				Aluminum	Aluminum	Aluminum
Bottom Pan Material				Impact Copolymer	Impact Copolymer	Impact Copolymer
Hood Material				RRIM Polyurethane	RRIM Polyurethane	RRIM Polyurethane
Battery			V/A•h	N.A.	N.A.	N.A.
Headlight			W	H4 60/55	H4 60/55	H4 60/55
Taillight and Stoplight			W	8/27	8/27	8/27
Tachometer and Speedometer Bulbs			W	3	3	3
Fuel and Temperature Gauge Bulbs			W	N.A.	N.A.	N.A.
Fuse	Starter Solenoid		A	N.A.	N.A.	N.A.
	Fuel Level Sensor		A	N.A.	N.A.	N.A.
Fuel Tank			L (U.S. gal)	37.3 (9.9)	37.3 (9.9)	37.3 (9.9)
Chaincase/Gearbox			mL (U.S. oz)	250 (8.5)	250 (8.5)	250 (8.5)
Cooling System ④			L (U.S. oz)	3.8 (128.5)	3.8 (128.5)	3.8 (128.5)
Injection Oil Reservoir			L (U.S. oz)	N.A.	3.5 (118.4)	3.5 (118.4)

VEHICLE MODEL				MX Z 500 TRAIL (CAN./U.S.)	MX Z 600 SPORT (CAN./U.S.)	MX Z 600 R SPORT (CAN./U.S.)
ENGINE TYPE				493	593	593
Chain Drive Ratio				22/43	24/43	24/43
Chain	Pitch		in	3/8	3/8	3/8
	Type/Links Qty/Plates Qty			Silent 74/11	Silent 74/13	Silent 74/13
Drive Pulley	Type of Drive Pulley			TRA	TRA	TRA
	Ramp Identification and Roller Pin Type			283 ⑤	299 ⑤	299 ⑤
	Calibration Screw Position or Calibration Disc Quantity			4	4	3
	Spring Color			Green/White	Green/White	Green/Violet
	Spring Length		mm (in)	110.7 (4.35)	110.7 (4.36)	133.5 (5.26)
	Clutch Engagement		± 100 RPM	4400	4100	4100
Driven Pulley	Type			FORMULA	FORMULA	HPV27
	Spring Preload		± 0.7 kg (± 1.5 lb)	7.0 (15.4)	7.5 (16.54)	N.A.
	Cam Angle		Degree	42	47	47
Pulley Distance	Z		± 0.5 mm (± .020 in)	16.5 (.650)	16.5 (.650)	16.5 (.650)
Offset	X		± 0.5 mm (± .020 in)	35.5 (1.398)	35.5 (1.398)	35.5 (1.398)
	Y – X	MIN. – MAX.	mm (in)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)
Drive Belt Part Number (P/N)				414 860 700	414 860 700	414 860 700
Drive Belt Width (new) ①			mm (in)	35.3 (1.390)	35.3 (1.390)	35.3 (1.390)
Drive Belt Adjustment		Deflection	± 5 mm (± .197 in)	32 (1.260)	32 (1.260)	32 (1.260)
		Force ②	kg (lbf)	11.3 (25)	11.3 (25)	11.3 (25)
Track	Width		mm (in)	381 (15.0)	381 (15.0)	381 (15.0)
	Length		mm (in)	3074 (121)	3074 (121)	3074 (121)
	Profile Height		mm (in)	22.3 (.880)	22.3 (.880)	22.3 (.880)
	Adjustment	Deflection	mm (in)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)
		Force ③	kg (lbf)	7.3 (16)	7.3 (16)	7.3 (16)
Suspension Type		Track		SC-10 III	SC-10 III	SC-10 III
		Ski		ADSA	ADSA	ADSA
Length			mm (in)	2725 (107.3)	2725 (107)	2725 (107)
Width			mm (in)	1213 (47.7)	1329 (52)	1329 (52)
Height			mm (in)	1130 (44.5)	1130 (44)	1130 (44)
Ski Stance (carbide to carbide)			mm (in)	1080 (42.5)	1195 (47)	1195 (47)
Toe-out and Camber			mm (in) degree	0 (0) 0	0 (0) 0	0 (0) 0
Mass (dry)			kg (lb)	213 (468)	215 (472)	215 (472)
Ground Contact Area			cm^2 (in^2)	6670.9 (1034)	6836 (1060)	6836 (1060)
Ground Contact Pressure			kPa (PSI)	3.13 (.454)	3.09 (.448)	3.09 (.448)
Frame Material				Aluminum	Aluminum	Aluminum
Bottom Pan Material				Impact Copolymer	Impact Copolymer	Impact Copolymer
Hood Material				RRIM Polyurethane	RRIM Polyurethane	RRIM Polyurethane
Battery			V/A•h	N.A.	N.A.	N.A.
Headlight			W	H4 60/55	H4 60/55	H4 60/55
Taillight and Stoplight			W	8/27	8/27	8/27
Tachometer and Speedometer Bulbs			W	3	3	3
Fuel and Temperature Gauge Bulbs			W	N.A.	N.A.	N.A.
Fuse	Starter Solenoid		A	N.A.	N.A.	N.A.
	Fuel Level Sensor		A	N.A.	N.A.	N.A.
Fuel Tank			L (U.S. gal)	37.3 (9.9)	37.3 (9.9)	37.3 (9.9)
Chaincase/Gearbox			mL (U.S. oz)	250 (8.5)	250 (8.5)	250 (8.5)
Cooling System ④			L (U.S. oz)	3.8 (128.5)	3.8 (128.5)	3.8 (128.5)
Injection Oil Reservoir			L (U.S. oz)	3.5 (118.4)	3.5 (118.4)	3.5 (118.4)

VEHICLE MODEL				MX Z 600 TRAIL (CAN./U.S.)	MX Z 600 R ADRENALINE (CAN./U.S.)	MX Z 600 R RENEGADE (CAN./U.S.)
ENGINE TYPE				**593**	**593**	**593**
Chain Drive Ratio				24/43	24/43	21/43
Chain	Pitch		in	3/8	3/8	3/8
	Type/Links Qty/Plates Qty			Silent 74/13	Silent 74/13	Silent 74/13
Drive Pulley	Type of Drive Pulley			TRA	TRA	TRA
	Ramp Identification and Roller Pin Type			299 ⑤	299 ⑤	299 ⑤
	Calibration Screw Position or Calibration Disc Quantity			4	3	3
	Spring Color			Green/White	Green/Violet	Violet/Violet
	Spring Length		mm (in)	110.7 (4.35)	133.7 (5.26)	107.0 (4.21)
	Clutch Engagement		± 100 RPM	4100	4100	3800
Driven Pulley	Type			FORMULA	HPV27	HPV27
	Spring Preload		± 0.7 kg (± 1.5 lb)	7.0 (15.4)	N.A.	N.A.
	Cam Angle		Degree	47	47	47
Pulley Distance	Z		± 0.5 mm (± .020 in)	16.5 (.650)	16.5 (.650)	16.5 (.650)
Offset	X		± 0.5 mm (± .020 in)	35.5 (1.398)	35.5 (1.398)	35.5 (1.398)
	Y – X	MIN. – MAX.	mm (in)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)
Drive Belt Part Number (P/N)				414 860 700	414 860 700	417 300 127
Drive Belt Width (new) ①			mm (in)	35.3 (1.390)	35.30 (1.390)	36.35 (1.431)
Drive Belt Adjustment		Deflection	± 5 mm (± .197 in)	32 (1.260)	32 (1.260)	32 (1.260)
		Force ②	kg (lbf)	11.3 (25)	11.3 (25)	11.3 (25)
Track	Width		mm (in)	381 (15.0)	381 (15.0)	381 (15.0)
	Length		mm (in)	3074 (121)	3074 (121)	3455 (136)
	Profile Height		mm (in)	22.3 (.880)	22.3 (.9)	31.8 (1.3)
	Adjustment	Deflection	mm (in)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)
		Force ③	kg (lbf)	7.3 (16)	7.3 (16)	7.3 (16)
Suspension Type		Track		SC-10 III	SC-10 III	SC-10 II 136
		Ski		ADSA	ADSA	ADSA
Length			mm (in)	2725 (107.3)	2725 (107.3)	3005 (118.3)
Width			mm (in)	1213 (47.7)	1218 (48.0)	1172 (46.1)
Height			mm (in)	1130 (44.5)	1130 (44.5)	1136 (44.7)
Ski Stance (carbide to carbide)			mm (in)	1080 (42.5)	1195 (47)	1092 or 1156 (43 or 45.5)
Toe-out and Camber			mm (in) degree	0 (0) 0	0 (0) 0	0 (0) 0
Mass (dry)			kg (lb)	213 (469)	215 (472)	221 (486)
Ground Contact Area			cm^2 (in^2)	6670.9 (1034)	6836 (1060)	7522 (1166)
Ground Contact Pressure			kPa (PSI)	3.13 (.469)	3.09 (.448)	2.88 (.418)
Frame Material				Aluminum	Aluminum	Aluminum
Bottom Pan Material				Impact Copolymer	Impact Copolymer	Impact Copolymer
Hood Material				RRIM Polyurethane	RRIM Polyurethane	RRIM Polyurethane
Battery			V/A•h	N.A.	N.A.	N.A.
Headlight			W	H4 60/55	H4 60/55	H4 60/55
Taillight and Stoplight			W	8/27	8/27	8/27
Tachometer and Speedometer Bulbs			W	3	3	3
Fuel and Temperature Gauge Bulbs			W	N.A.	N.A.	N.A.
Fuse	Starter Solenoid		A	N.A.	N.A.	N.A.
	Fuel Level Sensor		A	N.A.	N.A.	N.A.
Fuel Tank			L (U.S. gal)	37.3 (9.9)	37.3 (9.9)	37.3 (9.9)
Chaincase/Gearbox			mL (U.S. oz)	250 (8.5)	250 (8.5)	250 (8.5)
Cooling System ④			L (U.S. oz)	3.8 (128.5)	3.8 (128.5)	4.0 (135.3)
Injection Oil Reservoir			L (U.S. oz)	3.5 (118.4)	3.5 (118.4)	3.5 (118.4)

VEHICLE MODEL				MX Z 600 X (CAN./U.S.)	MX Z 600 R X (CAN./U.S.)	MX Z 700 SPORT (CAN./U.S.)
ENGINE TYPE				593	593	693
Chain Drive Ratio				24/43	24/43	25/43
Chain	Pitch		in	3/8	3/8	3/8
	Type/Links Qty/Plates Qty			Silent 74/13	Silent 74/13	Silent 76/13
Drive Pulley	Type of Drive Pulley			TRA	TRA	TRA
	Ramp Identification and Roller Pin Type			299 ⑤	299 ⑤	300 ⑤
	Calibration Screw Position or Calibration Disc Quantity			4	3	3
	Spring Color			Green/White	Green/Violet	Violet/Yellow
	Spring Length		mm (in)	110.7 (4.36)	133.7 (5.26)	157.9 (6.22)
	Clutch Engagement		± 100 RPM	4100	4100	3800
Driven Pulley	Type			FORMULA	HPV27	FORMULA
	Spring Preload		± 0.7 kg (± 1.5 lb)	7.0 (15.43)	N.A.	8 (17.6)
	Cam Angle		Degree	47	47	48/44
Pulley Distance	Z		± 0.5 mm (± .020 in)	16.5 (.650)	16.5 (.650)	16.5 (.650)
Offset	X		± 0.5 mm (± .020 in)	35.5 (1.398)	35.5 (1.398)	35.5 (1.398)
	Y – X	MIN. – MAX.	mm (in)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)
Drive Belt Part Number (P/N)				414 860 700	414 860 700	417 300 127
Drive Belt Width (new) ①			mm (in)	35.3 (1.390)	35.3 (1.390)	36.4 (1.431)
Drive Belt Adjustment		Deflection	± 5 mm (± .197 in)	32 (1.260)	32 (1.260)	32 (1.260)
		Force ②	kg (lbf)	11.3 (25)	11.3 (25)	11.3 (25)
Track	Width		mm (in)	381 (15.0)	381 (15.0)	381 (15.0)
	Length		mm (in)	3074 (121)	3074 (121)	3074 (121)
	Profile Height		mm (in)	25.4 (1.0)	25.4 (1.0)	22.34 (.880)
	Adjustment	Deflection	mm (in)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)
		Force ③	kg (lbf)	7.3 (16)	7.3 (16)	7.3 (16)
Suspension Type		Track		SC-10 III	SC-10 III	SC-10 III
		Ski		ADSA	ADSA	ADSA
Length			mm (in)	2801 (110)	2801 (110)	2725 (107)
Width			mm (in)	1217 (48)	1217 (48)	1329 (52)
Height			mm (in)	1085 (43)	1085 (43)	1130 (44)
Ski Stance (carbide to carbide)			mm (in)	1195 (47)	1195 (47)	1195 (47)
Toe-out and Camber			mm (in) degree	0 (0) 0	0 (0) 0	0 (0) 0
Mass (dry)			kg (lb)	215 (472)	215 (472)	215 (472)
Ground Contact Area			cm^2 (in^2)	6836 (1060)	6836 (1060)	6836 (1060)
Ground Contact Pressure			kPa (PSI)	3.09 (.448)	3.09 (.448)	3.09 (.448)
Frame Material				Aluminum	Aluminum	Aluminum
Bottom Pan Material				Impact Copolymer	Impact Copolymer	Impact Copolymer
Hood Material				RRIM Polyurethane	RRIM Polyurethane	RRIM Polyurethane
Battery			V/A•h	N.A.	N.A.	N.A.
Headlight			W	H4 60/55	H4 60/55	H4 60/55
Taillight and Stoplight			W	8/27	8/27	8/27
Tachometer and Speedometer Bulbs			W	3	3	3
Fuel and Temperature Gauge Bulbs			W	N.A.	N.A.	N.A.
Fuse	Starter Solenoid		A	N.A.	N.A.	N.A.
	Fuel Level Sensor		A	N.A.	N.A.	N.A.
Fuel Tank			L (U.S. gal)	37.3 (9.9)	37.3 (9.9)	37.3 (9.9)
Chaincase/Gearbox			mL (U.S. oz)	250 (8.5)	250 (8.5)	250 (8.5)
Cooling System ④			L (U.S. oz)	3.8 (128.5)	3.8 (128.5)	3.8 (128.5)
Injection Oil Reservoir			L (U.S. oz)	3.5 (118.4)	3.5 (118.4)	3.5 (118.4)

VEHICLE MODEL				MX Z 700 R SPORT (CAN./U.S.)	MX Z 700 TRAIL (CAN./U.S.)	MX Z 700 R ADRENALINE (CAN./U.S.)
ENGINE TYPE				693	693	693
Chain Drive Ratio				25/43	25/43	25/43
Chain	Pitch		in	3/8	3/8	3/8
	Type/Links Qty/Plates Qty			Silent 76/13	Silent 76/13	Silent 76/13
Drive Pulley	Type of Drive Pulley			TRA	TRA	TRA
	Ramp Identification and Roller Pin Type			300 ⑤	300 ⑤	300 ⑤
	Calibration Screw Position or Calibration Disc Quantity			3	3	3
	Spring Color			Green/Violet	Green/Violet	Green/Violet
	Spring Length		mm (in)	133.7 (5.26)	133.7 (5.26)	133.7 (5.26)
	Clutch Engagement		± 100 RPM	3800	3800	3800
Driven Pulley	Type			HPV 27	FORMULA	HPV 27
	Spring Preload		± 0.7 kg (± 1.5 lb)	N.A.	8 (17.6)	0 (0)
	Cam Angle		Degree	50/47	48/44	50/47
Pulley Distance	Z		± 0.5 mm (± .020 in)	16.5 (.650)	16.5 (.650)	16.5 (.650)
Offset	X		± 0.5 mm (± .020 in)	35.5 (1.398)	35.5 (1.398)	35.5 (1.398)
	Y – X	MIN. – MAX.	mm (in)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)
Drive Belt Part Number (P/N)				417 300 127	417 300 127	417 300 127
Drive Belt Width (new) ①			mm (in)	36.4 (1.431)	36.4 (1.431)	36.4 (1.431)
Drive Belt Adjustment		Deflection	± 5 mm (± .197 in)	32 (1.260)	32 (1.260)	32 (1.260)
		Force ②	kg (lbf)	11.3 (25)	11.3 (25)	11.3 (25)
Track	Width		mm (in)	381 (15.0)	381 (15.0)	381 (15.0)
	Length		mm (in)	3074 (121)	3074 (121)	3074 (121)
	Profile Height		mm (in)	22.34 (.880)	22.3 (.880)	25.4 (1.0)
	Adjustment	Deflection	mm (in)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)
		Force ③	kg (lbf)	7.3 (16)	7.3 (16)	7.3 (16)
Suspension Type		Track		SC-10 III	SC-10 III	SC-10 II 136
		Ski		ADSA	ADSA	ADSA
Length			mm (in)	2725 (107)	2725 (107)	2725 (107)
Width			mm (in)	1329 (52)	1213 (48)	1329 (52)
Height			mm (in)	1130 (44)	1130 (44)	1130 (44)
Ski Stance (carbide to carbide)			mm (in)	1195 (47)	1080 (42.5)	1195 (47)
Toe-out and Camber			mm (in) degree	0 (0) 0	0 (0) 0	0 (0) 0
Mass (dry)			kg (lb)	215 (472)	215 (472)	215 (472)
Ground Contact Area			cm^2 (in^2)	6836 (1060)	6671 (1034)	6836 (1060)
Ground Contact Pressure			kPa (PSI)	3.09 (.448)	3.16 (.458)	3.09 (.448)
Frame Material				Aluminum	Aluminum	Aluminum
Bottom Pan Material				Impact Copolymer	Impact Copolymer	Impact Copolymer
Hood Material				RRIM Polyurethane	RRIM Polyurethane	RRIM Polyurethane
Battery			V/A•h	N.A.	N.A.	N.A.
Headlight			W	H4 60/55	H4 60/55	H4 60/55
Taillight and Stoplight			W	8/27	8/27	8/27
Tachometer and Speedometer Bulbs			W	3	3	3
Fuel and Temperature Gauge Bulbs			W	N.A.	N.A.	N.A.
Fuse	Starter Solenoid		A	N.A.	N.A.	N.A.
	Fuel Level Sensor		A	N.A.	N.A.	N.A.
Fuel Tank			L (U.S. gal)	37.3 (9.9)	37.3 (9.9)	37.3 (9.9)
Chaincase/Gearbox			mL (U.S. oz)	250 (8.5)	250 (8.5)	250 (8.5)
Cooling System ④			L (U.S. oz)	3.8 (128.5)	3.8 (128.5)	3.8 (128.5)
Injection Oil Reservoir			L (U.S. oz)	3.5 (118.4)	3.5 (118.4)	3.5 (118.4)

VEHICLE MODEL				MX Z 700 R RENEGADE (CAN./U.S.)	MX Z 700 X (CAN./U.S.)	MX Z 700 R X (CAN./U.S.)
ENGINE TYPE				693	693	693
Chain Drive Ratio				23/43	25/43	25/43
Chain	Pitch		in	3/8	3/8	3/8
	Type/Links Qty/Plates Qty			Silent 74/13	Silent 76/13	Silent 76/13
Drive Pulley	Type of Drive Pulley			TRA	TRA	TRA
	Ramp Identification and Roller Pin Type			299 ⑤	300 ⑤	300 ⑤
	Calibration Screw Position or Calibration Disc Quantity			3	3	3
	Spring Color			Violet/Yellow	Green/Violet	Green/Violet
	Spring Length		mm (in)	157.9 (6.22)	133.7 (5.26)	133.7 (5.26)
	Clutch Engagement		± 100 RPM	3800	3800	3800
Driven Pulley	Type			HPV 27	FORMULA	HPV27
	Spring Preload		± 0.7 kg (± 1.5 lb)	0 (0)	8.0 (17.64)	N.A.
	Cam Angle		Degree	47	48/44	50/47
Pulley Distance	Z		± 0.5 mm (± .020 in)	16.5 (.650)	16.5 (.650)	16.5 (.650)
Offset	X		± 0.5 mm (± .020 in)	35.5 (1.398)	35.5 (1.398)	35.5 (1.398)
	Y – X	MIN. – MAX.	mm (in)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)
Drive Belt Part Number (P/N)				417 300 127	417 300 127	417 300 127
Drive Belt Width (new) ①			mm (in)	36.4 (1.431)	36.3 (1.431)	36.3 (1.431)
Drive Belt Adjustment		Deflection	± 5 mm (± .197 in)	32 (1.260)	32 (1.260)	32 (1.260)
		Force ②	kg (lbf)	11.3 (25)	11.3 (25)	11.3 (25)
Track	Width		mm (in)	381 (15.0)	381 (15.0)	381 (15.0)
	Length		mm (in)	3455 (136)	3074 (121)	3074 (121)
	Profile Height		mm (in)	31.8 (1.25)	25.4 (1.0)	25.4 (1.0)
	Adjustment	Deflection	mm (in)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)
		Force ③	kg (lbf)	7.3 (16)	7.3 (16)	7.3 (16)
Suspension Type		Track		SC-10 II 136	SC-10 III	SC-10 III
		Ski		ADSA	ADSA	ADSA
Length			mm (in)	3005 (118)	2801 (110)	2801 (110)
Width			mm (in)	1172 (46)	1217 (48)	1217 (48)
Height			mm (in)	1136 (45)	1085 (43)	1085 (43)
Ski Stance (carbide to carbide)			mm (in)	1156 or 1192 (45.5 or 47)	1195 (47)	1195 (47)
Toe-out and Camber			mm (in) degree	0 (0) 0	0 (0) 0	0 (0) 0
Mass (dry)			kg (lb)	221 (487)	215 (472)	215 (472)
Ground Contact Area			cm^2 (in^2)	7522 (1166)	6836 (1060)	6836 (1060)
Ground Contact Pressure			kPa (PSI)	2.88 (.418)	3.09 (.448)	3.09 (.448)
Frame Material				Aluminum	Aluminum	Aluminum
Bottom Pan Material				Impact Copolymer	Impact Copolymer	Impact Copolymer
Hood Material				RRIM Polyurethane	RRIM Polyurethane	RRIM Polyurethane
Battery			V/A•h	N.A.	N.A.	N.A.
Headlight			W	H4 60/55	H4 60/55	H4 60/55
Taillight and Stoplight			W	8/27	8/27	8/27
Tachometer and Speedometer Bulbs			W	3	3	3
Fuel and Temperature Gauge Bulbs			W	N.A.	N.A.	N.A.
Fuse	Starter Solenoid		A	N.A.	N.A.	N.A.
	Fuel Level Sensor		A	N.A.	N.A.	N.A.
Fuel Tank			L (U.S. gal)	37.3 (9.9)	37.3 (9.9)	37.3 (9.9)
Chaincase/Gearbox			mL (U.S. oz)	250 (8.5)	250 (8.5)	250 (8.5)
Cooling System ④			L (U.S. oz)	4 (135.3)	3.8 (128.5)	3.8 (128.5)
Injection Oil Reservoir			L (U.S. oz)	3.5 (118.4)	3.5 (118.4)	3.5 (118.4)

VEHICLE MODEL				MX Z 800 SPORT (CAN./U.S.)	MX Z 800 R SPORT (CAN./U.S.)	MX Z 800 TRAIL (CAN./U.S.)
ENGINE TYPE				**793**	**793**	**793**
Chain Drive Ratio				26/43	26/43	26/43
Chain	Pitch		in	3/8	3/8	3/8
	Type/Links Qty/Plates Qty			Silent 76/13	Silent 76/13	Silent 76/13
Drive Pulley	Type of Drive Pulley			TRA	TRA	TRA
	Ramp Identification and Roller Pin Type			301 ⑤	301 ⑤	301 ⑤
	Calibration Screw Position or Calibration Disc Quantity			3	3	3
	Spring Color			Violet/Yellow	Violet/Yellow	Violet/Yellow
	Spring Length		mm (in)	157.9 (6.22)	157.9 (6.22)	157.9 (6.22)
	Clutch Engagement		± 100 RPM	3800	3800	3800
Driven Pulley	Type			HPV 27	HPV 27	HPV 27
	Spring Preload		± 0.7 kg (± 1.5 lb)	N.A.	N.A.	N.A.
	Cam Angle		Degree	47/44	47/44	47/44
Pulley Distance	Z		± 0.5 mm (± .020 in)	16.5 (.650)	16.5 (.650)	16.5 (.650)
Offset	X		± 0.5 mm (± .020 in)	35.5 (1.398)	35.5 (1.398)	35.5 (1.398)
	Y – X	MIN. – MAX.	mm (in)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)
Drive Belt Part Number (P/N)				417 300 127	417 300 127	417 300 127
Drive Belt Width (new) ①			mm (in)	36.4 (1.431)	36.4 (1.431)	36.4 (1.431)
Drive Belt Adjustment		Deflection	± 5 mm (± .197 in)	32 (1.260)	32 (1.260)	32 (1.260)
		Force ②	kg (lbf)	11.3 (25)	11.3 (25)	11.3 (25)
Track	Width		mm (in)	381 (15.0)	381 (15.0)	381 (15.0)
	Length		mm (in)	3074 (121)	3074 (121)	3074 (121)
	Profile Height		mm (in)	25.4 (1.0)	25.4 (1.0)	25.4 (1.0)
	Adjustment	Deflection	mm (in)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)
		Force ③	kg (lbf)	7.3 (16)	7.3 (16)	7.3 (16)
Suspension Type		Track		SC-10 III	SC-10 III	SC-10 III
		Ski		ADSA	ADSA	ADSA
Length			mm (in)	2725 (107)	2725 (107)	2725 (107)
Width			mm (in)	1218 (48)	1218 (48)	1213 (48)
Height			mm (in)	1130 (44)	1130 (44)	1130 (44)
Ski Stance (carbide to carbide)			mm (in)	1195 (47)	1195 (47)	1080 (43)
Toe-out and Camber			mm (in) degree	0 (0) 0	0 (0) 0	0 (0) 0
Mass (dry)			kg (lb)	215 (474)	215 (474)	215 (474)
Ground Contact Area			cm^2 (in^2)	6836 (1060)	6836 (1060)	6670 (1034)
Ground Contact Pressure			kPa (PSI)	3.09 (.448)	3.09 (.448)	3.16 (.458)
Frame Material				Aluminum	Aluminum	Aluminum
Bottom Pan Material				Impact Copolymer	Impact Copolymer	Impact Copolymer
Hood Material				RRIM Polyurethane	RRIM Polyurethane	RRIM Polyurethane
Battery			V/A•h	N.A.	N.A.	N.A.
Headlight			W	H4 60/55	H4 60/55	H4 60/55
Taillight and Stoplight			W	8/27	8/27	8/27
Tachometer and Speedometer Bulbs			W	3	3	3
Fuel and Temperature Gauge Bulbs			W	N.A.	N.A.	N.A.
Fuse	Starter Solenoid		A	N.A.	N.A.	N.A.
	Fuel Level Sensor		A	N.A.	N.A.	N.A.
Fuel Tank			L (U.S. gal)	37.3 (9.9)	37.3 (9.9)	37.3 (9.9)
Chaincase/Gearbox			mL (U.S. oz)	250 (8.5)	250 (8.5)	250 (8.5)
Cooling System ④			L (U.S. oz)	3.8 (128.5)	3.8 (128.5)	3.8 (128.5)
Injection Oil Reservoir			L (U.S. oz)	3.5 (118.4)	3.5 (118.4)	3.5 (118.4)

VEHICLE MODEL				MX Z 800 R ADRENALINE (CAN./U.S.)	MX Z 800 R RENEGADE (CAN./U.S.)	MX Z 800 X (CAN./U.S.)
ENGINE TYPE				793	793	793
Chain Drive Ratio				26/43	23/43	26/43
Chain	Pitch		in	3/8	3/8	3/8
	Type/Links Qty/Plates Qty			Silent 76/13	Silent 74/13	Silent 76/13
Drive Pulley	Type of Drive Pulley			TRA	TRA	TRA
	Ramp Identification and Roller Pin Type			301 ⑤	301 ⑤	301 ⑤
	Calibration Screw Position or Calibration Disc Quantity			3	3	3
	Spring Color			Violet/Yellow	Violet/Yellow	Violet/Yellow
	Spring Length		mm (in)	157.9 (6.22)	157.9 (6.22)	157.9 (6.22)
	Clutch Engagement		± 100 RPM	3800	3800	3800
Driven Pulley	Type			HPV 27	HPV27	HPV27
	Spring Preload		± 0.7 kg (± 1.5 lb)	N.A.	N.A.	N.A.
	Cam Angle		Degree	47/44	47/44	47/44
Pulley Distance	Z		± 0.5 mm (± .020 in)	16.5 (.650)	16.5 (.650)	16.5 (.650)
Offset	X		± 0.5 mm (± .020 in)	35.5 (1.398)	35.5 (1.398)	35.5 (1.398)
	Y – X	MIN. – MAX.	mm (in)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)
Drive Belt Part Number (P/N)				417 300 127	417 300 127	417 300 127
Drive Belt Width (new) ①			mm (in)	36.4 (1.431)	36.35 (1.431)	36.4 (1.431)
Drive Belt Adjustment		Deflection	± 5 mm (± .197 in)	32 (1.260)	32 (1.260)	32 (1.260)
		Force ②	kg (lbf)	11.3 (25)	11.3 (25)	11.3 (25)
Track	Width		mm (in)	381 (15.0)	381 (15.0)	381 (15.0)
	Length		mm (in)	3074 (121)	3455 (136)	3074 (121)
	Profile Height		mm (in)	25.4 (1.0)	31.8 (1.3)	25.4 (1.0)
	Adjustment	Deflection	mm (in)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)
		Force ③	kg (lbf)	7.3 (16)	7.3 (16)	7.3 (16)
Suspension Type		Track		SC-10 III	SC-10 II 136	SC-10 III
		Ski		ADSA	ADSA	ADSA
Length			mm (in)	2725 (107)	3005 (118.3)	2801 (110)
Width			mm (in)	1329 (52)	1172 (46.1)	1217 (48)
Height			mm (in)	1086 (43)	1136 (44.7)	1085 (43)
Ski Stance (carbide to carbide)			mm (in)	1195 (47)	1092 or 1156 (43 or 45.5)	1195 (47)
Toe-out and Camber			mm (in) degree	0 (0) 0	0 (0) 0	0 (0) 0
Mass (dry)			kg (lb)	215 (474)	222 (489)	215 (472)
Ground Contact Area			cm^2 (in^2)	6836 (1060)	7522 (1166)	6836 (1060)
Ground Contact Pressure			kPa (PSI)	3.09 (.448)	2.90 (.421)	3.09 (.448)
Frame Material				Aluminum	Aluminum	Aluminum
Bottom Pan Material				Impact Copolymer	Impact Copolymer	Impact Copolymer
Hood Material				RRIM Polyurethane	RRIM Polyurethane	RRIM Polyurethane
Battery			V/A•h	N.A.	N.A.	N.A.
Headlight			W	H4 60/55	H4 60/55	H4 60/55
Taillight and Stoplight			W	8/27	8/27	8/27
Tachometer and Speedometer Bulbs			W	3	3	3
Fuel and Temperature Gauge Bulbs			W	N.A.	N.A.	N.A.
Fuse	Starter Solenoid		A	N.A.	N.A.	N.A.
	Fuel Level Sensor		A	N.A.	N.A.	N.A.
Fuel Tank			L (U.S. gal)	37.3 (9.9)	37.3 (9.9)	37.3 (9.9)
Chaincase/Gearbox			mL (U.S. oz)	250 (8.5)	250 (8.5)	250 (8.5)
Cooling System ④			L (U.S. oz)	3.8 (128.5)	4.0 (135.3)	3.8 (128.5)
Injection Oil Reservoir			L (U.S. oz)	3.5 (118.4)	3.5 (118.4)	3.5 (118.4)

VEHICLE MODEL				MX Z 800 R X (CAN./U.S.)	SUMMIT 600 SPORT (CAN./U.S.)	SUMMIT 600 R SPORT (CAN./U.S.)
ENGINE TYPE				793	593	593
Chain Drive Ratio				26/43	19/43	19/43
Chain	Pitch		in	3/8	3/8	3/8
	Type/Links Qty/Plates Qty			Silent 76/13	Silent 72/13	Silent 72/13
Drive Pulley	Type of Drive Pulley			TRA	TRA	TRA
	Ramp Identification and Roller Pin Type			301 ⑤	300 ⑦	299 ⑦
	Calibration Screw Position or Calibration Disc Quantity			3	1	1
	Spring Color			Violet/Yellow	Violet/Green	Violet/Blue
	Spring Length		mm (in)	157.9 (6.22)	133.5 (5.26)	114.6 (4.51)
	Clutch Engagement		± 100 RPM	3800	4000	4000
Driven Pulley	Type			HPV27	FORMULA	HPV 27
	Spring Preload		± 0.7 kg (± 1.5 lb)	N.A.	7.5 (16.54)	N.A.
	Cam Angle		Degree	47/44	44	47/44
Pulley Distance	Z		± 0.5 mm (± .020 in)	16.5 (.650)	16.5 (.650)	16.5 (.650)
Offset	X		± 0.5 mm (± .020 in)	35.5 (1.398)	35.5 (1.398)	35.5 (1.398)
	Y – X	MIN. – MAX.	mm (in)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)
Drive Belt Part Number (P/N)				417 300 127	417 300 127	417 300 127
Drive Belt Width (new) ①			mm (in)	36.4 (1.431)	36.4 (1.431)	36.4 (1.431)
Drive Belt Adjustment		Deflection	± 5 mm (± .197 in)	32 (1.260)	32 (1.260)	32 (1.260)
		Force ②	kg (lbf)	11.3 (25)	11.3 (25)	11.3 (25)
Track	Width		mm (in)	381 (15.0)	381 (15.0)	381 (15.0)
	Length		mm (in)	3074 (121)	3648 (144)	3648 (144)
	Profile Height		mm (in)	25.4(1.0)	50.8 (2.0)	50.8 (2.0)
	Adjustment	Deflection	mm (in)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)
		Force ③	kg (lbf)	7.3 (16)	7.3 (16)	7.3 (16)
Suspension Type		Track		SC-10 III	SC-10 144	SC-10 144
		Ski		ADSA	ADSA	ADSA
Length			mm (in)	2801 (110)	2947 (116)	2947 (116)
Width			mm (in)	1217 (48)	1139 (45)	1139 (45)
Height			mm (in)	1085 (43)	1130 (44)	1130 (44)
Ski Stance (carbide to carbide)			mm (in)	1195 (47)	1025 or 1080 (40 or 43)	1025 or 1080 (40 or 43)
Toe-out and Camber			mm (in) degree	0 (0) 0	0 (0) 0	0 (0) 0
Mass (dry)			kg (lb)	215 (472)	222 (489)	222 (489)
Ground Contact Area			cm^2 (in^2)	6836 (1060)	8684 (1346)	8684 (1346)
Ground Contact Pressure			kPa (PSI)	3.09 (.448)	2.51 (.364)	2.51 (.364)
Frame Material				Aluminum	Aluminum	Aluminum
Bottom Pan Material				Impact Copolymer	Impact Copolymer	Impact Copolymer
Hood Material				RRIM Polyurethane	RRIM Polyurethane	RRIM Polyurethane
Battery			V/A•h	N.A.	N.A.	N.A.
Headlight			W	H4 60/55	H4 60/55	H4 60/55
Taillight and Stoplight			W	8/27	8/27	8/27
Tachometer and Speedometer Bulbs			W	3	3	3
Fuel and Temperature Gauge Bulbs			W	N.A.	N.A.	N.A.
Fuse	Starter Solenoid		A	N.A.	N.A.	N.A.
	Fuel Level Sensor		A	N.A.	N.A.	N.A.
Fuel Tank			L (U.S. gal)	37.3 (9.9)	37.3 (9.9)	37.3 (9.9)
Chaincase/Gearbox			mL (U.S. oz)	250 (8.5)	250 (8.5)	250 (8.5)
Cooling System ④			L (U.S. oz)	3.8 (128.5)	4 (135.3)	4 (135.3)
Injection Oil Reservoir			L (U.S. oz)	3.5 (118.4)	3.5 (118.4)	3.5 (118.4)

VEHICLE MODEL				SUMMIT 700 SPORT (CAN./U.S.)	SUMMIT 700 R SPORT (CAN./U.S.)	SUMMIT 800 SPORT (CAN./U.S.)
ENGINE TYPE				793	793	793
Chain Drive Ratio				21/43	21/43	21/43
Chain	Pitch		in	3/8	3/8	3/8
	Type/Links Qty/Plates Qty			Silent 74/13	Silent 74/13	Silent 74/13
Drive Pulley	Type of Drive Pulley			TRA	TRA	TRA
	Ramp Identification and Roller Pin Type			299 ⑦	300 ⑦	300 ⑦
	Calibration Screw Position or Calibration Disc Quantity			1	1	1
	Spring Color			Violet/Yellow	Violet/Yellow	Blue/Orange
	Spring Length		mm (in)	157.9 (6.22)	157.9 (6.22)	135.5 (5.36)
	Clutch Engagement		± 100 RPM	4100	4100	4000
Driven Pulley	Type			FORMULA	HPV27	HPV 27
	Spring Preload		± 0.7 kg (± 1.5 lb)	7.5 (16.5)	N.A.	N.A.
	Cam Angle		Degree	47	44	44
Pulley Distance	Z		± 0.5 mm (± .020 in)	16.5 (.650)	16.5 (.650)	16.5 (.650)
Offset	X		± 0.5 mm (± .020 in)	35.5 (1.398)	35.5 (1.398)	35.5 (1.398)
	Y – X	MIN. – MAX.	mm (in)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)
Drive Belt Part Number (P/N)				417 300 127	417 300 127	417 300 127
Drive Belt Width (new) ①			mm (in)	36.35 (1.431)	36.35 (1.431)	36.4 (1.431)
Drive Belt Adjustment		Deflection	± 5 mm (± .197 in)	32 (1.260)	32 (1.260)	32 (1.260)
		Force ②	kg (lbf)	11.3 (25)	11.3 (25)	11.3 (25)
Track	Width		mm (in)	381 (15.0)	381 (15.0)	381 (15.0)
	Length		mm (in)	3648 (144)	3648 (144)	3648 (144)
	Profile Height		mm (in)	50.8 (2.0)	50.8 (2.0)	50.8 (2.0)
	Adjustment	Deflection	mm (in)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)
		Force ③	kg (lbf)	7.3 (16)	7.3 (16)	7.3 (16)
Suspension Type		Track		SC-10 144	SC-10 144	SC-10 144
		Ski		ADSA	ADSA	ADSA
Length			mm (in)	2947 (116.0)	2947 (116.0)	3134 (123)
Width			mm (in)	1310 (51.6)	1310 (51.6)	1310 (52)
Height			mm (in)	1130 (44.5)	1130 (44.5)	1130 (44)
Ski Stance (carbide to carbide)			mm (in)	1139 (44.8)	1139 (44.8)	1025 or 1080 (40.3 or 42.5)
Toe-out and Camber			mm (in) degree	0 (0) 0	0 (0) 0	0 (0) 0
Mass (dry)			kg (lb)	224 (492)	224 (492)	225 (494)
Ground Contact Area			cm^2 (in^2)	8650 (1341)	7507 (1164)	8684 (1346)
Ground Contact Pressure			kPa (PSI)	2.54 (.368)	2.93 (.425)	2.54 (.368)
Frame Material				Aluminum	Aluminum	Aluminum
Bottom Pan Material				Impact Copolymer	Impact Copolymer	Impact Copolymer
Hood Material				RRIM Polyurethane	RRIM Polyurethane	RRIM Polyurethane
Battery			V/A•h	N.A.	N.A.	N.A.
Headlight			W	H4 60/55	H4 60/55	H4 60/55
Taillight and Stoplight			W	8/27	8/27	8/27
Tachometer and Speedometer Bulbs			W	3	3	3
Fuel and Temperature Gauge Bulbs			W	N.A.	N.A.	N.A.
Fuse	Starter Solenoid		A	N.A.	N.A.	N.A.
	Fuel Level Sensor		A	N.A.	N.A.	N.A.
Fuel Tank			L (U.S. gal)	37.3 (9.9)	37.3 (9.9)	37.3 (9.9)
Chaincase/Gearbox			mL (U.S. oz)	250 (8.5)	250 (8.5)	250 (8.5)
Cooling System ④			L (U.S. oz)	4.0 (135.3)	4.0 (135.3)	4 (135.3)
Injection Oil Reservoir			L (U.S. oz)	3.5 (118.4)	3.5 (118.4)	3.5 (118.4)

VEHICLE MODEL				SUMMIT 800 R SPORT (CAN./U.S.)	SUMMIT 800 X (CAN./U.S.)	SUMMIT 800 R X (CAN./U.S.)
ENGINE TYPE				**793**	**793**	**793**
Chain Drive Ratio				21/43	21/43	21/43
Chain	Pitch		in	3/8	3/8	3/8
	Type/Links Qty/Plates Qty			Silent 74/13	Silent 74/13	Silent 74/13
Drive Pulley	Type of Drive Pulley			TRA	TRA	TRA
	Ramp Identification and Roller Pin Type			300 ⑦	300 ⑦	300 ⑦
	Calibration Screw Position or Calibration Disc Quantity			1	1	1
	Spring Color			Blue/Orange	Blue/Orange	Blue/Orange
	Spring Length		mm (in)	135.5 (5.36)	135.5 (5.36)	135.5 (5.36)
	Clutch Engagement		± 100 RPM	4000	4000	4000
Driven Pulley	Type			HPV 27	HPV 27	HPV 27
	Spring Preload		± 0.7 kg (± 1.5 lb)	N.A.	N.A.	N.A.
	Cam Angle		Degree	44	44	44
Pulley Distance	Z		± 0.5 mm (± .020 in)	16.5 (.650)	16.5 (.650)	16.5 (.650)
Offset	X		± 0.5 mm (± .020 in)	35.5 (1.398)	35.5 (1.398)	35.5 (1.398)
	Y – X	MIN. – MAX.	mm (in)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)
Drive Belt Part Number (P/N)				417 300 127	417 300 127	417 300 127
Drive Belt Width (new) ①			mm (in)	36.4 (1.431)	36.4 (1.431)	36.4 (1.431)
Drive Belt Adjustment		Deflection	± 5 mm (± .197 in)	32 (1.260)	32 (1.260)	32 (1.260)
		Force ②	kg (lbf)	11.3 (25)	11.3 (25)	11.3 (25)
Track	Width		mm (in)	381 (15.0)	381 (15.0)	381 (15.0)
	Length		mm (in)	3648 (144)	3648 (144)	3648 (144)
	Profile Height		mm (in)	50.8 (2.0)	50.8 (2.0)	50.8 (2.0)
	Adjustment	Deflection	mm (in)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)
		Force ③	kg (lbf)	7.3 (16)	7.3 (16)	7.3 (16)
Suspension Type		Track		SC-10 144	SC-10 144	SC-10 144
		Ski		ADSA	ADSA	ADSA
Length			mm (in)	3134 (123)	3134 (123)	3134 (123)
Width			mm (in)	1310 (52)	1310 (52)	1310 (52)
Height			mm (in)	1130 (44)	1130 (44)	1130 (44)
Ski Stance (carbide to carbide)			mm (in)	1025 or 1080 (40.3 or 42.5)	1025 or 1080 (40.3 or 42.5)	1025 or 1080 (40.3 or 42.5)
Toe-out and Camber			mm (in) degree	0 (0) 0	0 (0) 0	0 (0) 0
Mass (dry)			kg (lb)	225 (494)	225 (494)	225 (494)
Ground Contact Area			cm^2 (in^2)	8684 (1346)	8684 (1346)	8684 (1346)
Ground Contact Pressure			kPa (PSI)	2.54 (.368)	2.54 (.368)	2.54 (.368)
Frame Material				Aluminum	Aluminum	Aluminum
Bottom Pan Material				Impact Copolymer	Impact Copolymer	Impact Copolymer
Hood Material				RRIM Polyurethane	RRIM Polyurethane	RRIM Polyurethane
Battery			V/A•h	N.A.	N.A.	N.A.
Headlight			W	H4 60/55	H4 60/55	H4 60/55
Taillight and Stoplight			W	8/27	8/27	8/27
Tachometer and Speedometer Bulbs			W	3	3	3
Fuel and Temperature Gauge Bulbs			W	N.A.	N.A.	N.A.
Fuse	Starter Solenoid		A	N.A.	N.A.	N.A.
	Fuel Level Sensor		A	N.A.	N.A.	N.A.
Fuel Tank			L (U.S. gal)	37.3 (9.9)	37.3 (9.9)	37.3 (9.9)
Chaincase/Gearbox			mL (U.S. oz)	250 (8.5)	250 (8.5)	250 (8.5)
Cooling System ④			L (U.S. oz)	4 (135.3)	4 (135.3)	4 (135.3)
Injection Oil Reservoir			L (U.S. oz)	3.5 (118.4)	3.5 (118.4)	3.5 (118.4)

VEHICLE MODEL				SUMMIT 800 HIGHMARK (CAN./U.S.)	SUMMIT 800 R HIGHMARK (CAN./U.S.)	SUMMIT 800 HIGHMARK X (CAN./U.S.)
ENGINE TYPE				**793**	**793**	**793**
Chain Drive Ratio				19/43	19/43	19/43
Chain	Pitch		in	3/8	3/8	3/8
	Type/Links Qty/Plates Qty			Silent 72/13	Silent 72/13	Silent 72/13
Drive Pulley	Type of Drive Pulley			TRA	TRA	TRA
	Ramp Identification and Roller Pin Type			300 ⑦	300 ⑦	300 ⑦
	Calibration Screw Position or Calibration Disc Quantity			1	1	1
	Spring Color			Blue/Orange	Blue/Orange	Blue/Orange
	Spring Length		mm (in)	135.5 (5.36)	135.5 (5.36)	135.5 (5.36)
	Clutch Engagement		± 100 RPM	4000	4000	4000
Driven Pulley	Type			HPV 27	HPV 27	HPV 27
	Spring Preload		± 0.7 kg (± 1.5 lb)	N.A.	N.A.	N.A.
	Cam Angle		Degree	44	44	44
Pulley Distance	Z		± 0.5 mm (± .020 in)	16.5 (.650)	16.5 (.650)	16.5 (.650)
Offset	X		± 0.5 mm (± .020 in)	35.5 (1.398)	35.5 (1.398)	35.5 (1.398)
	Y – X	MIN. – MAX.	mm (in)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)	1.0 – 2.0 (.040 – .080)
Drive Belt Part Number (P/N)				417 300 127	417 300 127	417 300 127
Drive Belt Width (new) ①			mm (in)	36.4 (1.431)	36.4 (1.431)	36.4 (1.431)
Drive Belt Adjustment		Deflection	± 5 mm (± .197 in)	32 (1.260)	32 (1.260)	32 (1.260)
		Force ②	kg (lbf)	11.3 (25)	11.3 (25)	11.3 (25)
Track	Width		mm (in)	381 (15.0)	381 (15.0)	381 (15.0)
	Length		mm (in)	3836 (151)	3648 (144)	3836 (151)
	Profile Height		mm (in)	50.8 (2.0)	50.8 (2.0)	50.8 (2.0)
	Adjustment	Deflection	mm (in)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)	30 – 35 (1-3/16 – 1-3/8)
		Force ③	kg (lbf)	7.3 (16)	7.3 (16)	7.3 (16)
Suspension Type		Track		SC-10 151	SC-10 151	SC-10 151
		Ski		ADSA	ADSA	ADSA
Length			mm (in)	3216 (127)	3216 (127)	3216 (127)
Width			mm (in)	1139 (45)	1139 (49)	1139 (45)
Height			mm (in)	1130 (44)	1130 (44)	1130 (44)
Ski Stance (carbide to carbide)			mm (in)	1025 or 1080 (40.3 or 42.5)	1025 or 1080 (40.3 or 42.5)	1025 or 1080 (40.3 or 42.5)
Toe-out and Camber			mm (in) degree	0 (0) 0	0 (0) 0	0 (0) 0
Mass (dry)			kg (lb)	227 (499)	227 (499)	227 (499)
Ground Contact Area			cm^2 (in^2)	9141 (1417)	9141 (1417)	9141 (1417)
Ground Contact Pressure			kPa (PSI)	2.44 (.354)	2.49 (.354)	2.44 (.354)
Frame Material				Aluminum	Aluminum	Aluminum
Bottom Pan Material				Impact Copolymer	Impact Copolymer	Impact Copolymer
Hood Material				RRIM Polyurethane	RRIM Polyurethane	RRIM Polyurethane
Battery			V/A•h	N.A.	N.A.	N.A.
Headlight			W	H4 60/55	H4 60/55	H4 60/55
Taillight and Stoplight			W	8/27	8/27	8/27
Tachometer and Speedometer Bulbs			W	3	3	3
Fuel and Temperature Gauge Bulbs			W	N.A.	N.A.	N.A.
Fuse	Starter Solenoid		A	N.A.	N.A.	N.A.
	Fuel Level Sensor		A	N.A.	N.A.	N.A.
Fuel Tank			L (U.S. gal)	37.3 (9.9)	37.3 (9.9)	37.3 (9.9)
Chaincase/Gearbox			mL (U.S. oz)	250 (8.5)	250 (8.5)	250 (8.5)
Cooling System ④			L (U.S. oz)	4.3 (143.7)	4.3 (143.7)	4.3 (143.7)
Injection Oil Reservoir			L (U.S. oz)	3.5 (118.4)	3.5 (118.4)	3.5 (118.4)

VEHICLE MODEL				SUMMIT 800 R HIGHMARK X (CAN./U.S.)
ENGINE TYPE				793
Chain Drive Ratio				19/43
Chain	Pitch		in	3/8
	Type/Links Qty/Plates Qty			Silent 72/13
Drive Pulley	Type of Drive Pulley			TRA
	Ramp Identification and Roller Pin Type			300 ⑦
	Calibration Screw Position or Calibration Disc Quantity			1
	Spring Color			Blue/Orange
	Spring Length		mm (in)	135.5 (5.36)
	Clutch Engagement		± 100 RPM	4000
Driven Pulley	Type			HPV 27
	Spring Preload		± 0.7 kg (± 1.5 lb)	N.A.
	Cam Angle		Degree	44
Pulley Distance	Z		± 0.5 mm (± .020 in)	16.5 (.650)
Offset	X		± 0.5 mm (± .020 in)	35.5 (1.398)
	Y – X	MIN. – MAX.	mm (in)	1.0 – 2.0 (.040 – .080)
Drive Belt Part Number (P/N)				417 300 127
Drive Belt Width (new) ①			mm (in)	36.4 (1.431)
Drive Belt Adjustment		Deflection	± 5 mm (± .197 in)	32 (1.260)
		Force ②	kg (lbf)	11.3 (25)
Track	Width		mm (in)	381 (15.0)
	Length		mm (in)	3648 (144)
	Profile Height		mm (in)	50.8 (2.0)
	Adjustment	Deflection	mm (in)	30 – 35 (1-3/16 – 1-3/8)
		Force ③	kg (lbf)	7.3 (16)
Suspension Type		Track		SC-10 151
		Ski		ADSA
Length			mm (in)	3216 (127)
Width			mm (in)	1139 (49)
Height			mm (in)	1130 (44)
Ski Stance (carbide to carbide)			mm (in)	1025 or 1080 (40.3 or 42.5)
Toe-out and Camber			mm (in) degree	0 (0) 0
Mass (dry)			kg (lb)	227 (499)
Ground Contact Area			cm^2 (in^2)	9141 (1417)
Ground Contact Pressure			kPa (PSI)	2.49 (.354)
Frame Material				Aluminum
Bottom Pan Material				Impact Copolymer
Hood Material				RRIM Polyurethane
Battery			V/A•h	N.A.
Headlight			W	H4 60/55
Taillight and Stoplight			W	8/27
Tachometer and Speedometer Bulbs			W	3
Fuel and Temperature Gauge Bulbs			W	N.A.
Fuse	Starter Solenoid		A	N.A.
	Fuel Level Sensor		A	N.A.
Fuel Tank			L (U.S. gal)	37.3 (9.9)
Chaincase/Gearbox			mL (U.S. oz)	250 (8.5)
Cooling System ④			L (U.S. oz)	4.3 (143.7)
Injection Oil Reservoir			L (U.S. oz)	3.5 (118.4)

ENGINE LEGEND

BTDC: Before Top Dead Center

CDI: Capacitor Discharge Ignition

K: Kilo (x 1000)

ST: Semi-trapezoidal

MAG: Magneto Side

N.A.: Not Applicable

PTO: Power Take Off Side

① The maximum horsepower RPM applicable on the vehicle. It may be different under certain circumstances and BOMBARDIER INC. reserves the right to modify it without obligation.

② Crankshaft end-play is not adjustable on these models. Specification is given for verification purposes only.

③ At 3500 RPM with headlamp turned on.

④ All resistance measurements must be performed with parts at room temperature (approx. 20°C (68°F)). Temperature greatly affects resistance measurements.

⑤ Press fit type, not replaceable.

⑥ Neelde with on groove, not adjustable.

⑦ Drive pulley retaining screw: torque to 80 to 100 N•m (66 to 74 lbf•ft), install drive belt, accelerate the vehicle at low speed (maximum 30 km/h (20 MPH)) and apply the brake; repeat 5 times. Recheck the torque of 90 to 100 N•m (66 to 74 lbf•ft).

VEHICLE LEGEND

ADSA: Advanced Direct Shock Action

RRIM: Reinforced Reaction Injection Molding

TRA: Total Range Adjustable

N.A.: Not Applicable

① Minimum allowable width may not be less than 3.0 mm (1/8 in) of new drive belt.

② Force applied midway between pulleys to obtain specified tension deflection.

③ Force or downward pull applied to track to obtain specified tension deflection.

④ Coolant mixture: 50% antifreeze/50% water.

⑤ Lever with roller pin (P/N 417 004 308) (solid).

⑥ Lever with roller pin (P/N 417 004 309) (hollow).

⑦ Lever with roller pin (P/N 417 222 478) (solid).

⑧ Lever with roller pin (P/N 417 222 491) 10.3 g threaded.

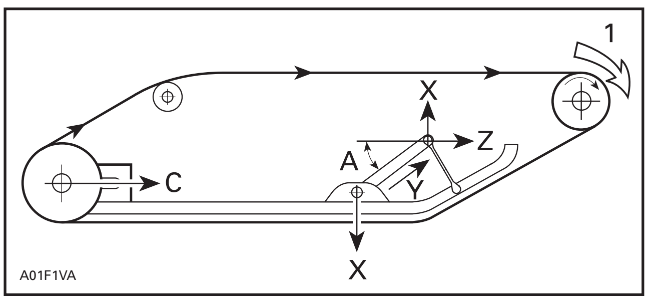
TABLE OF CONTENTS

SUSPENSION OPERATION/WEIGHT TRANSFER

The purpose of any suspension system is to isolate the rider from the terrain while still allowing for complete control of the vehicle. A snowmobile rear suspension has the added requirements of providing weight transfer and maintaining correct track tension.

Weight transfer is essentially the shifting of weight to the track for better traction during acceleration, and to the skis for positive handling during cornering.

The physics that apply to all rear suspensions are basically the same. As we apply torque from the engine to the drive axle, the torque is transferred to the track and pulls it for forward. That energy enters the suspension system at the rear axle and tries to pull it forward (force “C” in following illustration). The rear arm is a pivoting or sliding linkage that only provides vertical forces at the rear of the chassis, therefore, none of force “C” enters the chassis at the rear arm.



1. *Drive axel torque*

The front arm is mounted with a pivot to both the runners and the chassis. It is through this arm that the major reaction to the engine torque is applied. As the front arm begins to swivel from the load of force “C”, it pushes down on the front of the track (force “X” in illustration). This reduces weight on the skis and applies more weight on the track for better traction. The rest of the force “C” enters the chassis through the front arm and accelerates the vehicle (force “Z”).

If we keep force “C” constant, we can then vary the size of the vertical and horizontal forces at the front arm by varying angle “A”. As angle “A” is made smaller, force “X” decreases, and force “Z” increases. This reduces the amount of torque reaction and more weight stays on the skis. As angle “A” is increased, force “X” increases. The skis then tend to lift more during acceleration and more weight is placed on the track.

We can vary angle “A”, within limits, by adjusting the length of the limiter strap. The limiter strap is just that, a strap to limit the extension of the front of the suspension. Shortening the strap decreases angle “A” and is what we would do to set up a machine for more ski pressure. For more track pressure we would want to lengthen the strap to increase angle “A”. The limiter adjustment has the largest affect on controlling the amount of weight transfer.

NOTE: Track tension must be checked whenever a major change is made to the limiter length.

Front arm spring pressure will also affect weight transfer. A stiffer spring and/or more preload will transfer more weight to the track. A softer spring and/or less preload will keep more weight on the skis. Springs must also be selected to provide absorption to the intended size of bumps to be encountered. A soft spring will increase ski pressure but may bottom out on large bumps, while a stiff spring will provide more track pressure but may produce a harsh ride.

NOTE: In this and other Ski-Doo texts, we refer to the front arm of the rear suspension and it’s spring and shock absorber, as the center of the vehicle. The ski suspension is considered the front of the vehicle and the rear arm of the rear suspension and it’s spring(s) and shock(s) are indicated as the rear of the vehicle.

Also, think of the center arm as a pivot point. During acceleration the rear arm will want to compress and the front suspension will want to extend (possibly raising the skis off the ground). Because of this pivoting affect, the rear spring and preload will also affect weight transfer (to a lesser amount than center arm changes). A softer rear spring and/or less preload will allow more weight transfer to the track and less ski pressure, while stiffer rear springs and/or more preload will allow less weight transfer to the track and more ski pressure.

Contrary to popular belief, it is not necessary to have the skis 2 feet off the ground to achieve good weight transfer. In fact, the energy used to lift the front of the vehicle is not available to push the vehicle forward.

The main function of the rear arm is to support the weight of the vehicle and rider, yet provide usable travel to absorb bumps and jumps. The springs are chosen depending on the linkage design of the rear arm and the intended load to be applied. Stiffer springs will be used on vehicles intended to carry heavier loads and on vehicles that plan to encounter large bumps, while vehicles used for lighter loads and on smaller bumps will use softer springs.

Springs for the front suspension are chosen in a similar fashion. A softer spring will provide less ski pressure and will be used on lighter vehicles while stiffer springs will provide more ski pressure and be used on heavier vehicles.

NOTE: Shock absorber valving and the type of shock used will also affect weight transfer. Refer to the shock absorber section for details.

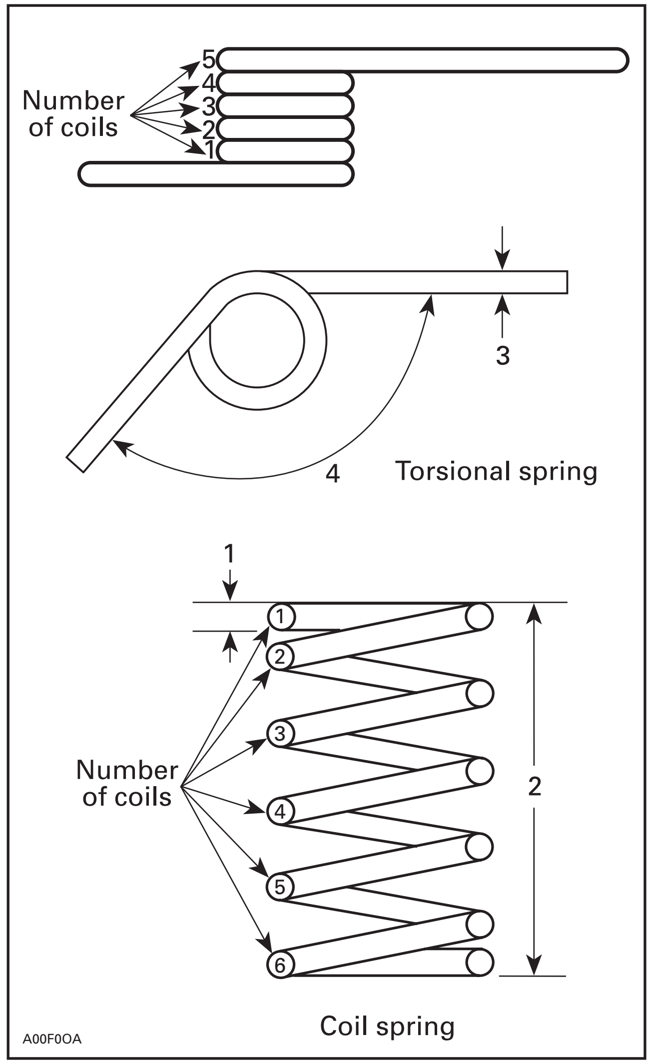
A.C.M.

The SC-10 High Performance and Cross Country Rear Suspensions incorporates the use of A.C.M. technology. Under hard acceleration, the A.C.M. linkage couples the front and rear arms moving the rails rearward, thus reducing ski lift. The A.C.M. can be used to increase and decrease weight transfer. Tightening the A.C.M. will decrease weight transfer. Loosening the A.C.M. will increase weight transfer.

SPRINGS

General

Generally, 2 types of springs are used on our suspensions. Coil springs and torsional springs. Refer to following illustration.



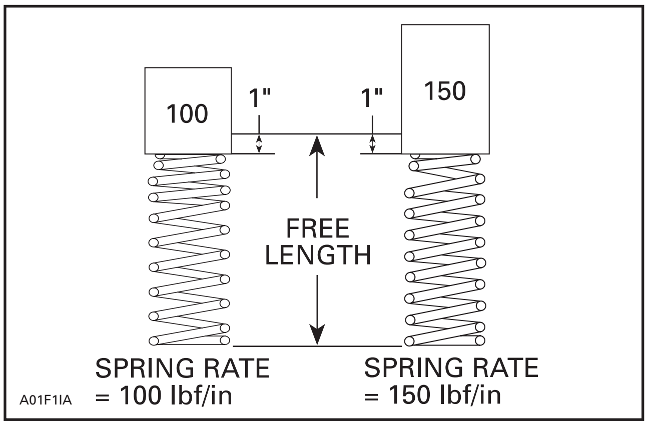
1. Wire diameter
2. Free length
3. Wire diameter
4. Opening angle

Several factors are used to determine the characteristics of a spring and they are similar for both the coil and torsional spring types. Wire diameter, material type, the number of coils and the physical shape of a spring all determine how a spring will act. Once these characteristics are built into a spring, they determine the spring rate and the free length in a coil spring or the opening angle and spring rate in a torsional spring.

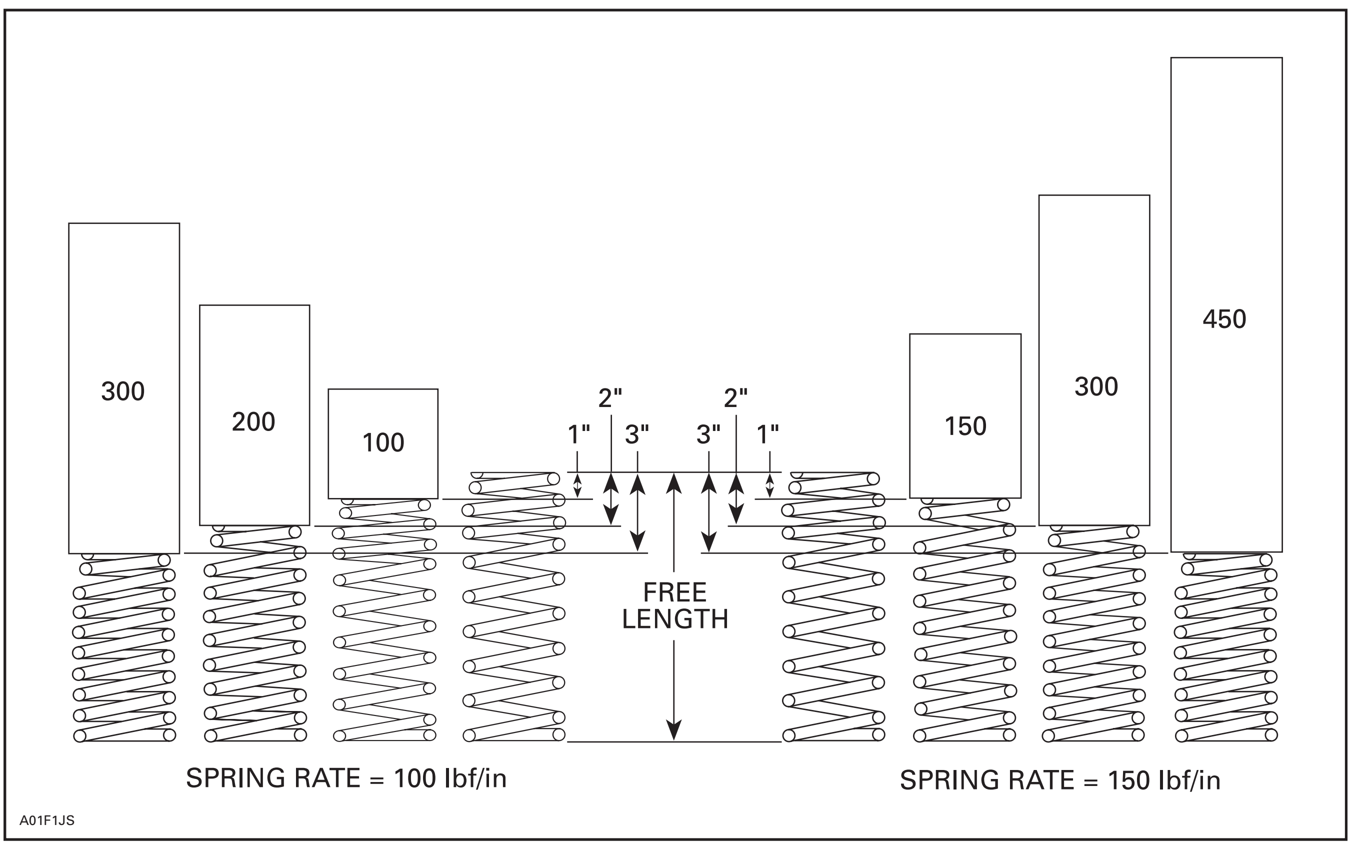
Coil Springs

The free length of a coil spring is the length with no load applied to the spring.

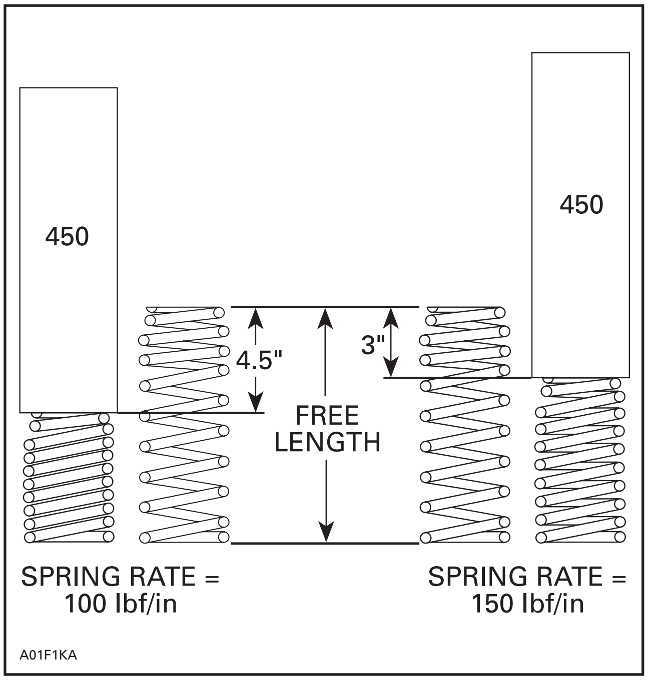
The spring rate of a coil spring is defined as the amount of force required to compress the spring one inch. If a 100 pound force compresses a spring 1 inch it is referred to as having a rate of 100 lbf/in (pounds per inch). If 150 pounds of force is required to compress a spring 1 inch then it would have a rate of 150 lbf/in (see following illustration).



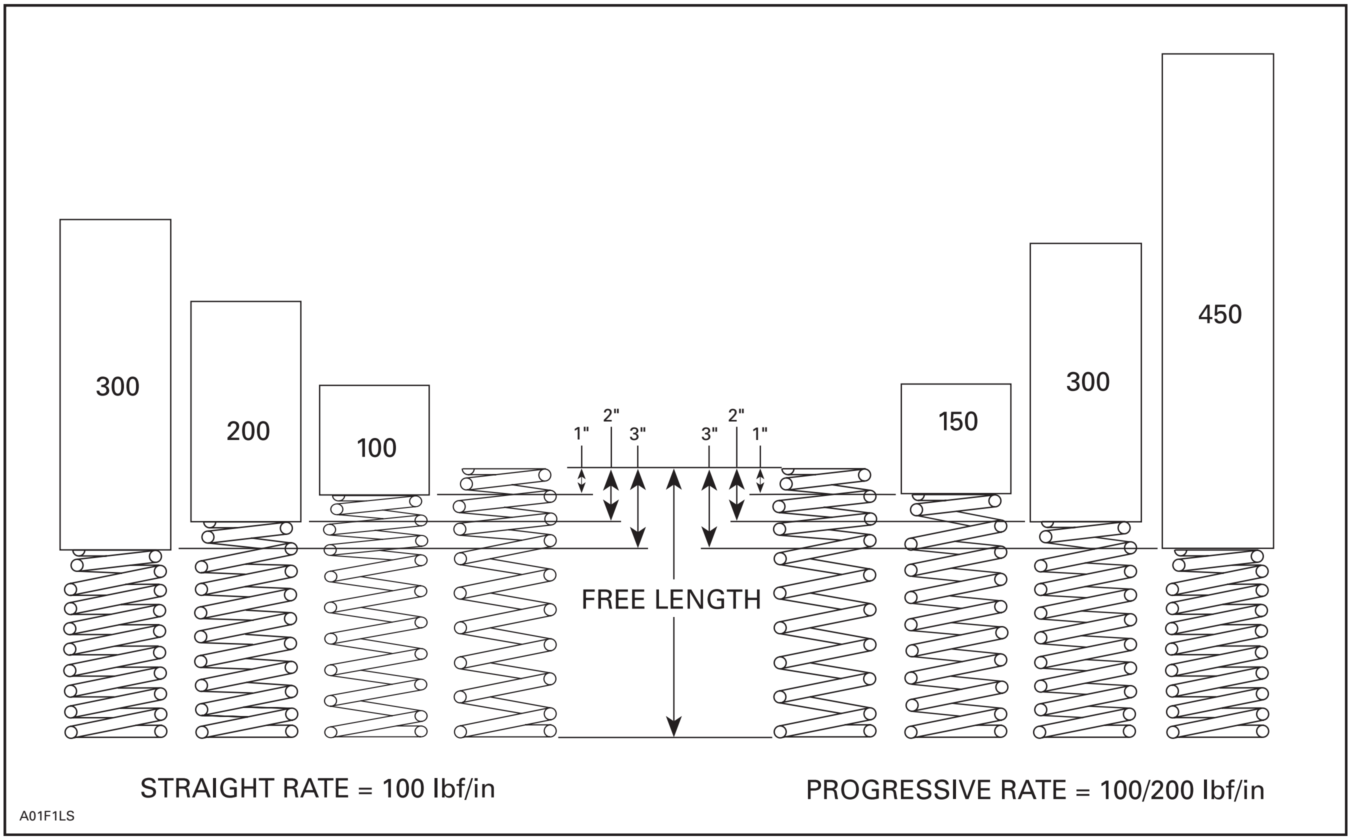
Most springs are designed as a straight rate spring. This means that the spring requires the same force to compress the last one inch of travel as the first one inch of travel. Example: A 100 lbf/in rate spring will compress one inch for every 100 pounds applied. A force of 200 pounds will compress the spring 2 inches. A 300 pound force will compress the spring 3 inches and so on. The 150 lbf/in rate spring will require 150 pounds to compress the spring each one inch. To compress this spring 3 inches it will require a force of 450 pounds (see following illustration).



In terms of your suspension, if a bump is encountered that translates into a force at the spring of 450 pounds, the 100 lbf/in spring will want to compress 4.5 inches while the 150 lbf/in spring will only compress 3 inches. If our suspension only has 4 inches of spring travel the unit with the 100 lbf/in spring will bottom out while the 150 lbf/in unit still has 1 inch of travel remaining (see following illustration).



A spring can also be progressively wound. This means that the rate of the spring is increasing as it is compressed. A 100/200 lbf/in progressive spring will require 100 pounds to compress the first one inch but will require 200 additional pounds to compress the last one inch (see following illustration).



An easy way to measure coil springs is to put a bathroom scale in a press with the spring resting on the scale. Measure the free length and then apply a load until the spring compresses 1 inch. The reading on the scale will approximate the rate of the spring. Now compress the spring another 1 inch. If the spring is a straight rate, the scale reading should be doubled. If the reading is more than doubled, then you have a progressive spring. If you can compress the spring another 1 inch (3 inches total) (do not exceed maximum scale rating or damage may occur) the reading should be 3 times your first reading. In order to maintain a reasonable cost on springs, the manufacturing tolerances are quite large. A 100 lbf/in rated spring may test anywhere from 80 to 120 lbf/in.

Now, so far we have assumed that the 2 springs in our examples have the same free length and that they are not preloaded at all. In the case of our suspensions, we mount the coil springs on a shock absorber. The shock will have a certain length between the spring retainers which is called the installed length of the spring. If the installed length is less than the free length (as is the case in most applications), then there will be some preloading of the spring.

Dual Rate Spring Formula

$$\frac{\text{Spring 1} \times \text{Spring 2}}{\text{Spring} + \text{Spring 2}}$$

A Dual Rate Spring will assume the rate of the heavier rate spring when the lighter spring bottoms or coil binds.

Example:

Spring 1 100# Rate

Spring 2 150# Rate

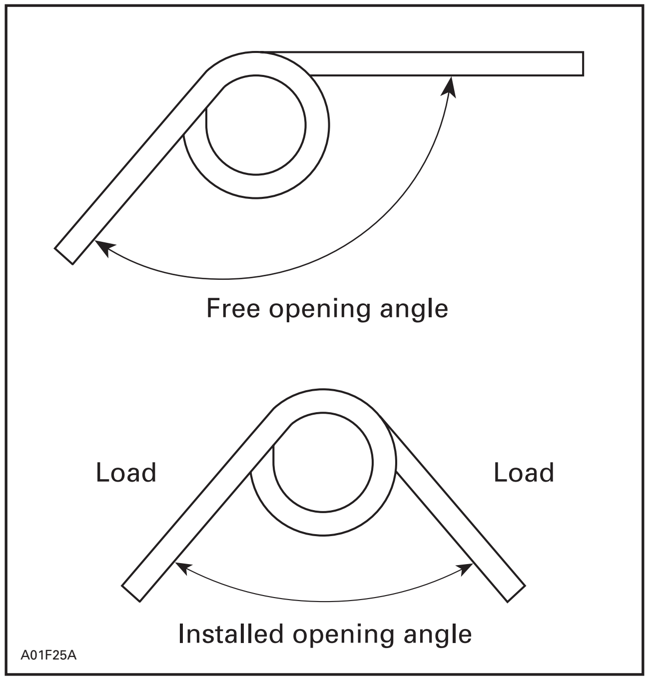
$$\frac{100 \times 150}{100 + 150} = \frac{1500}{250} = 60$$

Spring 1 was a 100# Rate separately, but when stacked on the 150# spring (spring 2), it now has a 60# rate. As the spring bottoms or coil binds, it will assume the 150# rate of spring 2.

Torsional Springs

A torsional spring acts just like a coil spring but it is shaped differently. It is much more difficult to measure the rate of a torsional spring because of the lengths of the legs and where the load will be applied. The rear torsional springs on the S chassis are rated in lb-ft/degree (pounds-feet per degree of rotation). Suffice it to say that there are stiffer and softer springs for most applications.

The preload on a torsional spring is controlled by the free opening angle and the installed opening angle. If a torsional spring must be **twisted** more to be installed, then it will have more preload (following illustration).



Spring Identification

Our springs will have one, 2 or 3 stripes of color painted on the spring. This is the color code used for identification. Refer to the applicable chart to find a cross reference between the part number, model application, color code, spring rate, free length and spring type. The spring type denotes physical characteristics of the spring like the inside diameter of the ends which will determine the type of retainer used to hold the spring. All spring types are not interchangeable.

CHECK THE SPRING TYPE AND FIT OF THE SPRING RETAINER BEFORE INSTALLING DIFFERENT SPRINGS!

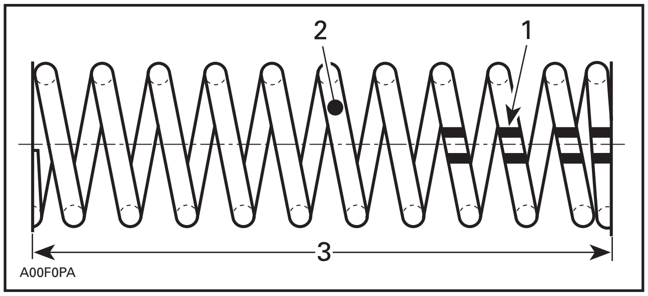
SPRING DESCRIPTION

COIL SPRINGS (compression)

NOTE: Read color when spring is upright and stripes are down.

Type R (straight on both ends)

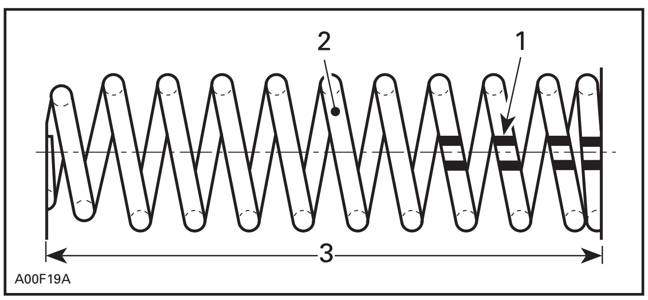
(Single Rate Spring)



1. Color code stripes
2. Wire diameter
3. Free length

Type S (barrel shape on one end)

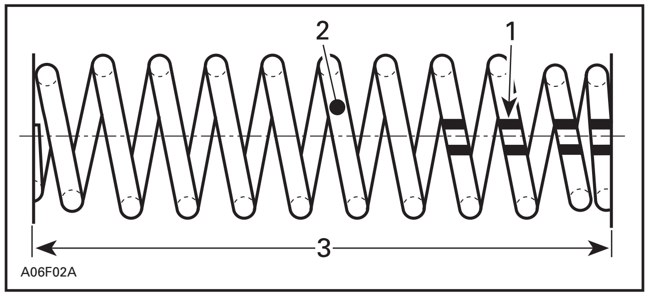
(Single Rate Spring)



1. Color code stripes
2. Wire diameter
3. Free length

Type T (barrel shape on both ends)

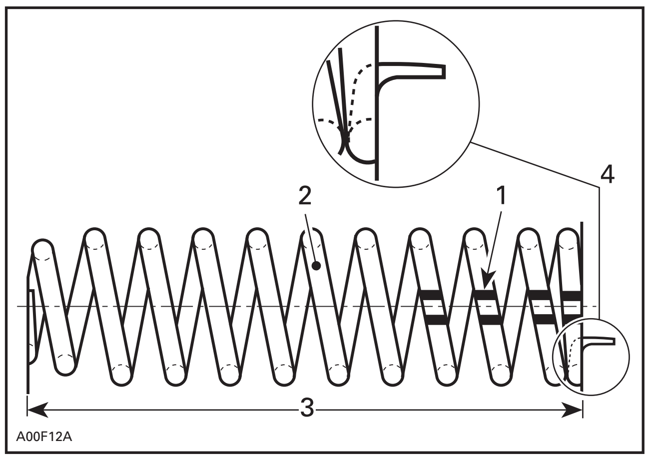
(Single Rate Spring)



1. Color code stripes
2. Wire diameter
3. Free length

Type U (barrel shape on one end with positioning tab at the other end)

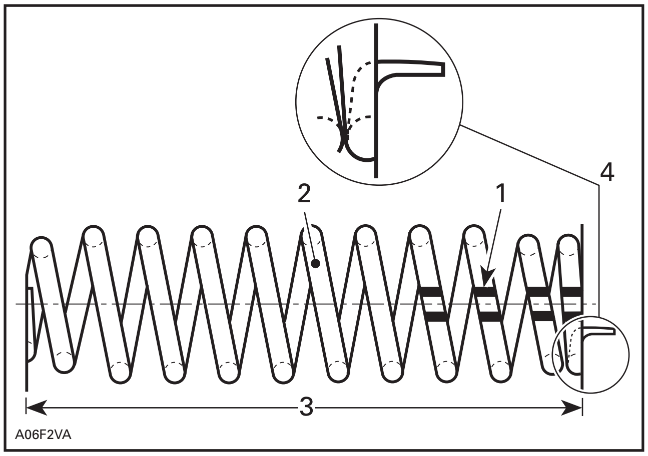
(Single Rate Spring)



1. Color code stripes
2. Wire diameter
3. Free length
4. Positioning tab

Type Y
(barrel shape on both ends with positioning tab at the color code coils end)

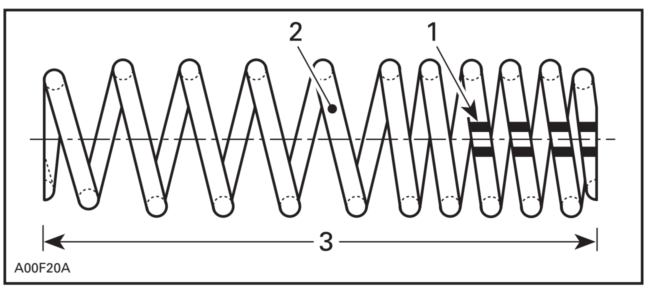
(Single Rate Spring)



1. *Color code stripes*
2. *Wire diameter*
3. *Free length*
4. *Positioning tab*

Type 2
(barrel shape on both ends)

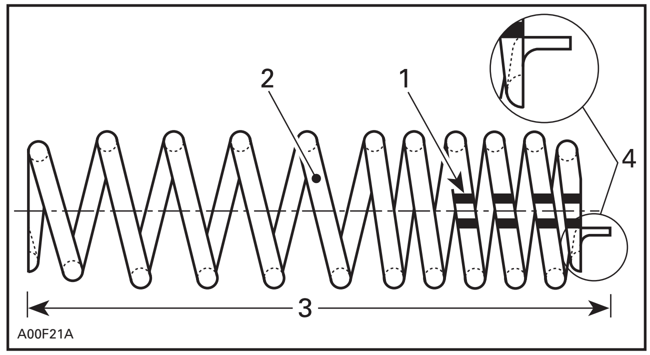
(Dual Rate Spring)



1. *Color code stripes*
2. *Wire diameter*
3. *Free length*

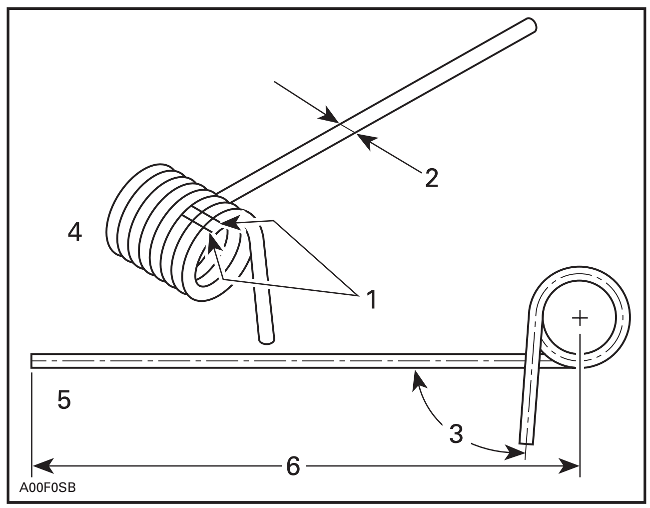
Type 4
(barrel shape on both ends with positioning tab at the color code coils end)

(Dual Rate Spring)



1. *Color code stripes*
2. *Wire diameter*
3. *Free length*
4. *Positioning tab*

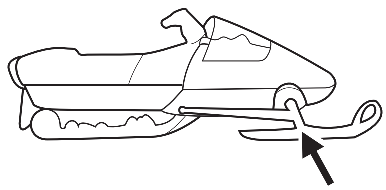
TORSION SPRINGS



1. *Color code stripes*
2. *Wire diameter*
3. *Opening angle (°)*
4. *Left hand (LH)*
5. *Right hand (RH)*
6. *Length*

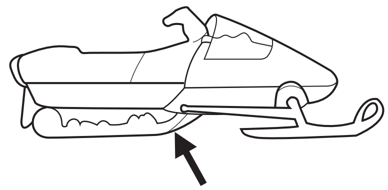
SPRING APPLICATIONS

2001 FRONT SPRINGS 2001

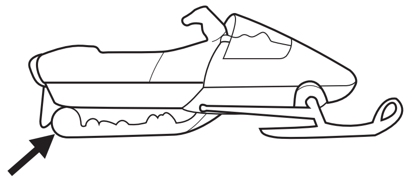


MODEL	(P/N) SOFTER SPRING	(P/N) STANDARD	(P/N) HARDER SPRING
MACH Z	414 956 300	**415 075 900**	415 039 700
MACH Z TECH PLUS	414 956 300	**415 075 900**	415 039 700
MX Z STANDARD	Not Applicable	**505 070 181**	Not Applicable
MX Z ADRENALINE	Not Applicable	**505 070 181**	Not Applicable
MX Z TRAIL	Not Applicable	**505 070 393**	Not Applicable
MX Zx	Not Applicable	**505 070 692**	Not Applicable
MX Z 500 F	414 956 300	**415 075 900**	415 039 700
MX Z 380 F	414 956 300	**415 075 900**	415 039 700
SUMMIT STANDARD	Not Applicable	**505 070 020**	505 070 305
SUMMIT X	Not Applicable	**505 070 573**	505 070 305
SUMMIT STANDARD HM	Not Applicable	**505 070 020**	505 070 305
SUMMIT X HM	Not Applicable	**505 070 573**	505 070 305
SUMMIT 500 F	414 859 300	**505 070 698**	414 968 600

2001	CENTER SPRINGS		2001
MODEL	(P/N) SOFTER SPRING	(P/N) STANDARD	(P/N) HARDER SPRING
MACH Z	415 070 400	**415 090 500 415 090 600**	415 103 600
MACH Z TECH PLUS	415 070 400	**415 090 500 415 090 600**	415 103 600
MX Z STANDARD	415 070 500	**503 189 325**	Not Applicable
MX Z ADRENALINE	415 070 500	**503 189 325**	Not Applicable
MX Z TRAIL	415 070 500	**503 189 325**	Not Applicable
MX Zx	415 070 500	**503 189 325**	Not Applicable
MX Z 500 F	414 974 400	**415 069 900**	414 771 300
MX Z 380 F	414 974 400	**415 069 900**	414 771 300
SUMMIT STANDARD	415 070 500	**503 189 325**	Not Applicable
SUMMIT X	415 070 500	**503 189 325**	Not Applicable
SUMMIT HM STANDARD	415 070 500	**503 189 325**	Not Applicable
SUMMIT HM X	415 070 500	**503 189 325**	Not Applicable
SUMMIT 500 F	414 974 400	**503 189 000**	414 771 300



2001	REAR SPRINGS		2001



MODEL	(P/N) SOFTER SPRING	(P/N) STANDARD	(P/N) HARDER SPRING
MACH Z	503 189 629 LH 503 189 627 RH	503 189 616 LH 503 189 615 RH	503 189 445 LH 503 189 443 RH
MACH Z TECH PLUS	503 189 629 LH 503 189 627 RH	503 189 616 LH 503 189 615 RH	503 189 445 LH 503 189 443 RH
MX Z STANDARD	503 189 629 LH 503 189 627 RH	503 189 445 LH 503 189 443 RH	503 189 524 LH 503 189 522 RH
MX Z ADRENALINE	503 189 629 LH 503 189 627 RH	503 189 445 LH 503 189 443 RH	503 189 524 LH 503 189 522 RH
MX Z TRAIL	503 189 629 LH 503 189 627 RH	503 189 445 LH 503 189 443 RH	503 189 524 LH 503 189 522 RH
MX Zx	503 189 629 LH 503 189 627 RH	503 189 445 LH 503 189 443 RH	503 189 524 LH 503 189 522 RH
SUMMIT STANDARD	503 189 594 LH 503 189 592 RH	503 189 629 LH 503 189 627 RH	503 189 445 LH 503 189 443 RH
SUMMIT X	503 189 594 LH 503 189 592 RH	503 189 629 LH 503 189 627 RH	503 189 445 LH 503 189 443 RH
SUMMIT HM STANDARD	503 189 594 LH 503 189 592 RH	503 189 629 LH 503 189 627 RH	503 189 445 LH 503 189 443 RH
SUMMIT HM X	503 189 594 LH 503 189 592 RH	503 189 629 LH 503 189 627 RH	503 189 445 LH 503 189 443 RH
SUMMIT 500 F	503 189 347 LH 503 189 346 RH	503 189 355 LH 503 189 354 RH	503 189 343 LH 503 189 342 RH

LH = Left Hand   RH = Right Hand

SPRING SPECIFICATIONS

Coil Springs Specifications

P/N	TYPE	SPRING RATE (lb/in) ± 10	FREE LENGTH (mm) ± 3	WIRE DIAMETER (mm) ± .05	COLOR CODE STRIPES	COLOR OF SPRING
414 771 300	R	135	272.5	8.41	BK/BK	SAFARI RED
414 859 300	R	90	239	7.14	BK/WH	YELLOW
414 956 300	R	100	265	7.14	PI/WH/BL	YELLOW
414 968 600	R	125	235	7.49	RD	NEON GREEN
415 039 700	R	150	258	8.71	PI	BLACK
415 057 500	R	160	264	8.71	RD/GD	BLACK
415 075 900	R	125	262	7.92	BL/RD/BK	YELLOW
415 090 500	R	293	45	6.17	YL/BL/YL	BLACK
505 070 685	R	125	262	7.92	YL/YL/BK	FULL MOON
505 070 698	R	100	239	7.14	WH/BK/BK	YELLOW
415 090 600	S	220	210	9.19	RD/BL/YL	BLACK
415 069 900	T	115	265	7.49	SI/YL/YL	BLACK
415 070 400	T	115	270	8.25	GN/YL/YL	BLACK
415 070 500	T	135	242	8.41	BL/YL/YL	BLACK
415 103 600	T	135	264	8.25	GN/GN/YL	BLACK
503 189 000	T	115	265	7.92	YL/GD/YL	BLACK
503 189 325	T	150	242	8.25	YL/SI/YL	BLACK
503 189 659	T	180	242	8.71	BL/RD/YL	BLACK
503 189 686	T	200	242	9.19	RD/SI/YL	BLACK
505 070 305	T	105	250	8.25	RD/OR/BK	YELLOW
505 070 475	T	90	250	7.77	BK/YL/GN	SILVER REFLECTION
505 070 573	Y	90	250	7.77	RD/BL/GN	YELLOW
505 070 298	2	70 - 100	340	8.25	BL/PI/BK	YELLOW
505 070 393	2	55 - 85	320	7.77	RD/BL/RD	YELLOW
505 070 684	2	65 - 95	340	8.25	BK/GD/BK	FULL MOON
505 070 686	2	55 - 85	320	7.77	YL/WH/BK	FULL MOON
505 070 181	4	55 - 85	320	7.77	PI/BK/BK	YELLOW
505 070 692	4	55 - 85	320	7.77	BL/GN/RD	YELLOW
706 000 172	R	45	345	6.91	GR/BKRD	YELLOW
505 070 941	T	150	315	9.52	RD/SI/BK	YELLOW
503 189 999	R	325	189	9.52	GD/SI/YL	BLACK
503 189 990	R	275	189	9.19	GD/WH/YL	BLACK

SPRING COLOR CODES
BK = BLACK BL = BLUE GD = GOLD GN = GREEN OR = ORANGE PI = PINK RD = RED SI = SILVER WH = WHITE YL = YELLOW

P/N	TYPE	SPRING RATE (lb/in) ± 10	FREE LENGTH (mm) ± 3	WIRE DIAMETER (mm) ± .05	COLOR CODE STRIPES	COLOR OF SPRING
503 189 988	U	215	64	6.35	GD/GD/YL	BLACK
505 070 852	4	40-85	340	7.49	RD/GR/RD	YELLOW
706 000 130	R	45	360	6.91	WH/RD/BK	YELLOW
503 189 812	2	125-200	250	8.41	BL/GR/YL	BLACK
505 070 762	T	105	300	8.71	GR/GD/BK	YELLOW
505 070 760	Y	95	280	8.25	BL/GD/BK	YELLOW
505 070 758	2	45-85	320	7.49	RD/GD/BK	YELLOW
505 070 576	T	150	300	9.19	RD/BL/WH	YELLOW
505 070 575	U	290	45	6.17	RD/BL/GD	YELLOW
505 070 572	2	55-85	320	7.77	RD/BL/BL	SILVER
706 000 068	R	68	355	7.77	GR/WH/BK	YELLOW
505 070 536	T	150	300	9.19	GR/WH/YL	BLACK
505 070 534	U	290	45	6.17	BL/WH/YL	BLACK
505 070 474	4	55-85	320	7.77	BK/YL/BL	SILVER
505 070 473	R	125	260	7.92	BK/YL/RD	SILVER
505 070 446	R	100	242	7.14	RD/YL/BK	BLUE
505 070 394	R	125	235	7.49	RD/WH/YL	BLACK
505 070 391	2	65-95	340	8.25	YL/BK/BK	SILVER
505 070 392	2	55-85	320	7.77	RD/GD/YL	BLACK
503 189 090	S	220	200	9.19	YL/WH/YL	BLACK
505 070 034	4	60-90	325	7.77	BL/GR/BK	YELLOW
505 070 302	U	100	265	7.14	OR/PI/BK	YELLOW
505 070 300	U	150	260	8.71	GR/PI/BK	YELLOW
505 070 233	U	125	260	7.92	PI/BL/BK	YELLOW
505 070 153	2	65-95	340	8.25	GR/GR/BK	YELLOW
505 070 130	R	75	410	6.17	YL/PI/YL	BLACK
505 070 240	T	90	265	7.49	RD/PI/BK	YELLOW
706 200 006	V	140	270	8.25	OR/BK/BK	YELLOW
505 070 146	T	100	315	8.71	RD/RD/RD	YELLOW
505 070 144	T	100	390	8.25	RD/BK/RD	YELLOW
505 070 093	T	85	290	7.77	BK/GR/BK	RED
505 070 092	2	65-95	340	8.25	BK/YL/BK	RED
505 070 091	2	65-95	340	8.25	BK/BL/BK	GOLD
505 070 090	R	125	235	7.49	BL/BL/BK	COPPER
505 070 089	R	125	260	7.92	GR/BK/BK	GOLD

SPRING COLOR CODES
BK = BLACK   BL = BLUE   GD = GOLD   GN = GREEN   OR = ORANGE   PI = PINK   RD = RED SI = SILVER   WH = WHITE   YL = YELLOW

Part numbers with a 486 prefix must be ordered from the Valcourt Race Dept.
All others must be ordered from your local Ski-Doo dealer.

Torsion Spring Specification

P/N	WIRE DIAMETER (mm)	OPENING ANGLE ± 7	LENGTH (mm)	COLOR CODE
486 071 100 RH 486 071 200 LH	10.3	135	400	YL/YL
486 071 300 RH 486 071 400 LH	10.3	150	400	WH/WH
486 078 500 RH 486 078 600 LH	10.0	115	400	YL/RD
503 188 100 RH 503 188 200 LH	11.11	100	400	BL/YL
503 189 080 RH 503 189 083 LH	11.5	100	385	GD
486 093 200 RH 486 093 300 LH	11.5	80	400	GN/YL
503 189 241 RH 503 189 242 LH	11.11	105	400	OR/YL
503 189 327 RH 503 189 329 LH	11.89	100	385	SI
503 189 334 RH 503 189 335 LH	11.11	105	400	YL/GD
486 099 100 RH 486 099 300 LH	11.89	140	385	YL/RD/YL
503 189 881 RH 503 189 883 LH	11.11	75	385	YL/BL
503 189 898 RH 503 189 900 LH	11.5	90	385	GD/GD/GD
503 189 902 RH 503 189 904 LH	10.6	80	385	RD/RD/YL
503 189 947 RH 503 189 948 LH	10.3	75	385	GN/YL/YL
503 189 992 RH 503 189 994 LH	11.11	73	385	GN/RD/YL
503 189 338 RH 503 189 339 LH	11.11	90	400	GN/GN
503 189 342 RH 503 189 343 LH	10.6	80	400	RD/RD/RD
503 189 346 RH 503 189 347 LH	10.3	85	400	YL/YL/YL
503 189 350 RH 503 189 351 LH	11.5	100	385	GD/GD

P/N	WIRE DIAMETER (mm)	OPENING ANGLE ± 7	LENGTH (mm)	COLOR CODE
503 189 354 RH 503 189 355 LH	10.6	90	400	WH/WH/WH
503 189 358 RH 503 189 359 LH	11.11	80	400	BL/BL
503 189 443 RH 503 189 445 LH	11.11	95	385	GN/GN/GN
503 189 522 RH 503 189 524 LH	11.11	90	385	GN/GN/YL
503 189 592 RH 503 189 594 LH	10.3	85	385	GD/RD
503 189 615 RH 503 189 616 LH	11.11	100	385	RD/YL
503 189 627 RH 503 189 629 LH	10.6	90	385	YL/WH
503 189 674 RH 503 189 675 LH	11.11	80	385	GD/YL/YL
503 189 681 RH 503 189 683 LH	11.9	80	385	SI/SI

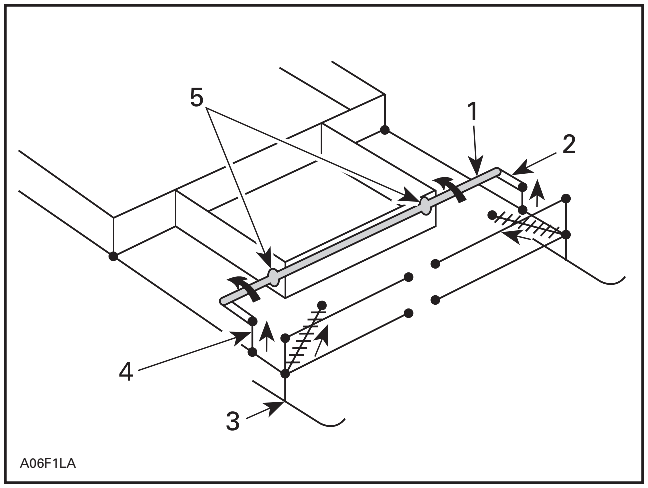
Part numbers with a 486 prefix must be ordered from the Valcourt Race Dept.
All others must be ordered from your local Ski-Doo dealer.

CORNERING DYNAMICS

The ideal situation, while going through a turn, is to keep the snowmobile as flat as possible without the skis or track losing contact with the driving surface.

As you enter a corner and turn the skis, the rest of the vehicle will want to continue straight ahead. If the skis do not bite the surface, they will start slipping and the vehicle will not turn as tight as the skis are turned. This is called **understeering** or pushing. If the skis bite very well and the track starts sliding out, then the vehicle is **oversteering** or is said to be loose. If the ski and track traction is balanced, then the vehicle will maintain a good line though the corner. Because the center of gravity of the vehicle wants to continue straight ahead and because the center of gravity is above ground level, weight will be transferred to the outside of the vehicle. This causes the machine to roll to the outside. As the radius of the corner gets tighter and/or speeds increase, the machine rolls more, and more weight is transferred to the outside of the vehicle until the front or back loses traction or the vehicle tips over.

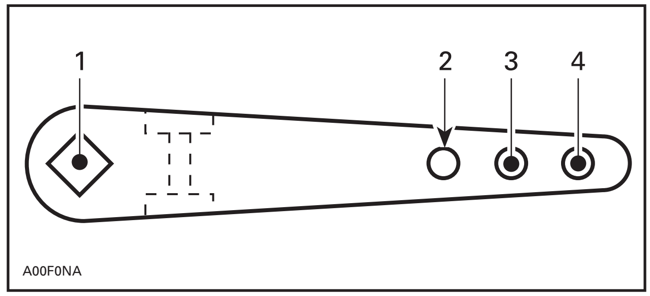
Roll can be reduced by installing stiff springs on the front suspension and/or a lot of preload, but this will cause a harsher ride than necessary. Lowering the center of gravity will also reduce roll but there are practical limits as to how low the center of gravity can go. Most vehicles are equipped with an antiroll bar or **stabilizer** bar. Common terminology will refer to it as a **sway** bar. (It is inaffect an **anti-sway** bar) The bar is mounted to and pivots on the chassis. The ends of the bar have lever arms from 3″ to 7″ in length. The ends of the levers are connected to the front suspension. As the outside suspension is compressed during a corner, the bar is twisted and forces the inside spring to compress also. The bar is “borrowing” spring pressure from the inside spring and adding it to the outside spring. The suspension can now resist more chassis roll (see following illustration).



1. *Sway bar*
2. *End lever*
3. *Cornering force*
4. *Connector linkage*
5. *Pivot bushings*

By having a sway bar in the suspension, softer springs can be used to achieve a good ride because the bar will help control roll in a corner. The bar has no affect on ride when traveling straight ahead over bumps that are even from side to side. However, if only one ski encounters a bump, then the bar will transfer energy between the springs. This leads to another design decision. The diameter of the sway bar determines how much spring pressure will be **borrowed** from the opposite spring. A smaller bar will twist more and not transfer as much energy. A larger diameter bar will transfer more energy which will reduce chassis roll, but will produce a harsher ride on uneven, bumpy terrain. A smaller diameter bar will give a more compliant ride on the nasty bumps but it will allow the chassis to roll more in corners. A cross country sled will use small to medium diameter bars while oval and lemans racers will use large diameter bars.

The length of the lever arm also affects the **stiffness** of the sway bar. A shorter lever will **stiffen** the bar and a longer lever will **soften** the bar. Many lever arms will have 2 holes to mount the connector linkage. The hole closest to the bar will act stiffer (see following illustration).



END LEVER

1. *Sway bar*
2. *Stiffer*
3. *Softer*
4. *Softest*

Unlike other models the MX Z and ZX A.D.S.A. suspension use a non adjustable sway bar. In order to change the roll stiffness the diameter of the sway bar must be changed.

Anti-Roll Bar Options

P/N	DIAMETER MM	SKI STANCE	MODEL
486 094 300	15.8	41	MX Z
486 094 400	18	41	MX Z
505 070 309	14	41	MX Z
505 070 282	14.3	37	Summit
506 131 800	17.5	42.5	MX Z
505 070 563	15.8	42.5	MX Z
505 070 490	12.7	42.5	MX Z
506 134 300	12.7	41	Mach
486 073 600	15.9	41	Mach
486 073 800	19.1	41	Mach
486 074 000	25.4	41	Mach

Part numbers with a 486 prefix must be ordered from the Valcourt Race Dept.

All others must be ordered from your local Ski-Doo dealer.

When changing the sway bar diameter you must also change the ball joint blocks and bushings.

For snowcross racing some racers prefer to disconnect the sway bar. This will let the front suspension act more independently, as the suspension is no longer coupled.

Another little known fact that has a large affect on roll is the limiter strap length. As mentioned earlier, if the limiter is lengthened, the front suspension will extend during acceleration, which reduces ski pressure. If this vehicle was in a corner when power was applied, it would have quite a bit of chassis roll and the inside ski will start to lift off of the ground. Shortening the limiter will have a very large affect on controlling roll. A general guideline for initially setting limiter length for good ski pressure and reducing roll is to have the front and back of the track touch the ground at the same time when you set the back of the vehicle down. If the front of the track touches much sooner than the rear, there will be quite a lot of weight transfer and chassis roll during hard cornering. A quick adjust limiter assembly, (P/N 486 095 600 SC-10 II and P/N 486 095 700 SC-10) is available for models equipped with the SC-10 and SC-10 II rear suspension. If the adjuster nut is all the way tight and you need more ski pressure, install a shorter limiter strap.

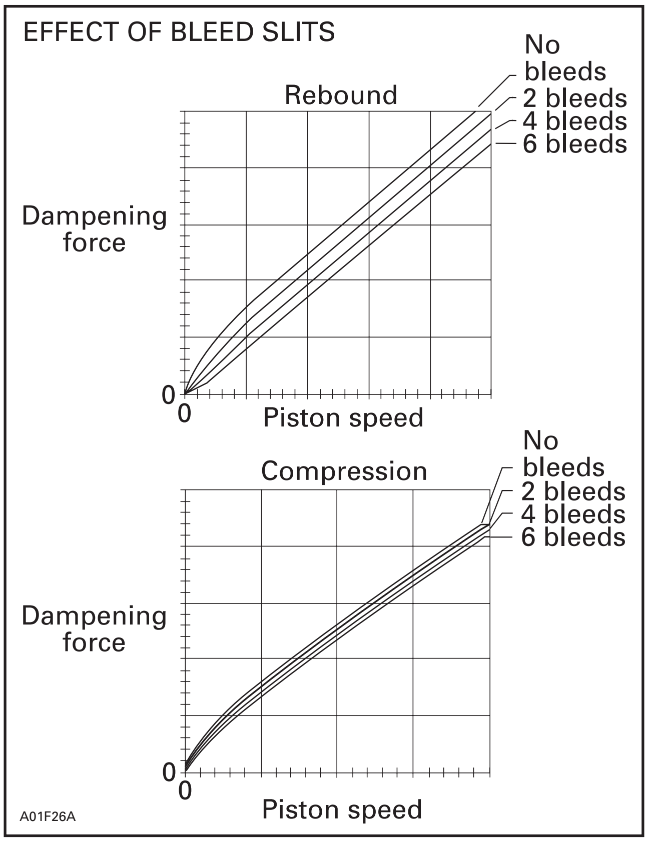
SHOCKS

Valving and Dampening

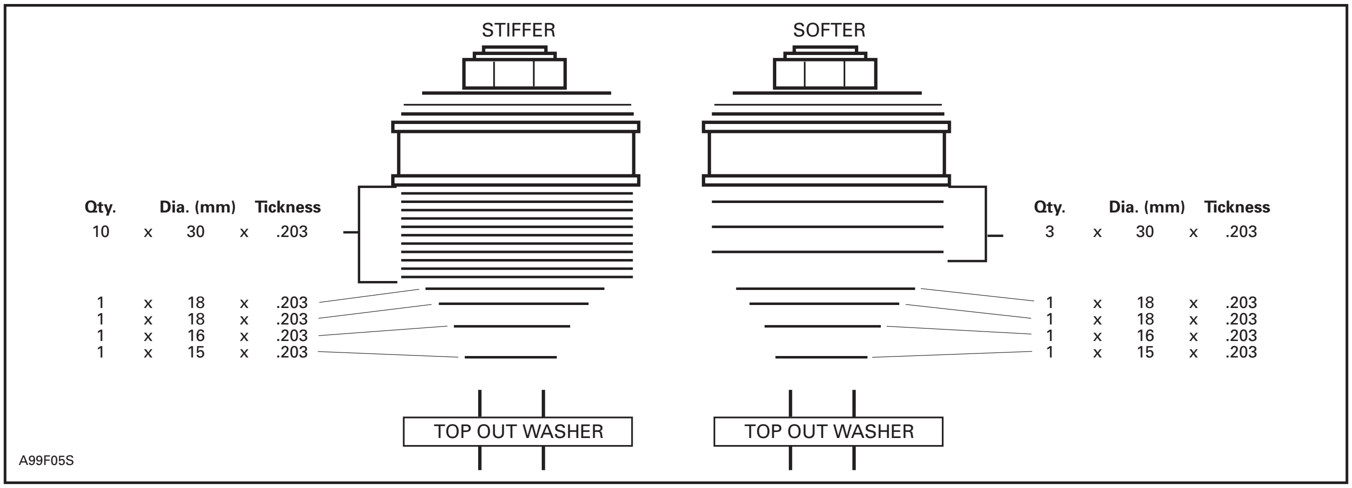
In the HPG shock, the piston passages are covered by a stack of thin metal shims of various thicknesses and diameters. The shims provide dampening by acting as spring loaded valves offering resistance to the oil traveling through the piston. There is a stack of shims on both sides of the piston. One side controls compression dampening and the other side controls rebound dampening. By varying the number and thickness of shims the dampening characteristics can be very accurately obtained. There may also be orifices or slits in the piston that are not covered by the shims. These are referred to as bleed slits. The size and number of these slits will also affect dampening. The external adjustment on the MVA, HPG shocks is a variable bleed hole.

Rebound dampening will usually be much stiffer than compression dampening. This is because rebound dampening must resist the force of the spring and because piston speeds are much slower during rebound.

At low piston speeds, the number of bleed slits will have a fairly large effect on dampening, but as piston speeds increase most of the dampening is controlled by the shim stack. This is because the flow area of the slits is much smaller than the flow area under the shims. Since only a small amount of oil can flow through the bleed slits (compared to the amount that flows under the shim stack), the slits have only a very small effect on dampening at high piston speeds. Because of this characteristic, bleed slits are most effective on rebound dampening. They will have only a very slight effect on compression damping because the typical piston speeds on compression strokes are several times faster than on rebound strokes. There really is no such thing as **high speed** rebound dampening.



As mentioned earlier, the configuration of the shim stack will control most of the dampening of the shock. There are several methods to tuning shim stacks. The first and most commonly used is to increase or decrease the overall stiffness of the stack. This can be done by changing the number of large shims or by increasing or decreasing their thickness.



The overall stiffness of the stack has been increased by adding 7-30 mm × .203 mm shims. This will result in firmer dampening at both low and high piston speeds. Thicker shims will also result in firmer dampening but it is better to use more thin shims than fewer thick shims. More thin shims will provide better, smoother dampening than a few thick shims. There is an equivalency between thick and thin shims, though. The following chart indicates how many thin shims are required to equal the stiffness of one thick shim.

(mm)

1 × .152 = 2.4 × .114
1 × .203 = 2.3 × .152
1 × .254 = 2.0 × .203

This means it will take 2.4 × .114 mm shims to have the same dampening as 1 × .152 mm shim. Obviously you can't use a fraction of a shim so you must find the lowest common denominator. For 2.4 it will be 5. For 2.3 it will be 10. The following chart shows the most common possibilities.

(mm)

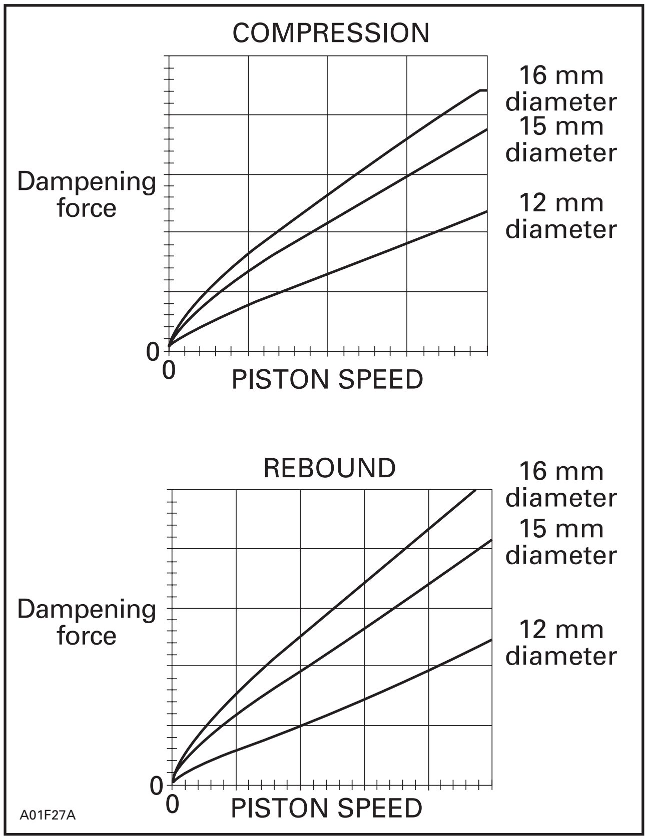
5 × .152 = 12 × .114
10 × .152 = 24 × .114
10 × .203 = 23 × .152
1 × .254 = 2 × .203
2 × .254 = 4 × .203
3 × .254 = 6 × .203
4 × .254 = 8 × .203
5 × .254 = 10 × .203
6 × .254 = 12 × .203
7 × .254 = 14 × .203
8 × .254 = 16 × .203
9 × .254 = 18 × .203
1 x .305 = 2 x .254
2 x .305 = 3 x .254
3 x .305 = 5 x .254
4 x .305 = 7 x .254
5 x .305 = 9 x .254
6 x .305 = 10 x .254

The diameter of the smaller shims that support the large shims will also affect the dampening. A larger support shim gives more support to the large shim thus making it act stiffer. Conversely, a smaller diameter support shim will allow the large shim to bend more easily thus softening the dampening. The following graph shows the effect of different diameter support washers.

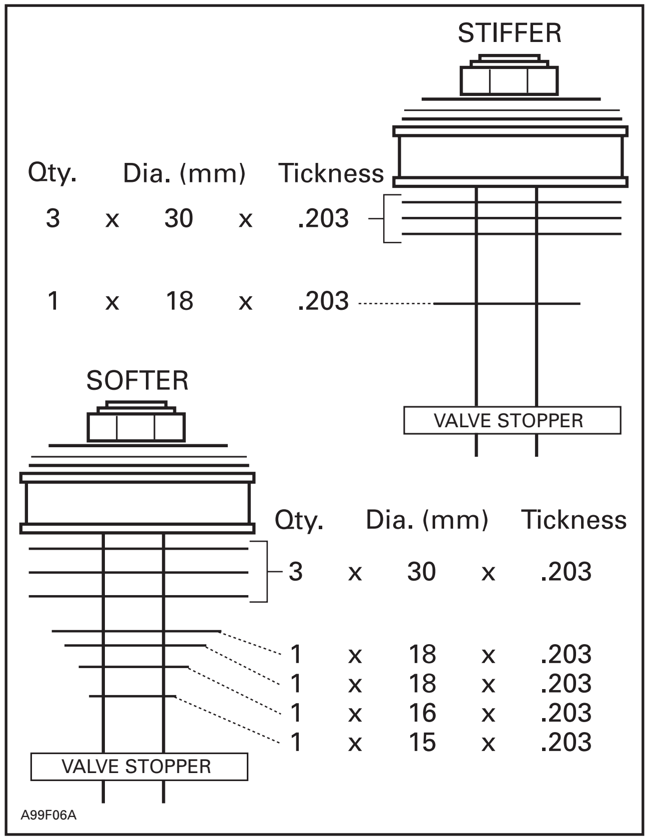
Shim Comparator Formula

Thickness³ or cubed.

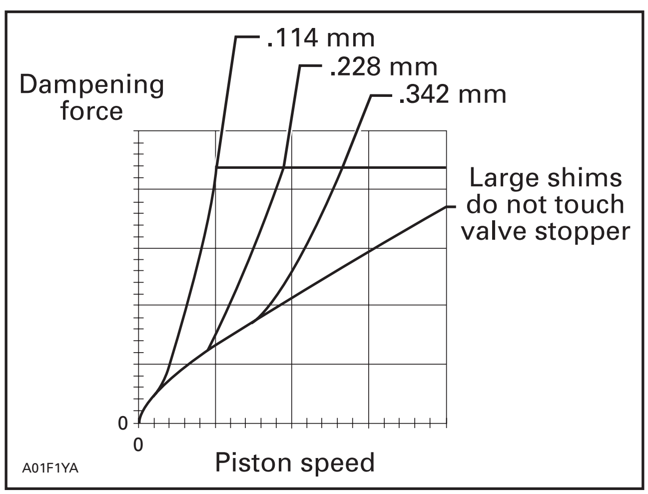
Example: .152 x .152 x .152



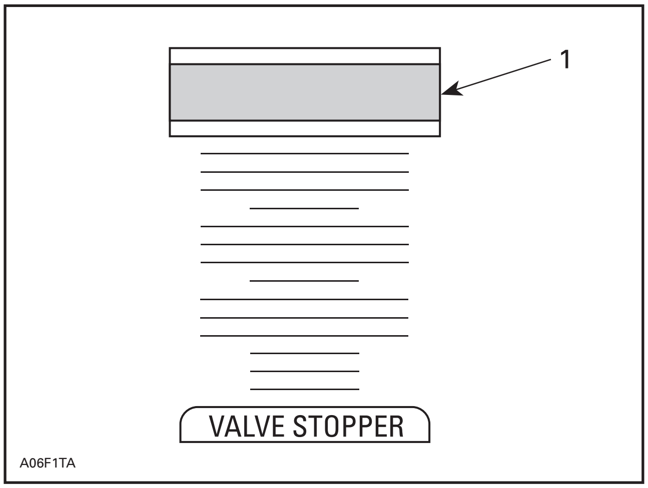
Another method of changing dampening is by controlling the amount of space the stack has to open. This is done by reducing the amount of smaller shims which support the larger shims. The larger shims act the same until they bottom out against the valve stopper.



The large shims are only able to deflect .203 mm instead of .610 mm thus reducing the flow area of the piston. This will result in the same low speed dampening, but the medium and high speed damping will be increased. The following graph represents the effect of changing the total thickness of small shims which determine the amount of large shim deflection.



As you can see, low speed dampening remains the same until the shim stack bottoms out against the valve stopper. Then the dampening becomes significantly stiffer. This is sometimes referred to as progressive dampening. Another similar way to achieve this type of dampening is to use multiple stacks of large and small shims.



1. *Piston*

The first stack of large shims will deflect very easily thus giving soft low speed dampening. The number of small shims will determine when the first stack hits the second stack of large shims. Now both stacks are acting together thus stiffening the dampening. This can be repeated several times until the complete stack of large shims bottoms out against the valve stopper.

As you can see, there are an unlimited number of valving combinations and many different versions will achieve very similar results. The following general guidelines should help reduce your tuning time.

– If the dampening is close to what you want, just add or remove 1 or 2 large shims, from the appropriate side, to fine tune the overall stiffness.

NOTE: Always use 30 mm diameter shims against the piston for compression dampening and 26 mm diameter shims against the piston for rebound dampening. Excludes C-46 shock.

– Generally, rebound dampening should not be changed unless a large change in spring rate is made.

– Bleed slit quantity will affect low speed dampening.

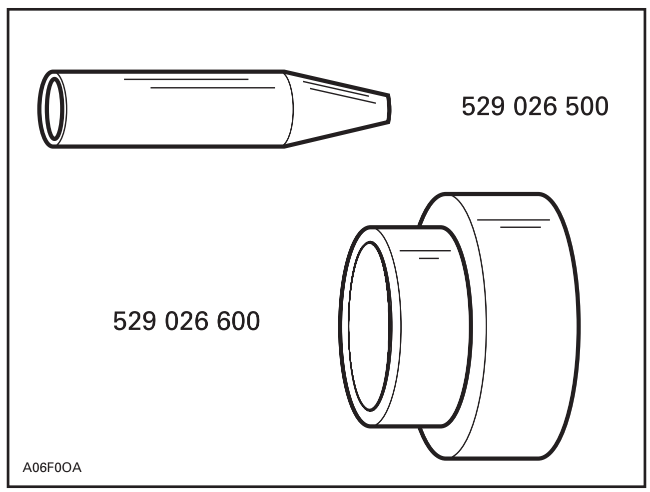
– Under dampening may be due to an aerated shock due to low gas pressure and/or old, used oil. Change the oil and recharge the gas pressure to 300 PSI before altering the shock valving.

– If the vehicle bounces or **pogos** a lot, the problem may be too little compression dampening NOT too little rebound dampening. Do not use too much rebound dampening! Excessive rebound dampening is a common error. Over-dampening will not allow the suspension to recycle to full extension after an obstacle compresses the suspension. This situation (called packing) will eventually bottom the suspension and not allow it to cycle properly.

– For faster weight transfer under acceleration and deceleration, use a piston with more bleed slits.

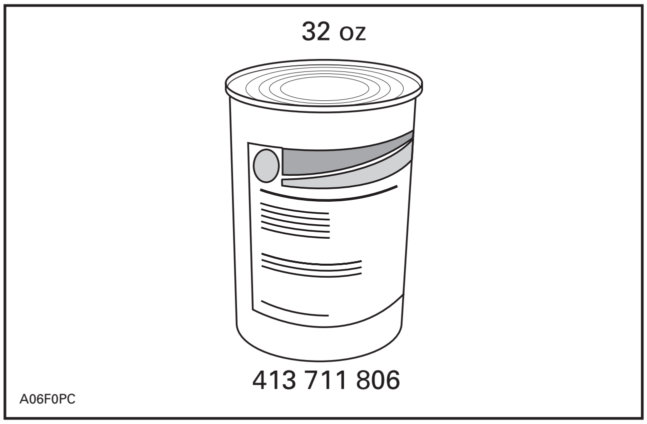
Special Tools

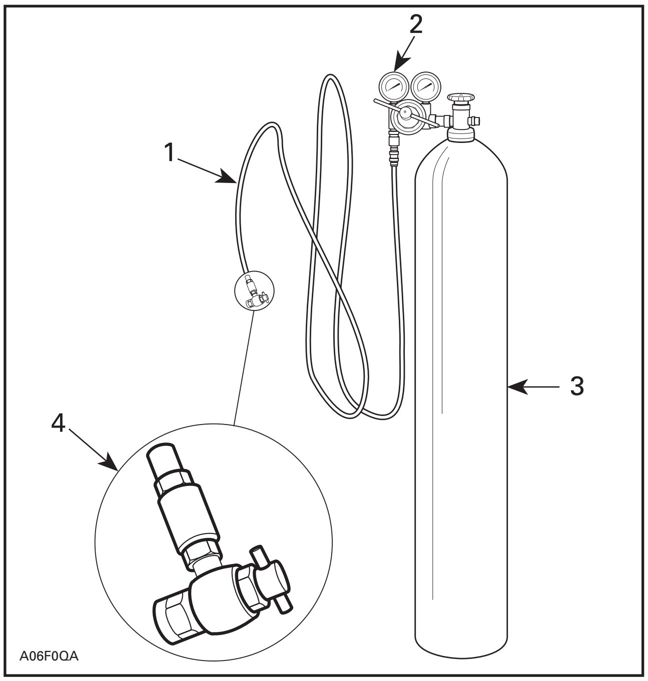
Special tools specific to the HPG T/A shock will be the seal pilot (P/N 529 026 500) and piston guide (P/N 529 026 600) from Bombardier. Excludes C-46 shock.



NOTE: Do not attempt to rebuild the T/A damper without the benefit of these assembly tools, damage will occur without their use.

Shock Oil and Nitrogen





1. Automotive type air pressure hose
2. 2 stage regulator, delivery pressure range 2070 kPa (300 PSI)
3. High pressure cylinder filled with industrial grade nitrogen
4. Valve tip (P/N 529 035 570)

NOTE: Commercially available through compressed gas dealers.

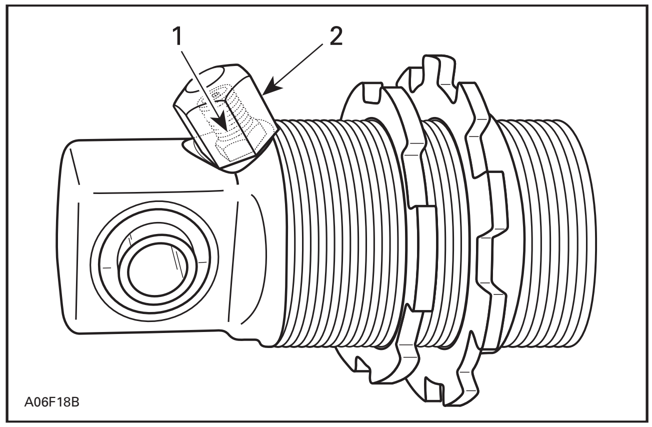
Disassembly and Assembly

Release N_2 (nitrogen) pressure from the damper Schrader valve on any HPG T/A with IFP.

NOTE: When rebuilding a gas emulsion shock, such as the center MX Z, mount the shock vertically in a vice with the schrader valve up and let it sit for 5 minutes before releasing the gas. This 5 minute period will allow most of the gas to separate from the oil and minimize oil spray.

⚠ WARNING

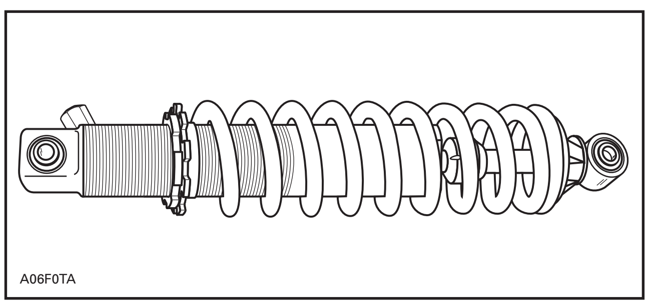
Nitrogen gas is under extreme pressure. Use caution when releasing this gas volume. Protective eye wear should be used.



1. *Schrader valve 1.5-2 N•m (13-17 lbf•**in**)*
2. *Schrader cap 5-6.5 N•m (44-57 lbf•**in**)*

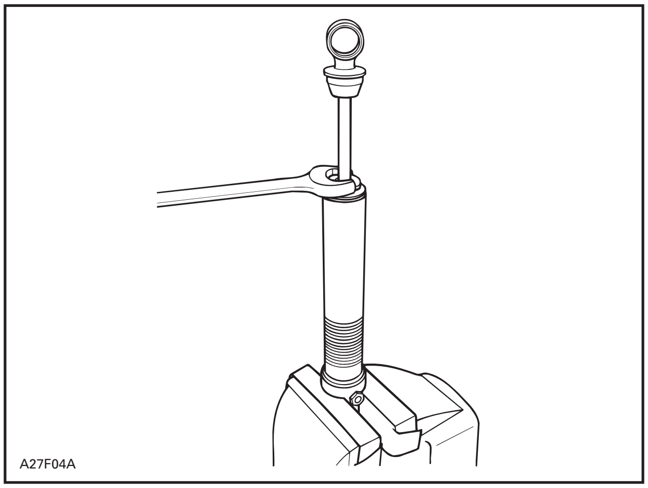
NOTE: Before unscrewing pre-load rings, measure the compressed length of the installed spring and mark position for reinstallation. For factory adjustment refer to the end of this section.

Use tools (P/N 861 743 900) to remove damper spring by unthreading spring pre-load rings, then removing spring retainer or use the spring removal tool (P/N 529 035 504).



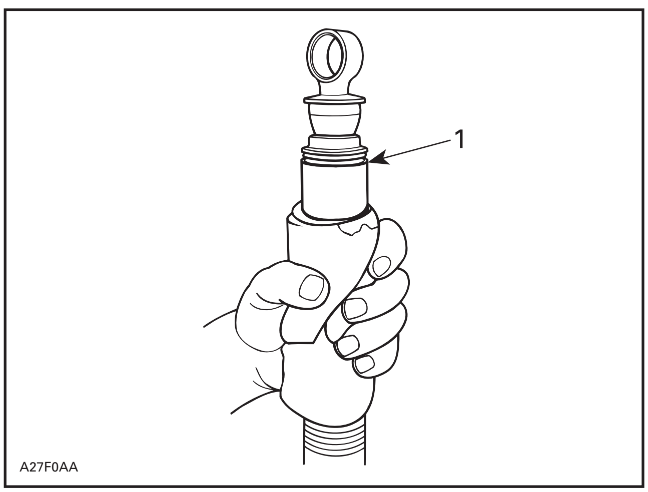
TYPICAL

Holding damper assembly in bench vise with aluminum jaw protectors, unthread seal assembly from damper body using a 32 mm (1.25 in) spanner wrench. This assembly uses a right hand thread.



With the seal assembly removed, slowly lift and remove damper rod assembly from the damper body.

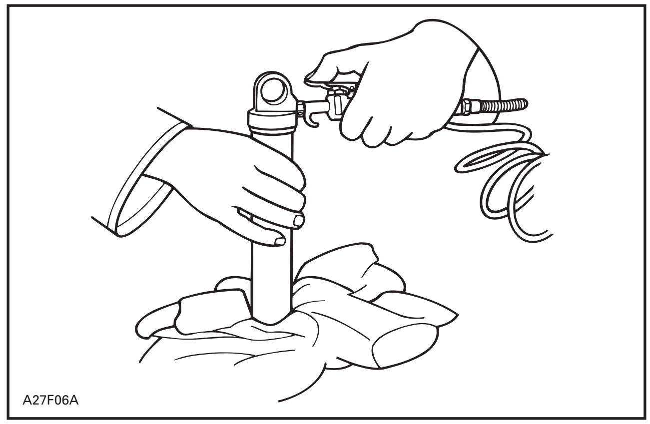
NOTE: Remove damper rod assembly slowly to reduce oil spillage and prevent piston seal damage by damper body threads. Wrap the damper body with a shop cloth to capture possible overflow oil while removing the damper piston.



1. Oil flows

Discard old oil into storage container. Never reuse damper oil during shock rebuild.

Remove Schrader valve core. Using compressed air pressure, carefully remove floating piston from damper body. Hold shop cloth over damper body opening to catch released floating piston. Allow room for floating piston to leave damper body.



TYPICAL

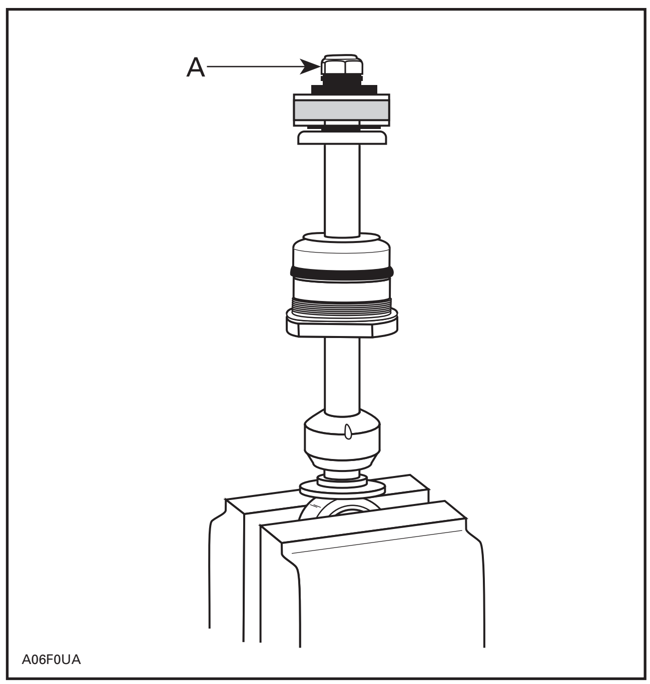
⚠ WARNING

Whenever using compressed air, use an O.S.H.A. approved air gun and wear protective eye wear.

Thoroughly clean, with a typical cleaning solution, and blow dry using low pressure air. Carefully inspect the damper body for any imperfections or signs of wear in the damper bore.

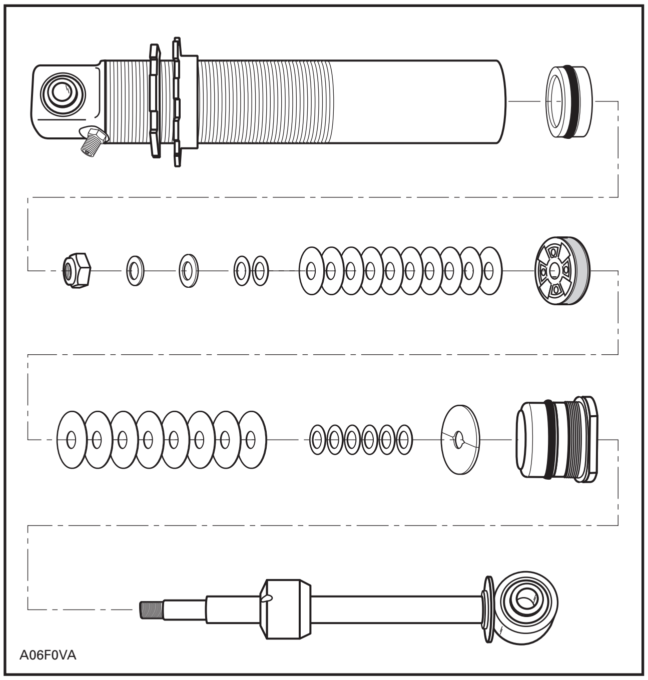
Replace damper body if wear is identified.

Holding the damper rod assembly in a bench vise, begin piston and valve removal.



A. Remove damper nut

Always arrange parts removed in the sequence of disassembly.



NOTE: As a general rule we suggest replacing the damper rod lock-nut after 4 rebuilds to ensure good locking friction and use Loctite 271 each time.

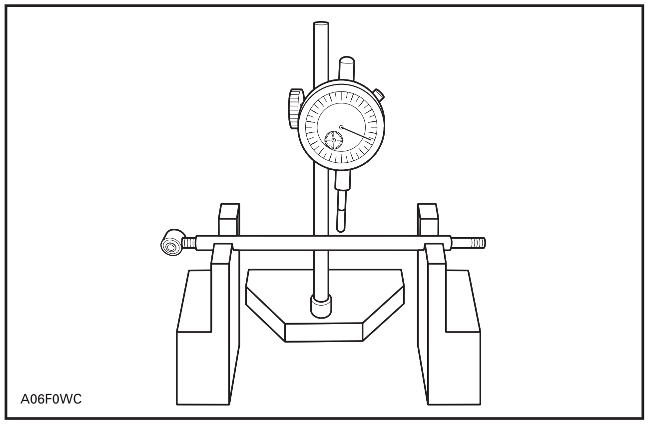
NOTE: If revalving is to be done, it is imperative that you identify the original shim pack (size and number of shims). The seal carrier need not be removed if only revalving is to be done.

Shims can be measured by using a vernier caliper or a micrometer.

NOTE: All shims should be carefully inspected and any bent or broken shims must be replaced for the shock to function properly.

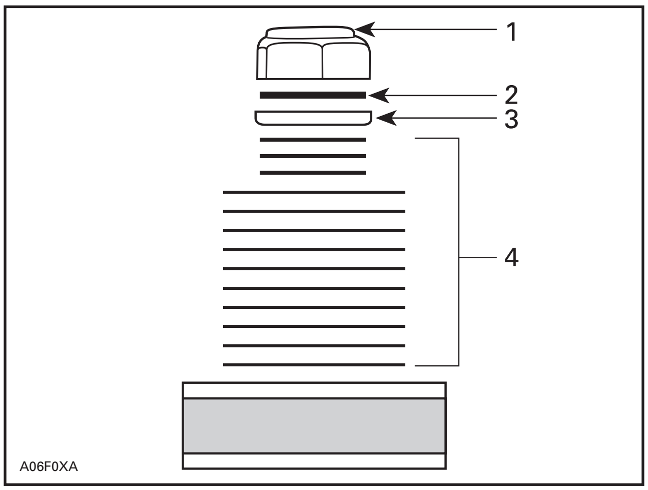
The damper rod is constructed of a plated shaft design. This damper shaft must be inspected for any visible wear on the surface of the damper rod.

Another check that must be completed if damper seal leakage has been noticed, is damper rod run-out. This damper rod run out must not exceed 025 mm (.001 in).



MAXIMUM DEFLECTION 0.025 mm (.001 in)

After the new or replacement shim pack has been selected, reassemble in the reverse order of disassembly. Torque piston nut 11-13 N•m (96-108 lbf•**in**). Use 271 Loctite.



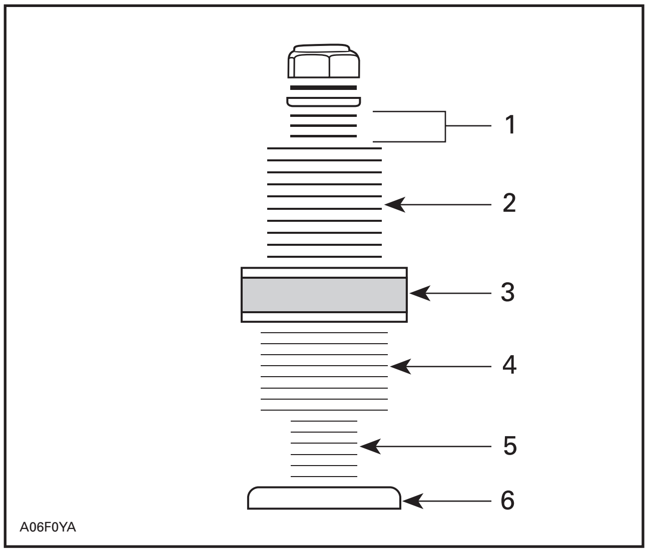
1. *Damper nut*
2. *Spacer*
3. *Washer*
4. *Shim pack*

CAUTION: The damper rod nut can only be reused 4 times, then, must be replaced. Do not substitute this part for non – O.E.M. use Loctite 271 on nut each time.

This spacer washer(s) (P/N 414 888 309) must be used as shown to ensure damper rod nut does not bottom out or contact shaft threads.

Rebound valve stopper with round edge facing shim stack.

NOTE: Rebound shim stack must not reach into threads of damper shaft. Washer under damper shaft nut is used to prevent damper shaft nut from bottoming on threads.



1. *Rebound dampening shim pack*
2. *Rebound dampening shim pack*
3. *Piston*
4. *Compression dampening shim*
5. *Compression dampening shim pack*
6. *Stopper*

Rebound

A minimum of 0.203 mm (.008 in) clearance must be allowed between shim stack and rebound valve stopper. Use at least one shim of 12 × .203 mm.

Whenever tuning for more rebound damping always use 26 mm (1.02 in) shims against piston to properly close piston orifice holes. More thin shims will offer more control than a few thick shims of the same overall thickness.

NOTE: When tuning for less dampening it is important to remember, never use less than 3-26 mm (1.02 in) shims against piston. This will guard against fatigue breakage.

Piston options include 5 pistons; 0, 1, 2, 4 and 6 slits for rebound dampening bleeds.

Compression

Whenever tuning for more compression dampening always use 30 mm (1.18 in) shims against piston to properly close piston orifice holes. Two thin shims will offer more control than one thick shim of the equal thickness.

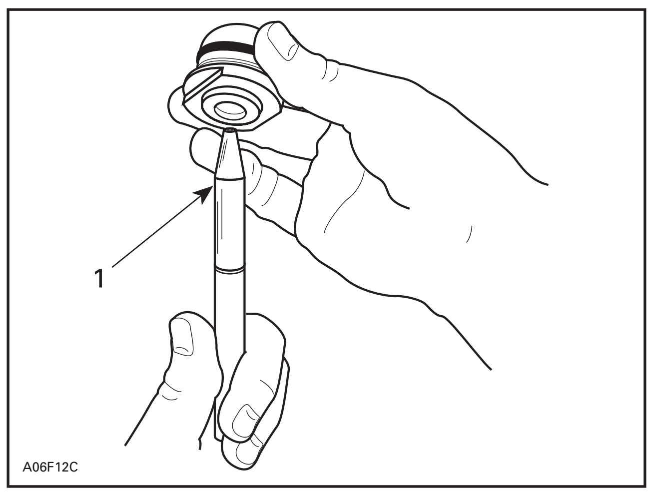
NOTE: When tuning for less dampening it is important to remember, never use less than 3 shims against piston. This will guard against fatigue breakage.

Fewer spacer shims will result in more high speed dampening. A minimum of 0-114 mm (.0045 in) clearance should be allowed between shim stack and compression valve stopper. Use at least one shim of 12 × .114.

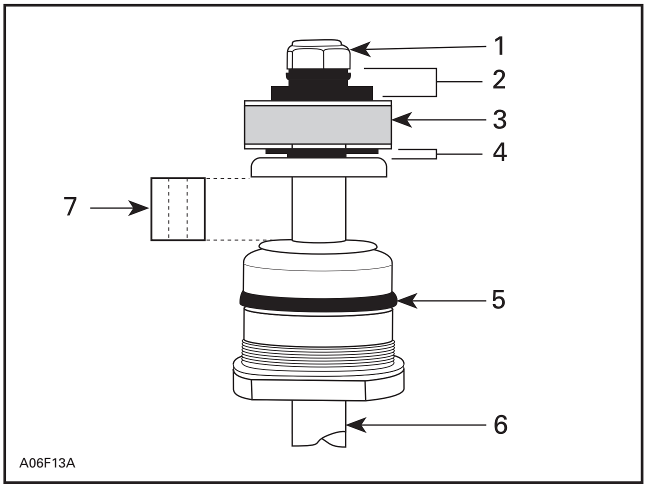
If the seal carrier assembly is replaced, use seal pilot (P/N 529 026 500) to guide seal over damper shaft. Lubricate seal carrier guide pilot before use.

CAUTION: Failure to use seal pilot will result in seal damage.

Reassemble damper rod assembly, taking care to properly assemble shim packs as required for your dampening needs Ensure that the shaft piston is installed with the slits/larger intake holes facing the rebound shim stack.



1. *Pilot (P/N 529 026 900)*



1. Damper nut torque 11-13 N•m (96-108 lbf•**in**) use Loctite 271
2. Rebound shim pack
3. Piston
4. Compression shim pack
5. O-ring visual inspection seal carrier assembly
6. Damper rod
7. Optional travel restriction spacer kit (P/N 861 744 200)

Kit includes:

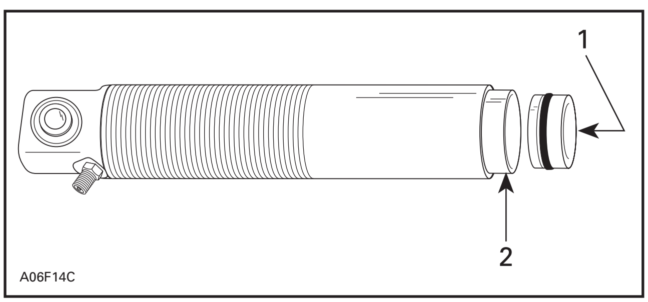
2 x 26 mm long spacer

1 x 48 mm long spacer

2 x 60 mm long spacer

Reinstall floating piston into damper body (ensure that Schrader valve core has been removed). Use molybdenum disulfide grease (example: molykote paste (P/N 413 703 700) or silicone grease Dow Corning MS4 (P/N 420 897 061) to ease O-ring past damper body threads with floating piston pilot (P/N 529 026 600).

CAUTION: Failure to install IFP correctly could result in shock damage.

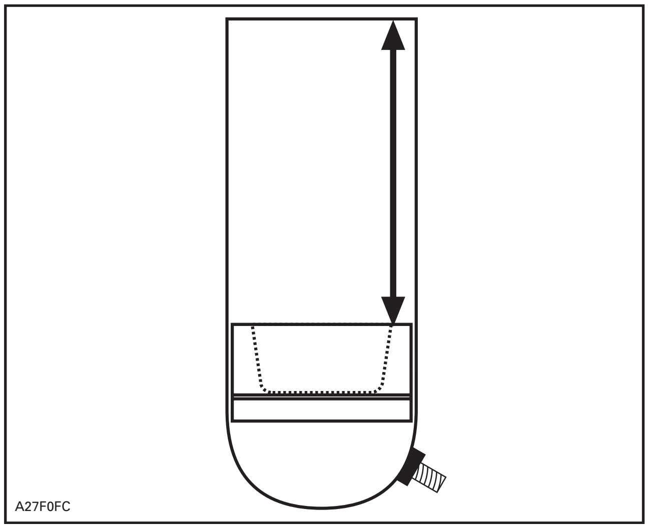


1. Push (slowly) by hand
2. Floating piston guide (P/N 529 026 600)

NOTE: Lubricate inside of piston guide with molykote GN paste (P/N 413 703 700) or MS4 silicone grease (P/N 420 897 061).

Install floating piston to the proper depth.

On all HPG take apart shocks from 1996 on. The floating piston is installed hollow side up.



Required distance for floating piston installation.

NOTE: If the floating piston is installed too far into the damper body, light air pressure through Schrader valve (with core removed) will move piston outward.

NOTE: Reinstall Schrader valve core after IFP has been installed at correct height and before adding oil.

⚠ WARNING

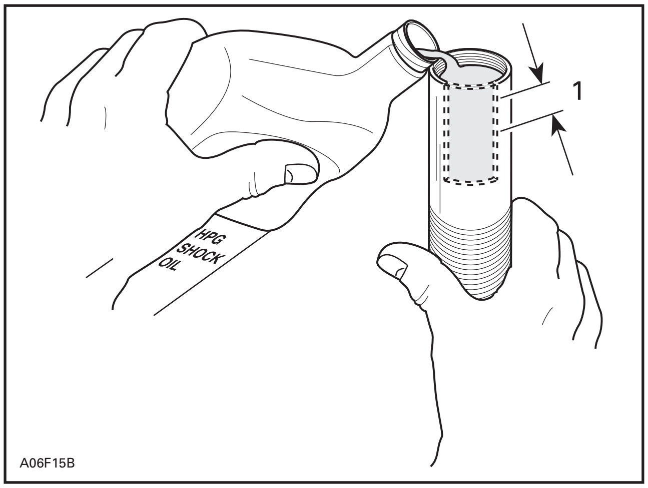
Whenever using compressed air exercise extreme caution, cover damper opening with shop cloth to reduce chance of possible injury.

CAUTION: Moisture laden compressed air will contaminate the gas chamber and rust floating piston.

⚠ WARNING

Always wear protective eye wear whenever using compressed air.

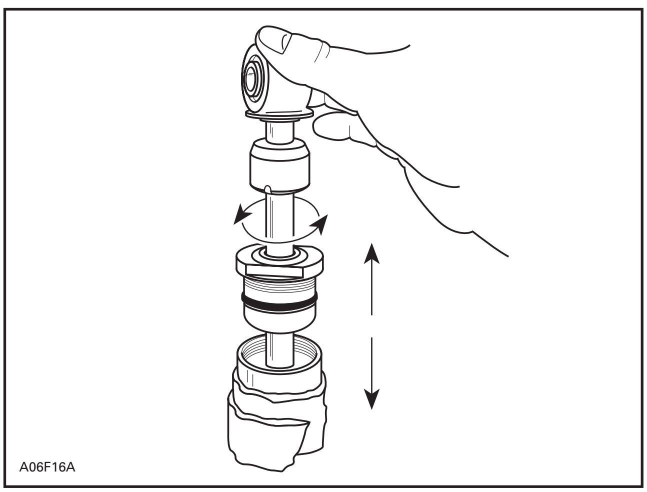
Fill the shock with Bombardier HPG shock oil (P/N 413 711 806) to approximately 10 mm (.393 in), from the base of seal carrier threads.



1. Fill to 10 mm (.393 in)

NOTE: Although we do not measure the exact amount of oil added to the damper, approximately 106 mL (3.58 oz U.S.) will be used.

Carefully insert damper rod into the damper body. Install damper rod assembly into the damper body. Lightly oil damper piston seal ring with shock oil to ease installation.



NOTE: Some shock oil will overflow when installing damper. Wrap damper with shop cloth to catch possible overflow oil.

CAUTION: Use care when passing piston into damper body at damper body threads.

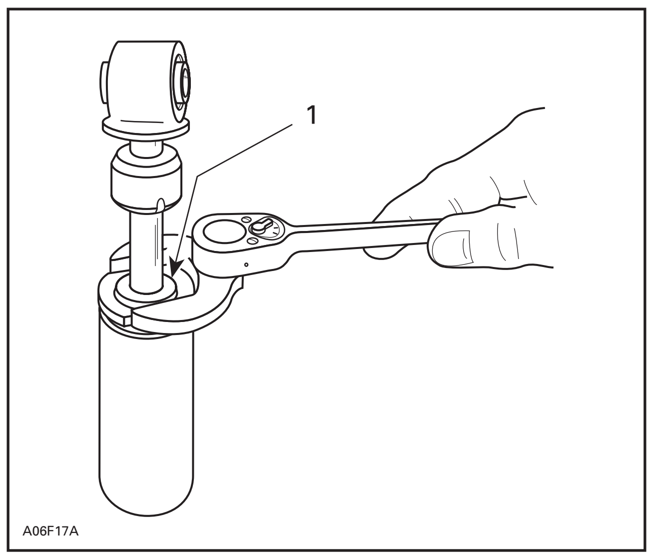
Slight oscillation of damper rod may be required to allow piston to enter damper body bore.

Slowly push piston into damper body. Slight up and down movement may be required to allow all air to pass through piston assembly. The gentle tapping of a small wrench, on the shock eye, may help dislodge air trapped in the submersed piston. Be careful not to drive the shaft any deeper into the oil than is necessary to just cover the shim stack.

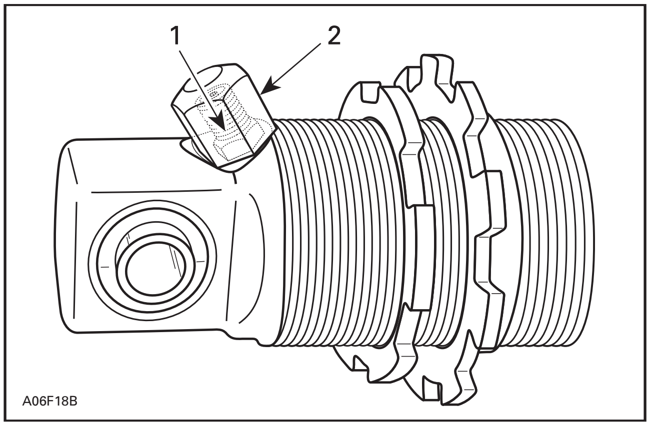
NOTE: Fast installation of the damper rod may displace the floating piston from its original position. This must not occur if the damper is expected to perform as designed.

With damper rod piston into-oil, TOP OFF damper oil volume. Oil level should be to damper body thread base.

Seal carrier assembly can now be threaded into damper body. This should be done slowly to allow weapage of oil and to minimize IFP displacement. After the seal carrier is fully in place avoid pushing the shaft into the body until the nitrogen charge is added.



1. Torque seal carrier to 88-89 N•m (64-72 lbf•ft)



1. *Schrader valve 1.5-2 N•m (13-17 lbf•**in**)*
2. *Schrader cap 5-6.5 N•m (44-57 lbf•**in**)*

Adding Gas Pressure

Nitrogen (N_2) can now be added to damper body.

NOTE: Never substitute another gas for nitrogen. Nitrogen has been selected for its inert qualities and will not contaminate the gas chamber of the shock.

Preset your pressure regulator to 2070 kPa (300 PSI) nitrogen (N_2), this gas pressure will restore the correct pressure for your damper.

CAUTION: Do not exceed the recommended pressure values.

When removing and retightening the Schrader valve acorn nut use minimal torque. When the cap is over tightened and subsequently removed it may prematurely break the seal of the Schrader valve to the shock body and cause a loss of nitrogen charge without being noticed. If you suspect this has happened then recharge the shock as a precaution. Inspect the acorn cap before installation to ensure that the internal rubber gasket is in its proper position.

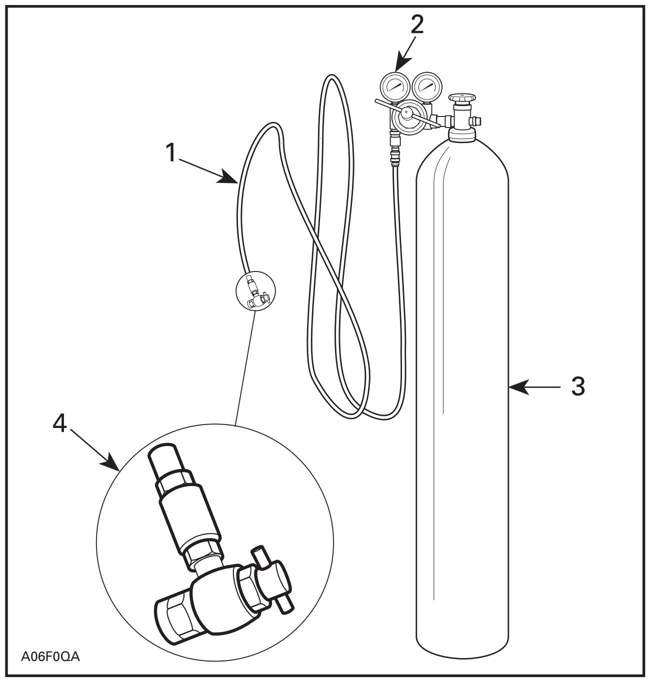
⚠ WARNING

Whenever working with high pressure gas, use eye wear protection. Never direct gas pressure toward anybody.

NOTE: Carefully inspect damper for gas or oil leaks. Any leaks must be corrected before continuing.

Damper gas pressure cannot be confirmed by using a pressure gauge. The volume of gas in the shock is very small, and the amount lost during gauge installation will lower the pressure too much and require refilling.

After recharging is complete and before installing the spring the rebuilt shock should be bench-tested. Stroke the shock to ensure full travel and smooth compression and rebound action. If the shaft moves in or out erratically this could indicate too much air is trapped inside. If the shaft will not move or has partial travel then it may be hydraulically locked. In either event the shock must be rebuilt again. Pay particular attention to the placement of the IFP, quantity of oil and shim stack/piston assembly.



1. *Automotive type air pressure hose*
2. *2 stage regulator, delivery pressure range 2070 kPa (300 PSI)*
3. *High pressure cylinder filled with industrial grade nitrogen*
4. *Valve tip (P/N 529 035 570)*

Reinstall damper spring retainer, then your spring. Next, thread the spring pre-load rings up to the spring. Set pre-load according to recommended spring length specifications. Your damper is now ready for reinstallation to your snowmobile.

HPG T/A Shock Spare Parts

SHIMS

P/N	SIZE (mm)	MOQ (minimum order quantity)
415 039 100	30 × .254	5
414 888 318	30 × .203	15
414 888 319	30 × .152	1
414 888 320	28 × .203	5
414 888 321	28 × .152	5
415 039 000	26 × .254	5
414 888 322	26 × .203	5
414 888 323	26 × .152	50
414 888 324	22 × .203	5
414 888 325	22 × .152	5
414 888 326	20 × .203	5
414 888 327	20 × .152	5
414 888 328	20 × .144	5
414 888 329	18 × .203	5
414 888 330	18 × .152	5
414 888 331	16 × .254	10
414 888 332	16 × .203	10
414 888 333	16 × .152	10
415 038 900	16 × .114	10
414 888 334	15 × .254	10
414 888 335	15 × .203	10
414 888 336	15 × .152	10
414 888 337	15 × .114	10
414 888 338	12 × .203	10
414 888 339	12 × .152	10
415 038 800	12 × .114	10
414 888 340	21 × .114	10
414 888 341	24 × .114	10

PISTONS

P/N	SIZE	MOQ (minimum order quantity)
414 888 304	0 slit	1
414 888 305	2 slits	2
414 888 306	4 slits	1
414 888 307	6 slits	1
	1 slit	

C-46 Shock Spare Parts

REAR SHOCK SHIMS

P/N	SIZE (mm)	MOQ (minimum order quantity)
503 189 011	22 × .114	5
503 189 012	22 × .152	5
503 189 013	22 × .203	5
503 189 014	22 × .254	5
503 189 015	22 × .305	5
503 189 016	24 × .114	5
503 189 017	24 × .152	5
503 189 018	24 × .203	5
503 189 019	24 × .254	5
503 189 020	24 × .305	5
503 189 021	26 × .114	5
503 189 022	26 × .152	5
503 189 023	26 × .203	5
503 189 024	26 × .254	5
503 189 025	26 × .305	5
503 189 026	28 × .114	5
503 189 027	28 × .152	5
503 189 028	28 × .203	5
503 189 029	28 × .254	5
503 189 030	28 × .305	5
503 189 031	30 × .114	5
503 189 032	30 × .152	5
503 189 033	30 × .203	5
503 189 034	30 × .254	5
503 189 035	30 × .305	5
503 189 036	36 × .152	5
503 189 037	36 × .203	5
503 189 038	36 × .254	5
503 189 039	40 x 114	5
503 189 040	40 x 203	5
503 189 041	40 x 254	5

PISTONS

P/N	SIZE	MOQ (minimum order quantity)
503 189 004	0.0	1
503 189 003	1.2	1
503 189 002	1.7	1
503 189 001	2.0	1

Shock Parts

2002 MX Zx 440

BOMBARDIER P/N	DESCRIPTION
REAR SHOCK (503 189 780) PARTS	
503 190 036	hose clamp
503 190 037	reservoir
503 190 038	rod assembly with upper mount
503 190 039	cylinder head assembly 9/16
503 190 040	floating piston assembly
503 190 041	valve end cap sub-assembly
503 190 042	rod spacer
CENTER SHOCK (503 189 779) PARTS	
503 190 104	rod assembly with upper mount assembly and bumper and ice-scraper
503 190 043	cylinder head assembly
503 190 044	SS braided hose
503 190 045	male elbow
503 190 046	45 straight thread elbow
503 189 998	spring retainer nut
503 190 047	floating piston sub assembly
503 190 048	reservoir end cap assembly
503 190 049	reservoir top cap assembly
503 190 050	reservoir cylinder

BOMBARDIER P/N	DESCRIPTION
CALIBRATION PARTS	
503 190 051	reservoir circlip
503 190 052	monotube screw
503 190 053	O-ring for monotube screw
503 190 054	monotube screw
503 190 055	monotube screw
503 190 056	pressure valve assembly
503 190 057	pressure valve assembly
503 190 058	thin colllar stover nut
503 190 059	monotube washer
503 190 060	monotube washer
503 190 061	.700 x .004 deflection disc
503 190 062	.700 x .006 deflection disc
503 190 063	.700 x .008 deflection disc
503 190 064	.700 x .010 deflection disc
503 190 065	.700 x .012 deflection disc
503 190 066	.700 x .015 deflection disc
503 190 067	.800 x .004 deflection disc
503 190 068	.800 x .006 deflection disc
503 190 069	.800 x .008 deflection disc
503 190 070	.800 x .010 deflection disc
503 190 071	.800 x .012 deflection disc
503 190 072	.800 x .015 deflection disc
503 190 073	.900 x .004 deflection disc
503 190 074	.900 x .006 deflection disc
503 190 075	.900 x .008 deflection disc
503 190 076	.900 x .010 deflection disc
503 190 077	.900 x .012 deflection disc

2002 MX Zx 440

BOMBARDIER P/N	DESCRIPTION
CALIBRATION PARTS	
503 190 078	.900 x .015 deflection disc
503 190 079	1.00 x .006 deflection disc
503 190 080	1.00 x .008 deflection disc
503 190 081	1.00 x .010 deflection disc
503 190 082	1.00 x .012 deflection disc
503 190 083	1.00 x .015 deflection disc
503 190 084	1.10 x .006 deflection disc
503 190 085	1.10 x .008 deflection disc
503 190 086	1.10 x .010 deflection disc
503 190 087	1.10 x .012 deflection disc
503 190 088	1.10 x .015 deflection disc
503 190 089	1.25 x .006 deflection disc

BOMBARDIER P/N	DESCRIPTION
503 190 090	1.25 x .008 deflection disc
503 190 091	1.25 x .010 deflection disc
503 190 092	1.25 x .012 deflection disc
503 190 093	1.25 x .015 deflection disc
503 190 094	1.30 x .006 deflection disc
503 190 095	1.30 x .008 deflection disc
503 190 096	1.30 x .010 deflection disc
503 190 097	1.30 x .012 deflection disc
503 190 098	1.30 x .015 deflection disc
503 190 099	monotube piston (blank)
503 190 100	monotube piston (.063)
503 190 101	monotube piston (.075)
503 190 102	gas fill tool kit
503 190 103	shock oil (blue)

	MX Z STD/ADRENALINE		MX Zx PACK		SUMMIT X	
Front	rebound 4 x 26 x .152 1 x 12 x .114 2 x 26 x .152 1 x 12 x .203 Piston = 2 slits IFP = 186 mm	compression 4 x 30 x .152 1 x 15 x .114 3 x 30 x .152 3 x 15 x .203	rebound 4 x 26 x.152 1 x 12 x.114 2 x 26 x .152 1 x 12 x 203 Piston = 2 slits IFP = 44.5 mm	compression 4 x 30 x .152 1 x 15 x .114 3 x 30 x .152 3 x 15 x .203	rebound 2 x 26 x.152 1 x 12 x .114 2 x 26 x .152 1 x 12 x .203 Piston = 2 slits IFP = 176 mm	compression 1 x 30 x .254 1 x 12 x .114 2 x 30 x .152 3 x 15 x .203
	Shock part # 505 070 733		Shock part # 503 070 876 Shock part # 503 070 878		Shock part # 503 070 753	
Center	rebound 4 x 26 x .203 1 x 12 x .254 Piston = 2 slits IFP = 132 mm	compression 4 x 30 x .203 1 x 15 x .114 2 x 30 x .203 3 x 15 x .203	rebound 4 x 26 x .203 1 x 12 x .254 Piston = 2 slits IFP = 128 mm	compression 4 x 30 x .203 1 x 15 x .114 2 x 30 x .203 3 x 15 x .203	rebound 4 x 26 x .203 1 x 12 x .254 Piston = 6 slits IFP = 134 mm	compression 6 x 30 x .152 1 x 12 x .114 6 x 30 x .152 3 x 12 x .203
	Shock part # 503 819 877		Shock part # 503 189 768		Shock part # 503 819 891	
Rear	rebound 10 x 26 x .203 1 x 12 x .203 Piston = 2 slits IFP = 189 mm	compression 5 x 30 x .203 1 x 12 x .114 4 x 30 x .203 3 x 12 x .203	rebound 7 x 36 x .203 1 x 20 x .305 Piston = 1.7 orifice IFP = 188 mm	comression 6 x 40 x .125 1 x 24 x .114 3 x 40 x .152 4 x 24 x .203	rebound 11 x 26 x .203 2 x 12 x .203 Piston = 4 slits IFP = 187 mm	compression 2 x 30 x .152 1 x 12 x .114 4 x 30 x .152 2 x 12 x .203
	Shock part # 503 819 879		Shock part # 503 189 801		Shock part # 503 819 895	

IFP: Internal Floating Piston

2002 MX Zx 440 Shock Calibration

	FRONT	CENTER	REAR
COMPRESSION	30 x .152 x 6	1.250 x .015	.900 x .006
	18 x .152 x 1	1.100 x .015	1.300 x .015
	30 x .203 x 4	.800 x .004	1.300 x .015
	24 x .114 x 1	1.300 x .015	
	20 x .114 x 1	1.300 x .015	
	16 x .114 x 1	.063 Piston Orifice	.076 Piston Orifice
REBOUND	26 x .152 x 6	1.100 x .008	1.100 x .010
	15 x .203 x 1	.700 x .010	.700 x .006
	Piston 1 slit		
	IFP 43.5 mm	IFP 48.3 mm	IFP 94 mm
BASE VALVE	4 slit washer		
	18 x .152 x 3		
	11 x .305 x 1		

Shock Calibration

MODEL	FRONT/SKI SHOCK	CENTER SHOCK	REAR SHOCK
2001 MX Zx 440 racing			
— Compression	3 x 30 x .152	5 x 30 x .203	4 x 40 x .203
	1 x 18 x .152	1 x 21 x .152	1 x 24 x .203
	5 x 30 x .203	5 x 30 x .254	5 x 40 x .254
	1 x 24 x .114	1 x 26 x .114	2 x 36 x .254
	1 x 20 x .114	1 x 24 x .114	1 x 26 x .114
	1 x 18 x .114	1 x 21 x .114	1 x 30 x .254
— Rebound	8 x 26 x .152	1 x 26 x .152	9 x 36 x .254
	1 x 15 x .203	1 x 21 x .114	1 x 24 x .203
	Piston - 3 slits	7 x 26 x .254	Piston - 2.0
	IFP 44.5 mm	1 x 15 x .152	IFP 190 mm
		Piston - 4 slits	
		IFP 130 mm	
2001 MX Z std/adrenaline			
— Compression	4 x 30 x .152	6x 30 x .203	4 x 30 x .203
	1x 15 x .114	2 x 15 x .203	1 x 15 x .114
	3 x 30 x .152		3 x 30 x .203
	3 x 15 x .203		3 x 15 x .203
— Rebound	2 x 26 x .152	6 x 26 x .203	10 x 26 x .203
	1 x 12 x .114	1 x 12 x .254	1 x 12 x .254
	2 x 26 x .152	Piston - 2 slits	Piston - 2 slits
	1 x 12 x .203	IFP 130 mm	IFP 183 mm
	Piston - 2 slits		
	IFP 172 mm		
2001 MX Z (X packages)			
— Compression	4 x 30 x .152	7 x 30 x .152	4 x 40 x .203
	1 x 15 x .114	1 x 15 x .152	1 x 24 x .203
	3 x 30 x .152	4 x 30 x .152	3 x 40 x .152
	3 x 15 x .203	3 x 15 x .203	2 x 24 x .203
— Rebound	2 x 26 x .152	4 x 26 x .203	9 x 36 x .203
	1 x 12 x .114	1 x 12 x .203	1 x 24 x .203
	1 x 12 x .203	Piston - 2 slits	Piston - 2 slits
	Piston - 2 slits	IFP 130 mm	IFP 190 mm
	IFP 44.5 mm		
2001 SUMMIT (X packages)			
— Compression	2 x 30 x .203	4 x 30 x .152	8 x 30 x .152
	1 x 12 x .114	1 x 12 x .114	3 x 12 x .203
	1 x 30 x .203	4 x 30 x .152	
	3 x 15 x .203	3 x 12 x .203	
— Rebound	2 x 26 x .152	4 x 26 x .203	11 x 26 x .203
	1 x 12 x .114	1 x 12 x .254	2 x 12 x .203
	1 x 12 x .203	Piston - 6 slits	Piston - 4 slits
	Piston - 2 slits	IFP 130 mm	IFP 183 mm
	IFP 157 mm		

MODEL	FRONT/SKI SHOCK	CENTER SHOCK	REAR SHOCK
2000 MX Zx			
— Compression	3 x 30 x .152	3 x 30 x .203	4 x 40 x .203
	1 x 16 x .152	1 x 19 x .152	1 x 24 x .203
	5 x 30 x .203	5 x 30 x .254	5 x 40 x .254
	1 x 24 x .114	1 x 28 x .254	2 x 36 x .254
	1 x 21 x .114	1 x 26 x .114	1 x 30 x .254
	1 x 18 x .114	1 x 21 x .114	1 x 26 x .114
	3 slit piston	4 slit piston	Piston orifice 2.0
— Rebound	8 x 26 x .152	1 x 26 x .152	9 x 36 x .254
	1 x 15 x .203	1 x 21 x .114	1 x 24 x .203
	IFP 445 mm	7 x 26 x .254	IFP 190 mm
		1 x 15 x .122	
		IFP 130 mm	
2000 MX Z 500/600 CN/700			
— Compression	4 x 30 x .152	7 x 30 x .152	5 x 30 x .152
	1 x 15 x .114	1 x 15 x .152	1 x 15 x .114
	3 x 30 x .152	4 x 30 x .152	3 x 30 x .203
	3 x 15 x .203	3 x 15 x .203	3 x 15 x .203
	2 slit piston	2 slit piston	2 slit piston
— Rebound	2 x 26 x .152	4 x 26 x .203	6 x 26 x .203
	1 x 12 x .114	1 x 12 x .254	1 x 12 x .114
	2 x 26 x .152	IFP 130 mm	3 x 26 x .203
	1 x 12 x .203		1 x 12 x .203
	IFP 172 mm		IFP 183 mm
2000 MX Z 600 U.S.			
— Compression	7 x 30 x .152	7 x 30 x .152	5 x 30 x .152
	3 x 15 x .203	1 x 15 x .152	1 x 15 x .114
		4 x 30 x .152	3 x 30 x .203
		3 x 15 x .203	3 x 15 x .203
	2 slit piston	2 slit piston	2 slit piston
— Rebound	6 x 26 x .203	4 x 26 x .203	6 x 26 x .203
	1 x 12 x .203	1 x 12 x .254	1 x 12 x .114
	IFP 172 mm	IFP 130 mm	3 x 26 x .203
			1 x 12 x .203
			IFP 183 mm
2000 MACH Z			
— Compression	N.A.	4 x 30 x .203	12 x 30 x .152
		3 x 16 x .203	3 x 15 x .203
		4 slit piston	2 slit piston
		4 x 26 x .152	8 x 26 x .203
— Rebound		1 x 12 x .203	1 x 12 x .203
		IFP 138 mm	IFP
2000 SUMMIT			
— Compression	N.A.	N.A.	12 x 30 x .152
			3 x 15 x .203
			2 slit piston
			8 x 26 x .203
— Rebound			1 x 12 x .203
			IFP 169 mm

SHOCK CALIBRATION WORK SHEET

MODEL: ______________________ DATE: ______________

RIDING CONDITIONS: ______________________________

	FRONT	CENTER	REAR	OPTION
PISTON SLITS				
IFP HEIGHT				
COMPRESSION				
REBOUND				
SPRING				
PRELOAD				

NOTES: ______________________________

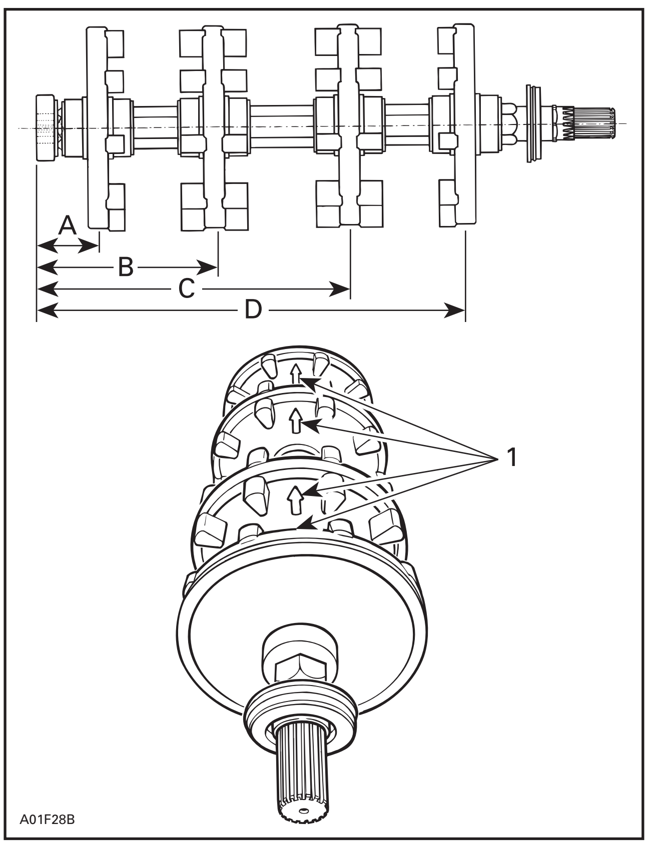
CHASSIS SET-UP

General

Reducing rolling resistance of a snowmobile is also an important area to explore when you are searching for the ultimate top speed. The horsepower required to overcome rolling resistance or drag increases approximately with the square of velocity so small reductions here can provide measurable improvements in top speed.

Good chassis set up starts with accurate alignment of the drive axle, countershaft, suspension system, and chassis. Use the following procedure to check your vehicle:

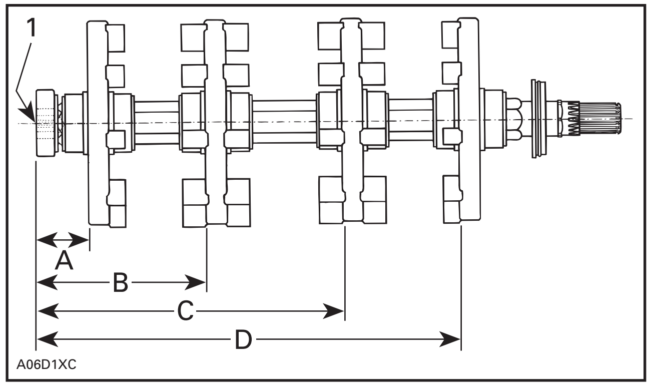
Remove the rear suspension, driven clutch, tuned pipe and muffler, track and drive axle. Check to see that the spacing of the drive sprockets is correct on the drive axle. The sprockets should be centered in the space between the rows of internal drive lugs on the track.



1. *Indexing marks aligned*
A. *65.8 mm (2-18/32 in)*
B. *159.3 mm (6-17/64 in)*
C. *282.3 mm (11-7/64 in)*
D. *375.8 mm (14-51/64 in)*

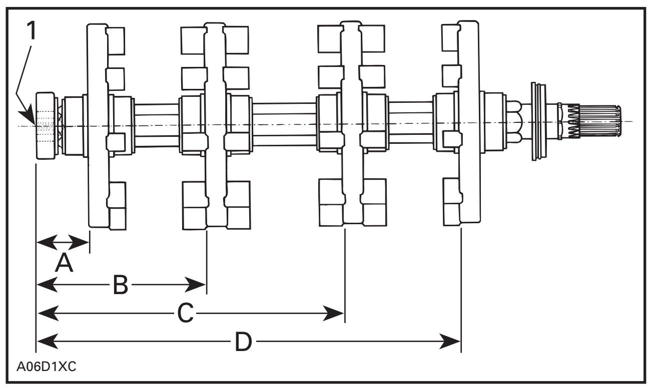
1995/1999 All S-Series DSA
1993/1997 All F-Series DSA

ZX Series



1. *Measure from end of drive axle*
A. *47.3 mm (1.862 in)*
B. *149.8 mm (5.898 in)*
C. *272.8 mm (10.740 in)*
D. *375.3 mm (14.776 in)*

CK3 Series



1. *Measure from end of drive axle*
A. *49 mm (1.929 in)*
B. *151.21 mm (5.953 in)*
C. *274.2 mm (10.795 in)*
D. *376.3 mm (14.815 in)*

Use a press or special tool (P/N 861 725 700) for shifting the sprockets. The sprocket indexing should also be checked. The maximum desynchronization is 1/16 inch (1.5 mm). The drive axle can be chucked in a lathe and spun to observe the sprocket "wobble" and run out. Wobble should not exceed 2 mm (.080 in). While this amount of wobble may look excessive, it does not affect performance. If wobble is more than allowed, the sprockets should be replaced.

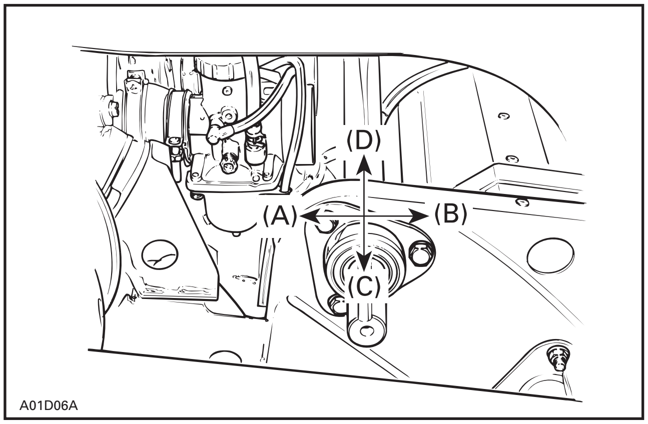
Maximum run out should not exceed 0.5 mm (.020 in). A maximum of 1 mm (.040 in) can be removed from the sprockets to true the diameter.

CAUTION: Do not remove more than 1 mm (.040 in) of material or the sprockets will start to go out of pitch with the track.

Reinstall the drive axle leaving the left end bearing housing off.

Loosen the left side countershaft eccentric bearing collar and slide the bearing retainer out so that the shaft end is free to locate itself in the support opening.

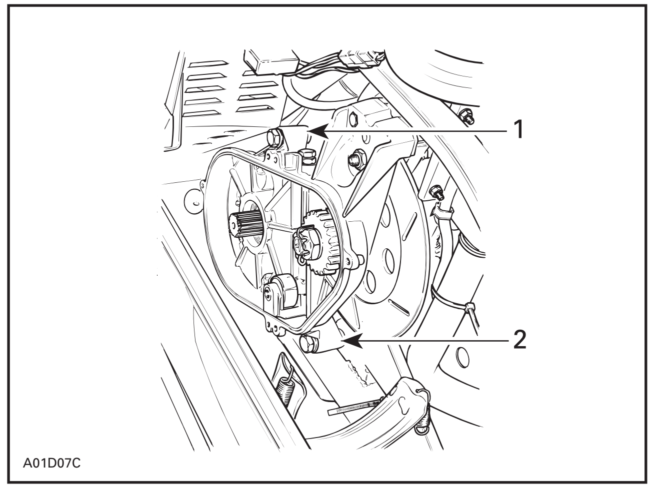
With both left shaft ends free, you can see if the shafts are centered in their bearing mount holes.



TYPICAL

NOTE: Shafts will have a tolerance in the bearing housings and the bearings them-selves. These tolerances can be felt by hand. The shafts should be mid-point in these tolerances when centered in the bearing mount holes. If not perfectly centered, the two upper chaincase bolts should be loosened and shims should be added between the chassis and chaincase as necessary to align the countershaft and drive axle in their bearing mount holes. Depending on the amount of shims added, it may be necessary to use longer chaincase bolts. Make certain the bolt is fully engaged in the nut when properly torqued.

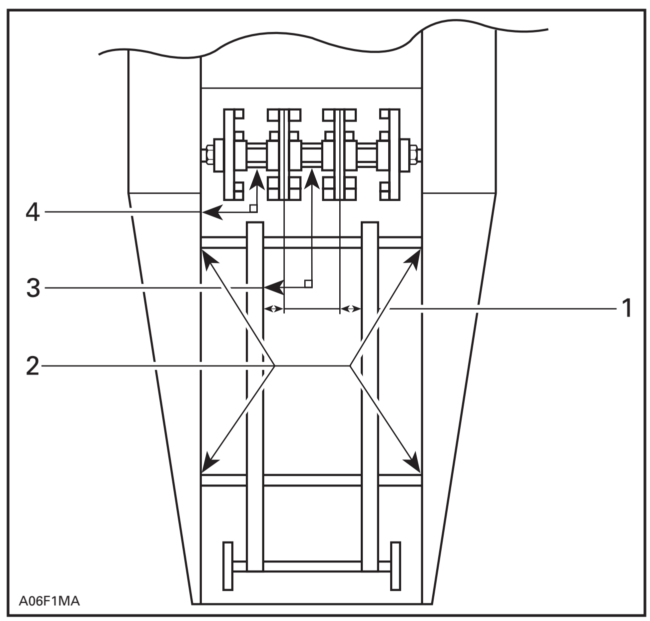
Now, reinstall the left end bearing housing. Using a large carpenters square, check to see that the drive axle is square (90°) with the tunnel. If not, slot the left end bearing housing holes and reshim the chaincase to square up the drive axle and the countershaft.



TYPICAL

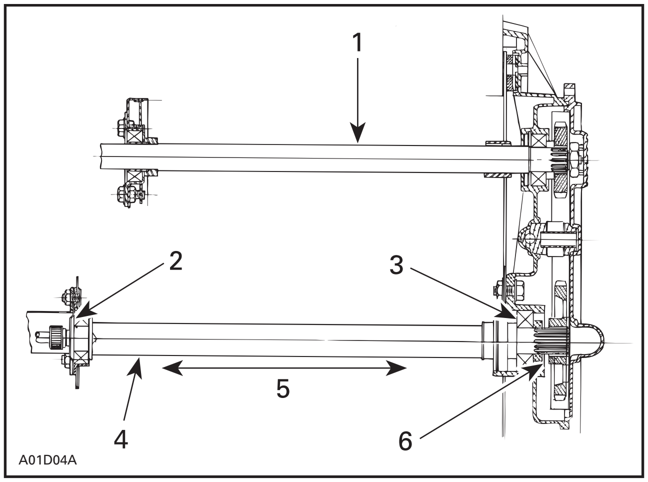
1. *Shim location*
2. *Shim location*

Reinstall the rear suspension and using a square check to see that the runners are square (90°) with the drive axle. If not, cut and shim the ends of the suspension cross tubes to perfectly align the runners and also remove any side-to-side movement. If the suspension must be shimmed, correlate the adjustment with the next step.



1. *Align runners with drive sprockets. Equal distance both sides. Shim drive axle to reduce end play Maximum end play = .060″ (ideal = less than .030″)*
2. *Cut ends of tubes and shim as required to align suspension and remove freeplay*
3. *Suspension square with drive axle*
4. *Drive axle square with tunnel*

Now check the axial play (side-to-side clearance) of the drive axle. The axle must not move more than 1.5 mm (.060 in) from side to side. Ideally, the axle has 0.25 – 0.50 mm (.010 – .020 in).



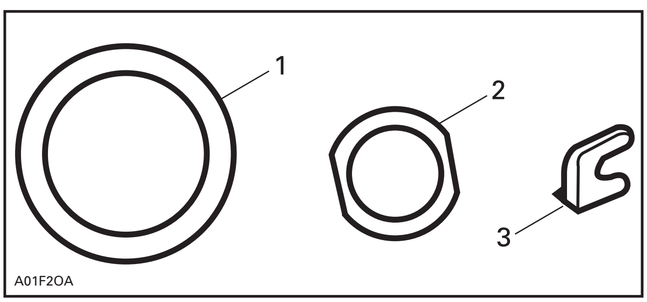
TOP VIEW

1. *Countershaft*
2. *Shim position on end bearing housing side*
3. *Shim position on chaincase side*
4. *Drive axle*
5. *Axial play*
6. *Shim between sprocket and spacer*

If the axle must be shifted left or right, note the direction and distance, and shim the axle as necessary.

Shims can be placed between the left side bearing and the end bearing housing to move the axle to the right or between the right side bearing and the chaincase to move the axle to the left.

NOTE: If shims are placed between the chaincase and the right side bearing, an equal thickness shim must be placed between the drive chain sprocket and the spacer on the axle.



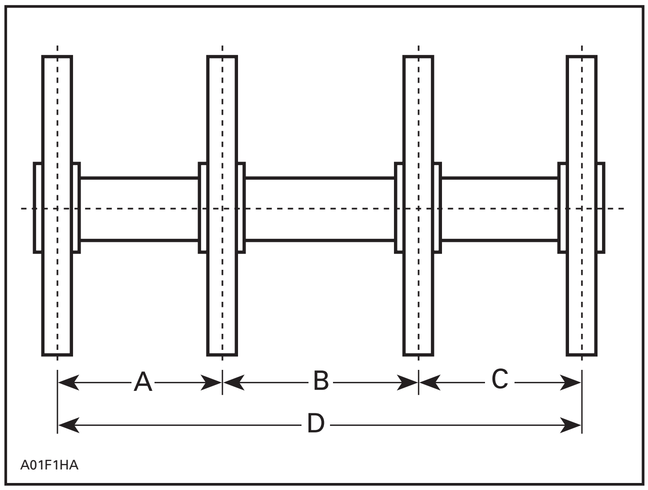
1. *(P/N 501 020 500)*
   Shim, drive axle end bearing housing 1.6 mm (.063 in) thick
2. *(P/N 506 041 400)*
   Shim, drive axle chaincase side 1.6 mm (.063 in) thick
3. *(P/N 504 039 800)*
   Shim, chaincase perpendicularity 0.5 mm (.020 in) thick

Rear Axle Modification

Heavily studded tracks combined with hard cornering put enormous loads on the track. To reduce the chance of derailing the track and to help spread the tensile loads of the track, a fourth idler wheel should be installed.

The two inner idlers should be placed so that they run between the left and right double rows of drive lugs. This will help maintain alignment of the track and lessen the chance of derailing.

Use the spacing shown in the drawing noting that the outer two idler wheels are in their original position.

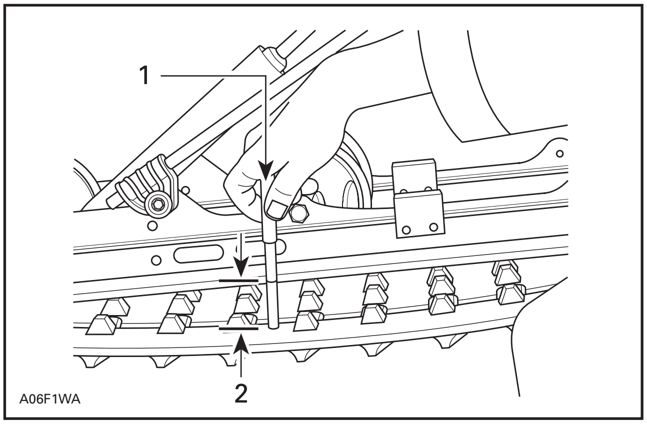


A. *101.5 mm (3-63/64 in)*
B. *123 mm (4-27/32 in)*
C. *101.5 mm (3-63/64 in)*
D. *326 mm (12.83 in)*

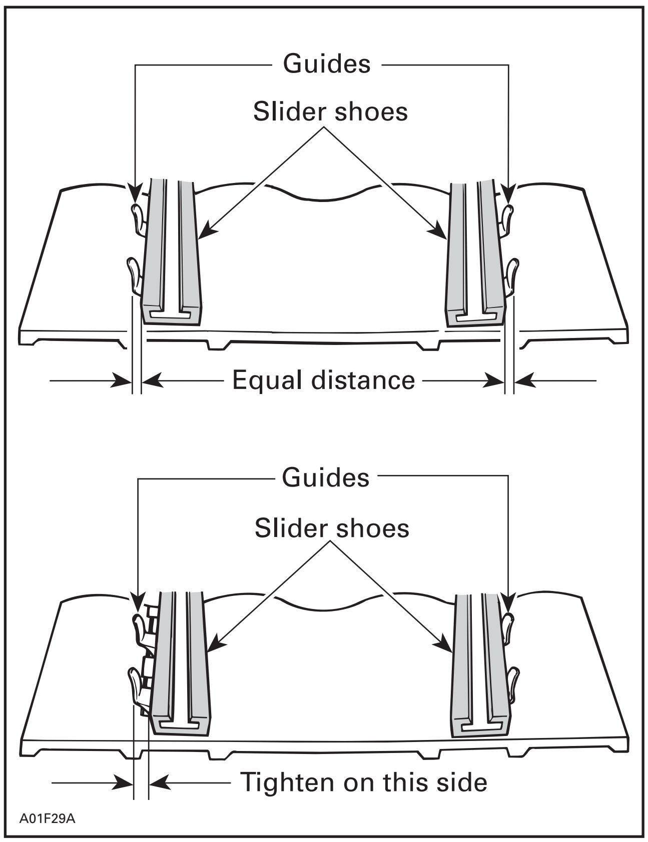
When you have reinstalled the track and suspension, make certain that all bolts attaching the suspension to the chassis are installed with high strength threadlocker (Loctite 271), and that bolts are properly torqued.

There are grease fittings on all moving parts of the suspension and they should be greased on a weekly basis with a quality, low temperature grease (P/N 413 711 500).

Finally, adjust the track tension and alignment. Track tension and alignment are most critical to top speed. Make certain the track is aligned so that you have equal clearance between the slider shoe and the track guides on each side of the snowmobile.



TYPICAL
1. *7.3 kg (16 lb)*
2. *Deflection*



For straight line racing, top speed can sometimes be increased by running the track a bit looser. Ratcheting of the drive sprockets during hard acceleration can occur if the track is too loose. Conversely, heavily studded tracks may need to be tighter to achieve top speed because the extra weight of the studs may cause the track to **balloon out** at high speeds.

NOTE: Track tension should be checked whenever major changes are made to the limiter strap length and/or ride height changes.

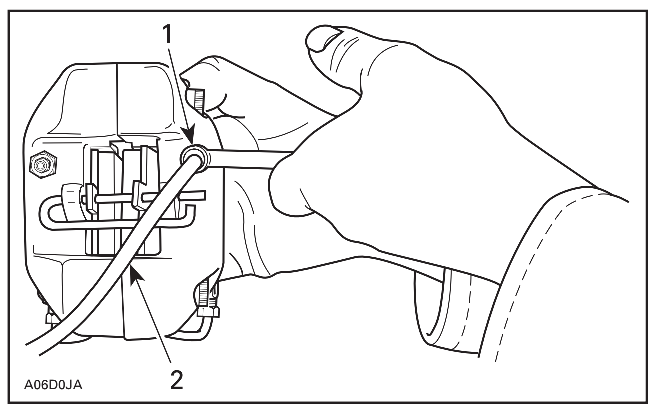
BRAKES

To achieve maximum top speed and proper brake functioning, it is important to make sure the brake disc is loose on the countershaft to allow the disc to float and remain centered between the brake pads. The shaft should be lubed to maintain the floating disc.

If extreme brake use is anticipated, use 3 inch diameter dryer hose (or equivalent) to route outside air directly from the hood vents to the brake area.

SKI-DOO hydraulic brake systems use DOT 4 brake fluid. For conditions where extreme brake heat is generated, DOT 5 fluid can be used. DOT 5 has a higher boiling point but it is more susceptible to moisture intrusion and should be changed on a regular basis. DOT 5 should not used for long, multi-day cross country racing where maintenance is minimal.

If the brakes become **spongy**, the system should be bled to remove any air bubbles. If the brake fluid is dark and/or cloudy, flush the complete system and refill with fresh brake fluid.



1. *Hold bleeder adaptor while opening bleeder*
2. *Clear hose to catch used brake fluid*

Pump a few time brake lever and while holding brade lever depressed, open bleeder and check for air to escape.

Repeat with the same bleeder until no air appears in hose.

Proceed the same way with the right side bleeder.

When refilling the injection oil container be careful not to overfill as excess oil can drop onto the brake disc and impregnate the brake pads. If this happens the brake pads should be replaced to ensure maximum braking performance.

AERODYNAMIC CONSIDERATIONS

Yes, aerodynamics are an important consideration in snowmobile design. The horsepower required to overcome aerodynamic drag increases according to the cube of the velocity. At speeds under 64 km/h (40 MPH), the aerodynamic considerations are not great, but when you approach the 160 km/h (100 MPH) mark, simply how you sit on the snowmobile can mean 6.4 km/h (4 MPH) in top speed.

Bombardier has spent many hours in the wind tunnel on the hood design, and has optimized the shape to fit the function. You cannot improve the shape of your snowmobile but you can reduce the frontal area of the snowmobile by lowering the ride height and by using the lowest windshield available.

The high windshield offers the rider good wind protection. That protection, however, translates into increased frontal area and more aerodynamic drag. If you are running at a local radar run with the high windshield on, you should sit upright behind the windshield. Crouching behind the windshield increases drag because of interruption of the air flow from the top of the windshield to the rider's back.

When the low windshield is fitted, the opposite is true, you should crouch behind the low windshield for best top speeds. When crouched behind the low windshield, there is an improvement in the aerodynamics compared to sitting upright behind the high windshield. That translates into an increase at top speed in a laboratory setting.

Because of the purity of the air flow in the wind tunnel, you should not expect this increase in normal running, but you can always expect a 3.2 – 4.8 km/h (2-3 MPH) improvement and even more when winds are still.

Lowering the vehicle a couple of inches can also improve top speed by 1-3 MPH.

ADJUSTING RIDE HEIGHT

A cross-country racer will want all the suspension travel you can for a rough snowcross-type event. But when racing a high speed event on a relatively smooth lake, giving up some of the suspension travel to lower the machine is advantageous. Lowering the machine, reducing the ride height, does 3 things for you:

1. Lowers the center of gravity of the machine; which improves cornering.
2. Reduces the frontal area of the sled; which improves aerodynamics.
3. Reduces the approach angle of the track; which reduces drag.

A person wanting to lower the machine for a short event like a radar run may simply chain or strap the machine down. Provided the course is quite smooth, this can work, but realize that strapping down the suspension preloads the springs highly and the ride will be very stiff. This technique is not recommended for most forms of racing.

The most common technique for lowering the machine is to use shorter springs or to shorten the existing springs by heating and collapsing a coil or 2 of the spring as needed. Realize that shortened springs will have very little preload when the suspension is in its "topped out" position, and it may be necessary to safety wire the spring collars into position, and use additional limiter devices like straps, chains or on HPG /A shocks, a spacer can be added internally to limit the extension of the shock.

NOTE: Some race organizations do not allow shortening springs so a proper optional short spring would be used.

Lowering the Front Suspension

Make limiter straps from standard rubber limiter strap material or link chain and go from shock bolt to shock bolt (longer shock bolts will be required). The length of the strap should be adjusted to obtain the desired ride height. Most rules require you to maintain 2 inches of suspension travel.

Shorter springs should be used to avoid excessive preload.

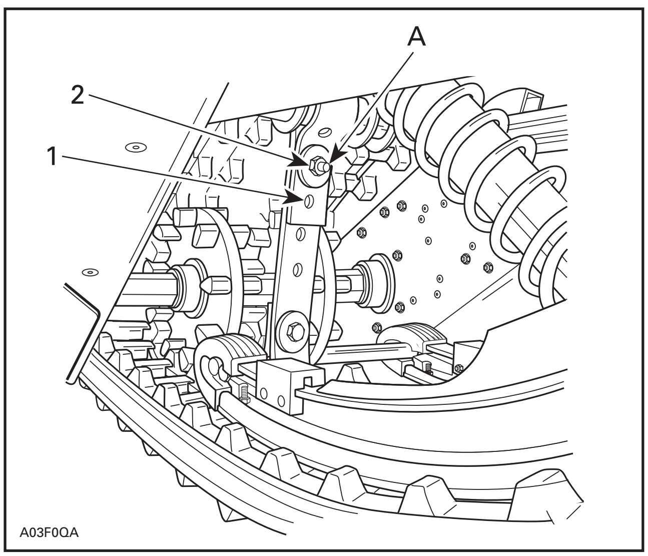
On vehicles with rebuildable shocks (HPG T/A), a spacer can be installed internally on the shock shaft to limit the shock extension. Spacers can be fabricated from 1 in O.D. aluminum round stock. (Refer to the shock rebuilding section for proper installation procedures).

The threaded adjusters can be loosened to provide the desired amount of spring preload.

Lowering the Rear Suspension

Option 1: The SC-10 rear suspension can be lowered by compressing the rear scissors to the desired ride height and installing a strap to maintain this height. Compressing the rear scissors adds a great deal of preload to the rear torsion springs. Use racing springs (P/N 486 099 100 LH) and (P/N 486 099 300 RH).

Option 2: It is also possible to lower the rear suspension on vehicles equipped with HPG T/A shocks, by using a spacer to limit shock extension. Use racing springs (P/N 486 099 100) and (P/N 486 099 300).



1. 1st hole
2. 2nd hole
A. 11 N•m (97 lbf•in)

Center

Shorten the limiter strap(s) to match the ride height of the front and rear and obtain the desired amount of weight transfer. New holes can be punched in rubber limiter straps. A shorter nylon limiter strap (P/N 414 955 300) is available for the vehicles with the strap and bolt style.

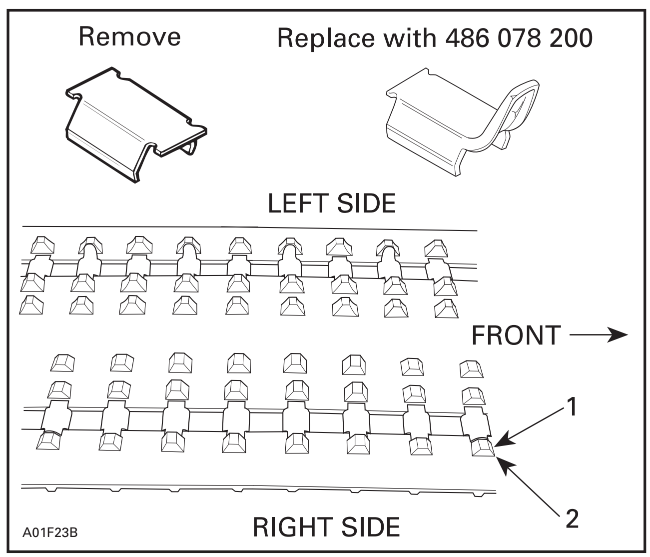
Quick Adjust Limiters may also be used (P/N 861 765 500) for the MX Zx. The Quick Adjust Limiter will allow you to shorten or lengthen the length of the limiter straps just by turning an adjuster knob.

On vehicles with HPG T/A shocks the threaded adjusters can be loosened to reduce the amount of spring preload. If less preload is desired or on vehicles with cam adjusters, shorter springs may be used to reduce excessive spring preload.

TRACK GUIDES

Additional taller track guides (P/N 486 078 200) should be installed when oval racing with a heavily studded track. These taller guides help prevent derailing without having to overly tighten the track. When in a turn, the side loads on the guides are extremely high and it is advantageous to reduce the load per guide by adding more of the guides.

All of the flat cleats should be removed from the right side of the track and replaced with guide cleats. (See drawing).



1. Standard
2. (P/N 486 078 200)

NOTE: When installing taller track guides or studs part (P/N 572 086 100), bushings should be installed inside the rear torsion springs on SC-10 rear suspensions. Track guide clearance should also be checked on top of the rear suspension A.C.M.

For ice lemans type racing where left and right hand corners are encounted, extra guides should also be installed on the left side of the track.

There are two special tools which greatly enhance the removal and addition of guide clips.

(P/N 529 028 700) Guide clip remover.

(P/N 529 008 500) Guide clip crimper.

TRACK STUDDING

⚠ WARNING

Installation of track studs is a modification not recommended. This modification may affect amongst others stopping distances and track strength. Studs may also be projected, thereby causing personal injuries to operator and/or bystanders. Bombardier disclaims liability for all damages and/or injuries resulting from use of the studs. Modifications of any Bombardier-made snowmobile voids the vehicle warranty and that such modifications may render use of the vehicle illegal in other than sanctioned racing events under existing federal, provincial and state regulations.

Traction control requires the installation of studs to the track so that you may improve the acceleration, direction and braking of the snowmobile on certain surfaces. Selection of the proper traction components is very important. It is also important to have the proper number of studs and to keep them sharp or replaced at all times.

For racing on hard ice, the single point stud is the most popular. If the ice gets a little softer, racers will add a variety of stamped studs. Always use Loctite when installing your studs.

Stud sharpness counts more than the number of studs. Fewer sharp, fresh studs work much better than a great many dull studs with a few new ones thrown in. Too many studs will keep the points from digging in and the sled will float, instead of hooking up.

If the studs do not prick your finger when you touch the tip they are not sharp enough. A small die grinder can be used to sharpen worn studs.

Place studs where pressure is concentrated on the edge of the track for turns, in the center of the track for acceleration and braking.

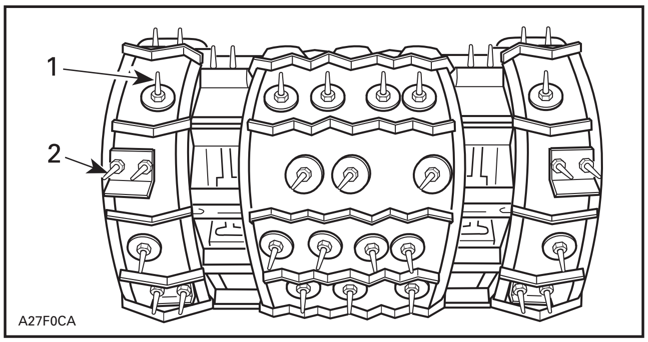
Hooker plates are welded to the track cleats and place the studs directly beneath the slider shoes for maximum pressure. The hooker setup is very hard on tracks, particularly the fiberglass reinforcing rods.

The other thing that must be kept in mind if hooker plates are used is that the studs will be directly in line with the heat exchanger protectors. The protectors must be removed and another system employed to protect the heat exchangers.

Depending upon machine setup, driver weight and driving characteristics, 250 to 300 penetrator studs will be required. The 121 inch track has 48 pitches. The most studs that can effectively be placed on each pitch is 7 — which means the maximum number of studs the track can hold is 336.

The drawing below shows a pattern of 6 studs alternating with 7 studs for a total of 312 studs. Try to keep studs from following the same line for 3 pitches.

NOTE: Refer to the appropriate section of this book for specific stud patterns for various types of racing.



TYPICAL
1. *6 stud row*
2. *7 stud row*

Most race associations sanctioning oval, snow cross and cross-country events limit the length of the studs to 3/8 inch above the high point of the track, while most drag and speed run associations allow a 3/4 inch limit. Rules do vary, however, and it is your responsibility to make certain your studs are legal. It is also necessary to protect the heat exchangers from damage from the studs.

Another item to keep in mind is the length of the threaded shank of the stud. Some stud patterns require that the stud pass under an idler wheel. If this is the case, you must be absolutely certain that the shank of the stud does not project beyond the flat face of the "T" nut. If necessary, grind the studs off.

CAUTION: Check condition of heat exchanger after every race.

Take the time and care to lay out your stud pattern carefully. And, make sure you write down what works best for you at certain tracks and various conditions.

NOTE: The track must be run in for ten (10) hours before holes are drilled to receive the studs. This must be done to stretch out all the elements of the track before any of the track cords are cut by the studding operation.

SLIDER SHOE LUBRICATION

When running a vehicle on surfaces that do not provide adequate lubrication for the slider shoes, the plastic will start to melt and stick to the track guide clips. This not only reduces the life of the slider shoes but it also substantially reduces vehicle speed. If rules allow, the most effective means to reduce slider shoe sticking is to apply a lubricant via a slide lubrication system.

The lube system should have a tank of approximately 1 to 1.5 gallons, a control valve, pump and a series of hoses and tees. A standard fuel pump can be used. The pump is operated by primary crankcase compression and can be connected to the fuel pump impulse line with a tee. Because the pump will operate whenever the engine is running, a control valve is used to conserve lubricant for the race.

When plumbing your system, run the supply line from the tank to the shutoff valve first. Make sure the valve is in a convenient location but protected from flailing arms and legs. Be certain to tie wrap the lines away from any rotating, vibrating or heated surfaces. The outputs from the pump should be routed through the tunnel just in front of and beneath the footrest.

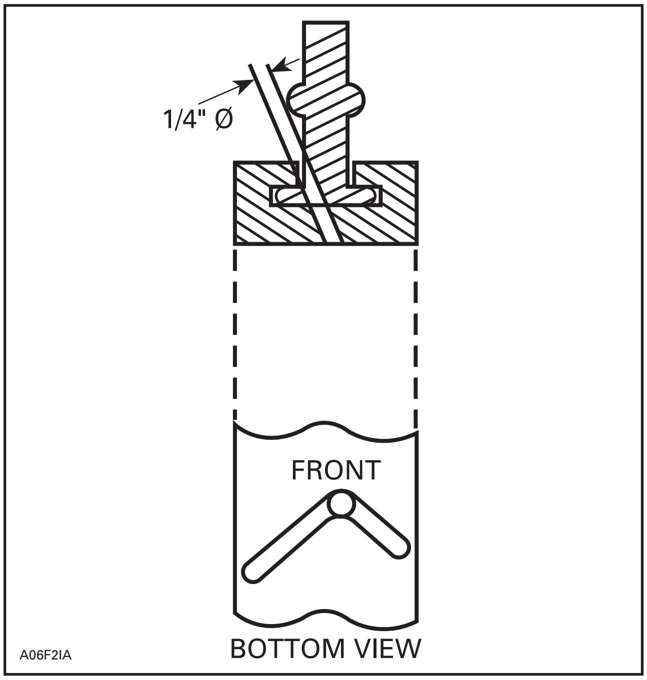
The 2 front nozzles should be located on each runner where the track just begins to touch the slider shoe. Drill a 1/4 inch diameter hole on the inner side of each runner down through the runner and slider shoe. Using red or green Loctite, insert a 1/4 inch diameter by 1-1/2 inch long roll pin in each location. Install the roll pin flush with the bottom of the aluminum runner. Do not let the pin protrude into the slider shoe. Prepare the slider shoes by grinding a "V" groove approximately 1/8 inch deep and 1/4 inch wide on the bottom side of the slider at each nozzle location. The grooves should run almost to the sides of the slider but not protrude on the sides. This will allow a better distribution of lubricant and make sure the lube supply does not become obstructed.

The 2 rear nozzles should be placed approximately half the remaining distance to the rear. For straight line racing, install the roll pins using the same procedure as above. For oval racing, mount the roll pins on the right side of both runners so the lubricant runs down the side of the slider shoe. This lubricates the sliders and the guiding portion of the track clips where side loading is highest during cornering. Be sure to clamp the side nozzles in place and secure all lines with locking ties.

Lubricant flow can be restricted at each nozzle by placing a Mikuni hex main jet inside each hose (about a no. 500). You cannot apply too much lube but you must last the race. Vary the restriction depending on your tank size and the length of the race.

PARTS LIST	QTY	P/N
Fuel pump	1	403 800 400
Impulse hose	1	414 286 700 (10 ft)
Hose clamp (1/4" D)	4	408 801 100
Fuel line (1/4" D)	1	414 834 000 (25 ft roll)
Tee (1/4 × 1/4 × 1/4)	3	414 155 300
Spring clamp (for fuel line)	@	414 554 800
Shutoff valve	1	414 539 000
Lube tank (1 to 1-1/2 gallon)	1	N.A.
Roll pin (1/4" dia. × 1-1/2")	4	N.A.
Locking tie	@	414 115 200 (package of 25)

If slide lubrication is not allowed, install a larger diameter idler wheel. This reduces the load on the slider shoes.



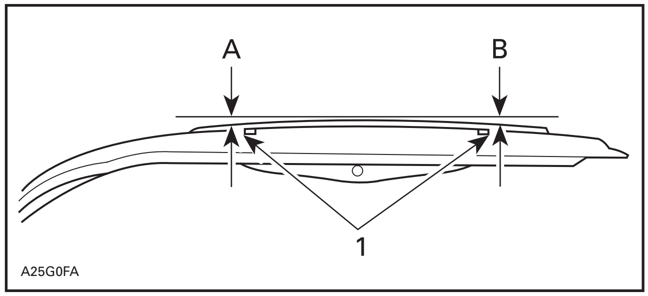
NOTE: Before installing a lubrication system check with your sanctioning body or race organization. In some cases, use of this system and/or certain lubricants is not allowed.

Also, a used or seasoned set of slider shoes will be faster than a brand new pair. The high spots and areas between the idler wheels will be worn down. If brand new sliders must be raced with stock wheels, remove about 1/8 inch of material from the bottom of the slider shoes.

SKIS AND RUNNERS

The skis on your Ski-Doo are not flat on their bottoms, they are slightly convex. This is done to improve stability at high speed on straightaways.

The plastic ski on the MX Zx and MX Z incorporates more of its use (rocker effect). This plastic ski will work very well on snowy surfaces as it increases flotation and reduces drag. For oval and Ice Lemans, the new profile is superior to the steel ski.



1. The above illustration is an example of what is called rocker
A. 2 mm (3/32 in)
B. 2 mm (3/32 in)

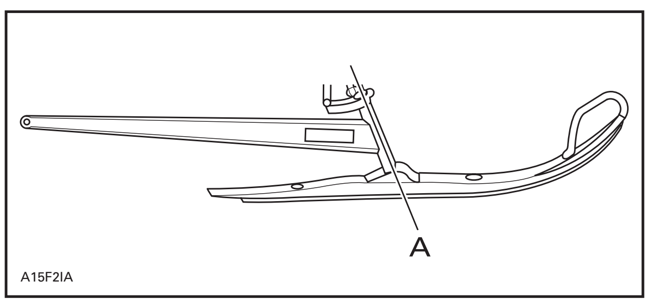
Check your skis from time to time to confirm the 2 mm (3/32 in) (measured at the ski runner studs) bow. If the skis have flattened, use a hydraulic press as necessary to restore the original shape. This is most important for oval racers.

Plastic skis or liners are good for a 2 MPH increase in speed in most snow conditions, more in sticky snow conditions.

Carbide inserted ski runners are necessary for all forms of racing except drag racing and radar runs. The type of racing you are involved in and the condition of the track will determine what style of carbide and how much carbide you will be using.

For the ice race track, special flat-backed race runners with 60° carbide inserts are a must. The flat back of the runner helps to keep the runner from being rolled over by cornering forces. The best racing runners are heat-treated to prevent them from bending under high side loads.

When installing carbide inserts, start with 100 mm (4 in) of carbide in front of a line projected from the center line of the ski leg and 125 mm (5 in) behind the line. Always keep the amount of carbide behind the line longer than in front.



A. 122 mm (5 in) *98 mm (4 in)*
147 mm (6 in) *171 mm (7 in)*

Once you have determined how much carbide you will be using, make up at least one more set. Sharp carbides dig! They must be sharp enough that when you drag your thumb nail over them, they will scrape off some of the nail. To keep your carbide runners is this condition, you must sharpen them every 5 or 6 laps. This is why you should have an extra set ready to go on in a hurry.

The condition of the skis and runners, as well as their alignment, has an effect on top speed. The ski toe-out must be correct; any irregularities in the skis should be removed, and bent or badly worn runners must be replaced.

Ski runners used for cross-country racing must be selected for the type of conditions you will be running in. When exposed earth or plowed roads are to be encountered in an event, full length carbide runners should be used. The concern here is to make the runner and the ski last through the event. These runners are usually set up with 245 mm (10 in) of 60° carbide in the center of the bar with the front and rear portions of the bar filled in with 120° carbide inserts.

When the event is held on a lake or surface conditions consist only of snow and ice, a flat-backer runner with 150 to 200 mm (6 to 10 in) of carbide will do the job. Remember, the more carbide you install, the more positively the front end steers, but more steering effort is also required. Cross-country events run for many hours not just a few minutes like an oval event. Match your carbide to the strength and endurance of your arms.

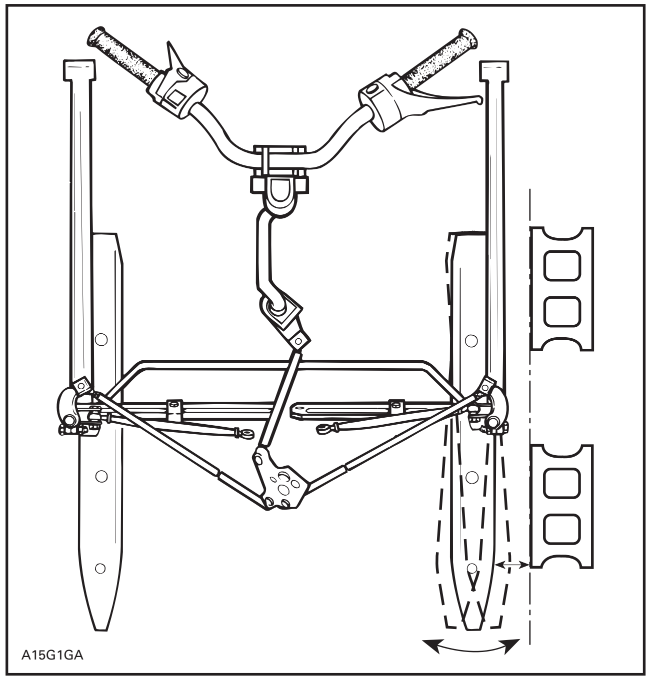
A cross-country carbide does not need to be razor sharp. In fact, testing should be done with a slightly dulled edge, that way your set-up will be right for the majority of the race. If you test with sharp carbides, your chassis set-up will be off when the runners lose their edge after 5-10 miles.

CAUTION: The amount of carbide allowed on each runner may be limited by your race association. Check your rule book.

BUMP STEER

Bump steer refers to the amount of change in the toe-out of the skis as the suspension moves through its total vertical travel. Block up the machine so that the skis are just off the ground and remove the springs from the shocks. This will allow you to cycle the suspension and measure the bump steer on your vehicle.

You will need a reference point to measure to as you cycle the suspension through its travel. Because you will be lifting the ski and suspension assemblies as you are measuring, you should use a reference point that is not easily bumped out of position. A pair of concrete blocks set on a line about 50 mm (2 inches) away from the edge of the ski and parallel to the ski works nicely.



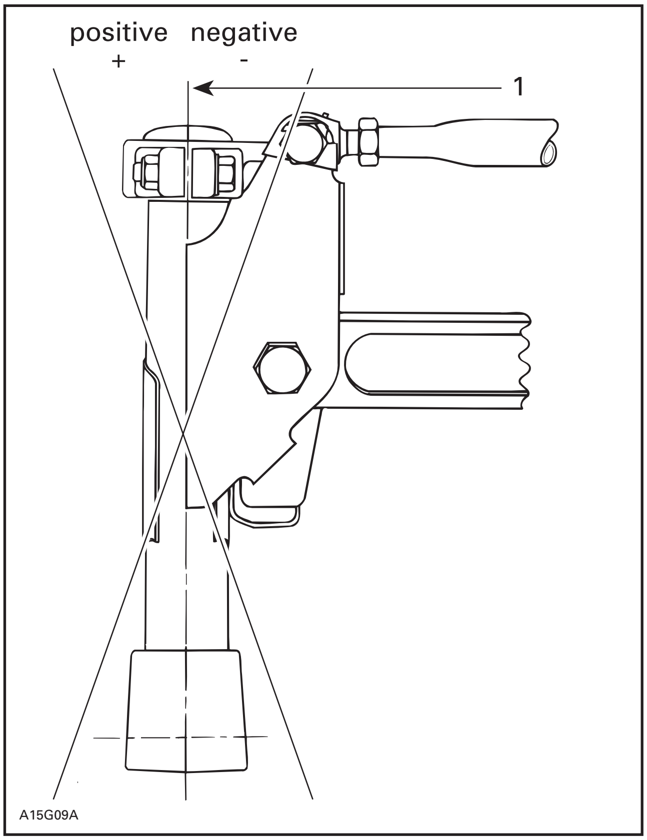
Lift the ski up to its upper travel limit. Using a measuring tape, measure the distances from the front and rear edges of the ski to the concrete block reference. The front and rear measurements must be equal or no more than 1.6 mm (1/16 in) difference if the bump steer adjustment is correct.

SKI LEG CAMBER

The camber angle of the ski legs changes how aggressively the ski runners hook up with the driving surface. Adding negative camber will have the most effect on handling. This is because the weight shift in a turn is always to the outside of the turn and the negative camber of the ski leg causes the wear bar to be presented to the driving surface in a more aggressive position. Positive camber will tuck the wear bar in toward the sled, thereby reducing its traction in a turn.

Camber adjustments do have an effect on the width of the machine. Make certain your camber adjustments do not push you beyond the overall width limit imposed in most forms of racing.

Camber is the tilting of the ski leg from the vertical. To obtain a negative camber angle, the ski leg must be tilted inward so that the ski legs are closer together at the top than at the bottom. Positive camber would tilt the top of the ski leg away from the machine. Camber angle is measured in degrees from the vertical and must be noted as positive or negative.



1. *Ski leg vertical = 0° camber*

Most oval racers set the left ski leg at 0° camber and the right at - 3° to - 5° camber. Trail riders and drag racers should set both ski legs at 0° camber while cross-country and snowcross riders most often set up both ski legs with - 1° to - 3° camber.

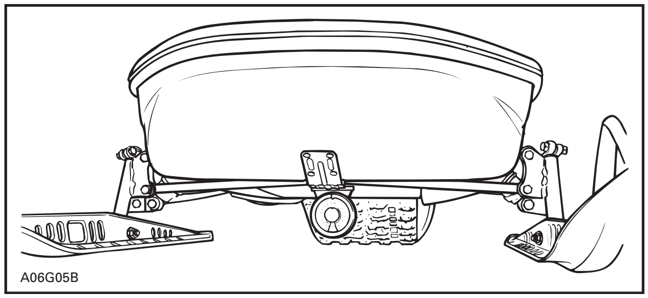
Camber angle is measured using an angle finder available from most tool supply stores.

Adjustment is performed by adjusting the length of the upper control arm.

Procedure

NOTE: Any chassis lowering should be performed before adjusting camber.

– Make sure the vehicle is leveled by placing the angle finder on the main horizontal frame member. Settle the suspension so the vehicle is sitting at the normal ride height.



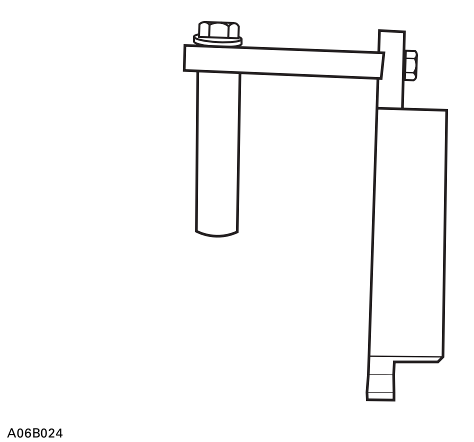
– Remove the black plastic cap from the spindle.
– Insert camber angle tool (P/N 529 021 600) into the spindle.
– Place an angle finder squarely on the camber angle tool.
– Loosen the lock nuts on the upper radius rods.

Unbolt the upper radius rod at the ski leg housing. Turn the radius rod in or out to achieve the desired camber angle.

Camber angle tool
(P/N 529 021 600)

NOTE: Angle finder with a magnetic base must be used.

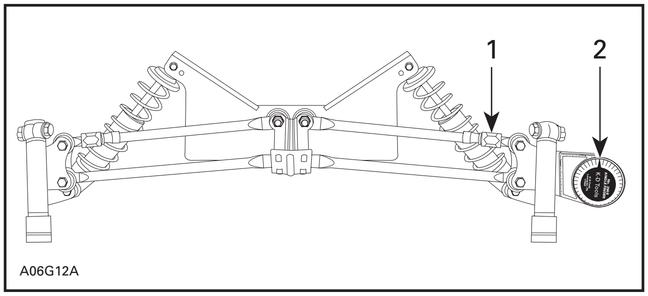
Suggestion: K-D tool no. 2968



APPLICATION

All DSA front suspensions.

CAUTION: The bushing fits into the ski leg housing in only one direction, therefore adjustments must be made in one full revolution increments.



TYPICAL
1. Adjustment
2. Camber reading

– Retorque all nuts and bolts to the proper torque.
– Ski toe-out must be checked after any camber adjustments.

SKI TOE-OUT

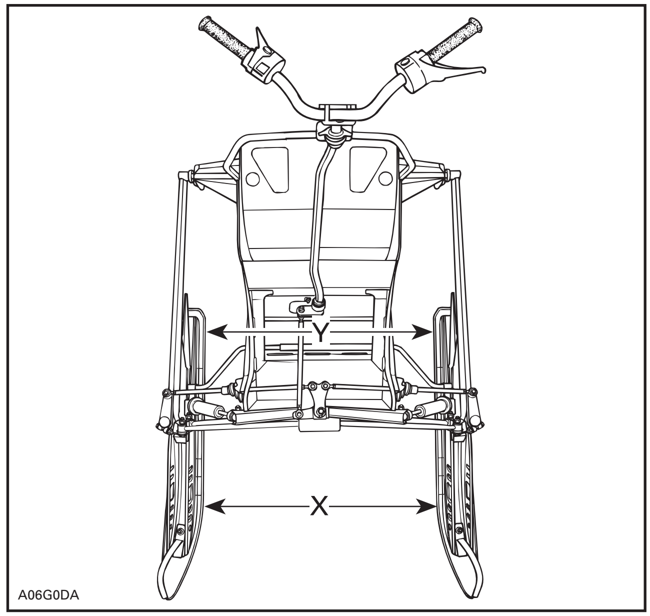
Most oval racers use modified handlebars with loops or angles on the left end. Often a driver prefers a handlebar position that is not horizontal when the skis are in their straight ahead position. This allows a more comfortable driving position when in a corner. Whatever handlebar you prefer should be positioned as you prefer it when going down a straightaway before you begin your toe-out adjustment.

Use a rubber cord stretched between the ski tips to keep constant pressure on the steering system while measuring toe-out. Measure the distance between the inner edges of the skis as far back and as far forward on the skis as possible. Avoid measuring at a point at the top or heel of the ski where the ski is tapered. With aggressive race carbide, the measurements should be taken at the front and back of the runners on the cutting edge for the most precise measurement.

Skis must have a toe-out of 3 to 6 mm (1/8 to 1/4 in) when they are in the straight ahead position.

Adjustment is performed by loosening the lock nuts on the ball joints at the ends of the left and right tie rods. Rotate tie rods as necessary to achieve the proper toe-out and handlebar position. Do not use the short tie rod that runs beneath the engine to adjust ski toe-out.

Never lengthen a tie rod so that the threaded portion of the ball joint extends over 17 mm (11/16 in) beyond the tie rod. To avoid this, distribute the adjustment requirements equally to both left and right tie rods.



X = Y ± 3 mm (1/8 in)

Retorque ball joint lock nuts to 29 N•m (21 lbf•ft) when toe-out is correct.

With the aggressive setup of the front end necessary for competitive oval racing, it is important to keep all the steering system components tight and free of play. Worn ball joints and bushings should be replaced, bolts holding the skis to the ski leg must be tight and wear bars must be straight and bolted securely to the skis. Any play in the steering will result in severe chattering in the corners and darting on the straightaways.

CHASSIS TUNING GUIDELINES

How to Deal with Handling Problems

There is usually never one adjustment that will correct a certain handling quirk. You will usually end up with several changes in setup to achieve the same goal. There are certain basics to keep in mind, however, when you are working with your sled:

– Handling problems encountered when entering a corner are usually corrected by working with front end adjustments.

- Handling problems encountered when exiting a corner are usually corrected by working with rear suspension adjustments.
- Basic handling problems are often traced to improper suspension adjustments.

Guide to Handling Problems

NOTE: PUSHING refers to the front of a vehicle not steering as much as the driver wants. The skis are not grabbing the surface with sufficient force. LOOSE refers to the rear of a vehicle sliding outward in a turn. The track is not grabbing the surface with sufficient force.

NOTE: Center spring/shock refers to the front arm of the rear suspension.

1. Problems encountered when entering a corner.
   a. Front end pushes coming into a corner (steering is not precise).
      - Sharpen carbide runners.
      - Add more carbide.
      - Shorten limiter strap on center arm.
      - Increase negative camber of ski legs.
      - Increase ski spring preload.
      - Decrease center spring preload.

   b. Rear of machine starts to come around or is loose when entering a corner.
      - Lengthen limiter strap on center arm.
      - Decrease ski spring preload.
      - Decrease negative camber of ski legs.
      - Increase center spring preload.
      - Sharpen/add track studs.

   c. Inside ski lifts.
      - Reduce the amount of negative camber on the ski legs.
      - Check for free operation of stabilizer bar.
      - Decrease preload of ski springs.
      - Shorten limiter strap on center arm.
2. Problems encountered while going around or exiting a corner.
   a. Front end pushes coming out of corner (steering is not precise).
      - Shorten limiter strap on center arm.
      - Decrease center spring preload.
      - Check condition of carbides.
      - Add more carbide.
      - Increase negative camber of ski legs.
      - Increase ski spring preload.
      - Increase rear spring preload.
      - Tighten A.C.M.
      - Increase rear to front coupling SC-10 II.

   b. Rear of machine starts to come around or is loose when exiting a corner.
      - Lengthen limiter strap on center arm.
      - Decrease ski spring preload.
      - Increase center spring preload.
      - Decrease negative camber of ski legs.
      - Decrease rear spring preload.
      - Loosen A.C.M.
      - Decrease rear to front coupling.

   c. Left ski lifts.
      - Shorten limiter strap on center arm.
      - Decrease center spring preload.
      - Check for free operation of stabilizer bar.
      - Increase stabilizer bar diameter or shorten end levers.
3. General handling problems.
   a. Machine darts from side to side on straightaway.
      - Check ski toe-out.
      - Check for loose ball joints in steering.
      - Too much negative ski leg camber.

   b. Excess effort required to turn handle bars.
      - Check steering linkages for binding and/or corrosion.
      - Rubber blocks between skis and ski legs have too much preload at the rear (causing rear of skis to be pushed down too much).
      - Lengthen limiter strap on center arm.
      - Increase center spring preload.
      - Decrease ski spring preload.
      - Too much carbide on ski runners.

4. Adjusting the suspension for ride and comfort.
   a. The rear springs of the rear suspension should be adjusted as follows:
      – Fully extend the rear suspension.
      – Measure from the floor to the bottom of the rear grab handle (remember this dimension).
      – Load the vehicle as it will be used (1 or 2 people, saddlebags full of equipment, etc.).
      – Again, measure from the floor to the bottom of the rear grab handle. This dimension should be 25 mm to 50 mm (1 in to 2 in) less than the fully extended dimension.
      – If the vehicle settles more than 50 mm (2 in), increase the rear spring preload.
      – If the vehicle settles less than 25 mm (1 in), decrease the rear spring preload.
      – This is a preliminary setting only! Increase and decrease the preload adjustments to fine tune for your preference.
      – The center spring and ski springs will have the most affect on handling, but if the preload is too stiff, it will produce a harsh ride.

General Tips

If the spring and preload combination you are using exerts the right amount of pressure at full compression but has too much force at initial compression, try a shorter, stiffer spring. The shorter spring will not be preloaded as much and will “act” softer during initial compression, but will get stiffer as the suspension compresses. Conversely, if a setup is good at initial compression but too stiff at full compression, then a softer spring would be used. The following chart can be used to determine how much force a spring and preload combination will exert during compression.

TABLE OF CONTENTS

EQUIVALENT WEIGHTS AND MEASURES CHART

LINEAR MEASURE	
1 inch = 25.4 millimeters (mm)	1 millimeter = .03937 inch
1 inch = 2.54 centimeters (cm)	1 centimeter = .3937 inch
1 foot = .3048 meter (m)	1 meter = 3.2808 feet
1 yard = .914 meter (m)	1 meter = 1.093 yards
1 statute mile = 1.609 kilometers (km)	1 kilometer = .6214 statute mile

WEIGHT	
1 Ounce = 28.35 Grams (g)	1 Gram = .03527 Ounce
1 Pound = .4536 Kilogram (kg)	1 Kilogram = 2.2046 Pounds
1 Ton = .907 Metric Ton (t)	1 Metric Ton = 1.102 Tons

VOLUME
1 Fl. U.S. Ounce = 29.574 Milliliters = .2957 Deciliter= .0296 Liter
1 Fl. U.S. Pint = 473.18 Milliliters = 4.7316 Deciliters = .4732 Liter
1 Fl.U.S. Quart = 946.35 Milliliters = 9.4633 Deciliters = .9463 Liter
1 U.S. Gallon = 3.785 Liters
1 Cu. Inch = 16.387 Cu. cm
1 Cu. Centimeter = .061 Cu. Inch
1 Cu. Foot = 2.831.16 Cu. Cm.
1 Cu. Decimeter = .0353 Cu. Foot
1 Cu. Yard = .7646 Cu. Meter
1 Dry Quart = 1.101 Liters

TEMPERATURE	
32° Fahrenheit = 0° Celsius	°F = 9/5°C + 32
0° Fahrenheit = -17.8° Celsius	°C = (°F – 32) = 5/9

SPEED
1 MPH = 1.61 km/h

ENGINE TUNING CAUTIONS

Here are a few items to keep in mind when working with your engine.

If you are in stock classes, know what adjustments are legal.

Modifications to the power curve of an engine will require recalibration of the transmission.

The lower the RPM at which you can generate the torque you need, the higher the percentage of that power that will reach the track.

Sloppy engine modification usually results in less power than you had stock.

Use the proper octane gasoline for your engine (Modification may require higher octane.).

Correct your carburetor jetting for the atmospheric conditions which exist at the time as close as possible to the time you will be competing.

Follow the assembly and disassembly procedures outlined in the appropriate *Shop Manual.*

BASIC ENGINE THEORY

Terminology

CYCLE	In a combustion engine, a cycle is accomplished when the four (4) phases; intake, compression, ignition and exhaust are complete.
TDC	**Top Dead Center:** The position of the piston when it reaches the upper limit of its travel inside the cylinder. BTDC: Before Top Dead Center ATDC: After Top Dead Center
BDC	**Bottom Dead Center:** The position of the piston when it reaches the lower limit of its travel inside the cylinder. BBDC: Before Bottom Dead Center ABDC: After Bottom Dead Center
BORE	Diameter of the cylinder.
STROKE	The maximum movement of the piston from BDC to TDC. It is characterized by 180° of crankshaft rotation.
COMBUSTION CHAMBER	Space between cylinder head and piston dome at TDC.
DISPLACEMENT	The volume of the cylinder displaced by the piston as it travels from TDC to BDC. The formula is: $\frac{Bore^2 \times Stroke \times \pi}{4}$ 20 = (π = 3.1416) Expressed in cc (cubic centimeters)
NOTE: To transfer cc to cubic inches, divide cc by 16.387.	
COMPRESSION	Reduction in volume or squeezing of a gas.

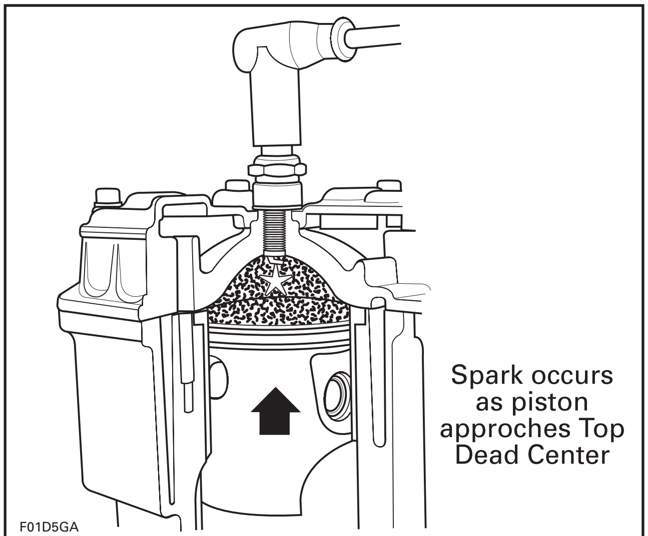
Combustion Process

NORMAL COMBUSTION

Since the beginning of this study we have spoken of air/fuel mixture combustion rather than explosion. This combustion is a slow then accelerated burning of the mixture within the combustion chamber. Ignition occurs with the firing of the spark plug.

This initial process generates heat and pressure which in turn, is transmitted by conduction to the contiguous portion of the unburned mixture. When this portion has reached the point of self-ignition it starts to burn releasing more pressure and heat.

This burning action, called a flame front, travels at a speed of approximately 30.3 m (100 feet) per second until all mixture is burned, thus providing maximum piston thrust.



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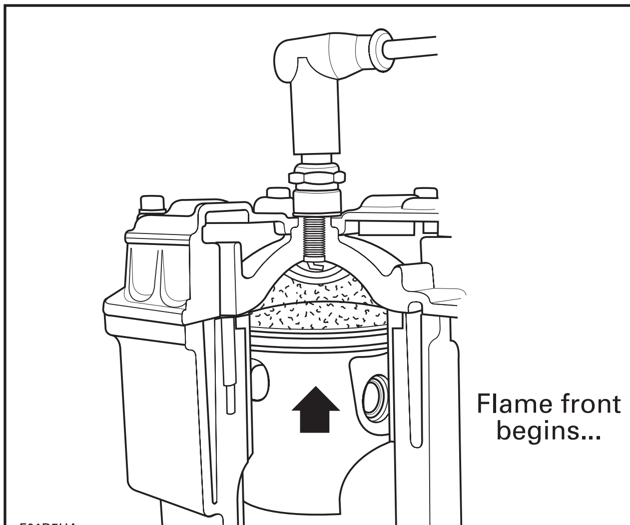

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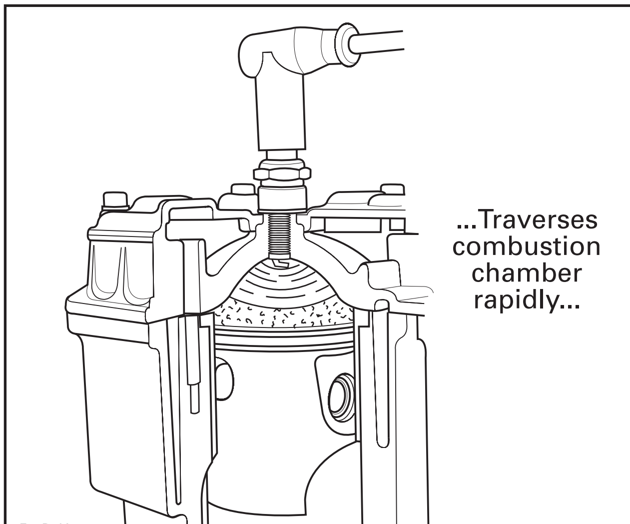

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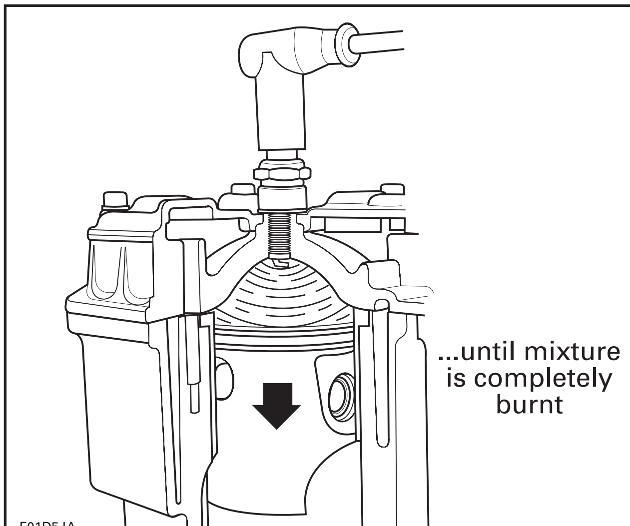

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With all operating parameters correct, normal combustion will take place. However, if for some reason the temperature inside the cylinder is increased during combustion, abnormal combustion will occur and lead to serious engine damage.

DETONATION

In detonation, the spark plug initiates burning and the air/fuel mixture starts to burn in the usual manner but as combustion continues, the heat generated affects the large portion of the yet unburned air/fuel mixture.

This unburned mixture temperature becomes so high that it burns spontaneously creating high-velocity pressure waves within the combustion chamber.

These shock waves can sometimes be heard as pinging. While these shock waves can be detrimental to the mechanical integrity of the engine, it is the excessive heat that causes most problems in 2-strokes. The piston may expand excessively causing a seizure or the piston may melt. The melting will occur at the hottest points, which will be right below the spark plug and around the edge of the piston — often at a ring locating pin. If allowed to continue, a hole may melt completely through the top of the piston.

PRE-IGNITION

Pre-ignition is the ignition of the mixture inside the combustion chamber before the timed spark. Pre-ignition sources are generally an overheated spark plug tip or a glowing carbon deposit on the piston head. Since ignition occurs earlier than the timed spark, the hot gases stay longer in the combustion chamber, thus increasing cylinder head and piston temperatures to a dangerous level.

Usually the piston is subject to damage. It may seize or the aluminum on the exhaust side of the piston dome may melt. Pre-ignition is always preceded by detonation.

CAUSES OF DETONATION:

Octane of the fuel is too low.

Air/fuel mixture is too lean.

a. Incorrect jetting.
b. Air leaks.
c. Varnish deposits in carburetor.
d. Malfunction anywhere in fuel system.

Spark plug heat range too high.

Ignition timing too far advanced.

a. Initial timing incorrect.
b. Ignition component failure.

Compression ratio too high.

a. Improperly modified engine.
b. Deposit accumulation on piston dome or head.

Exhaust system restrictions.

a. Muffler plugged/restricted.
b. Tail pipe diameter too small.
c. Incorrect design of expansion chamber.

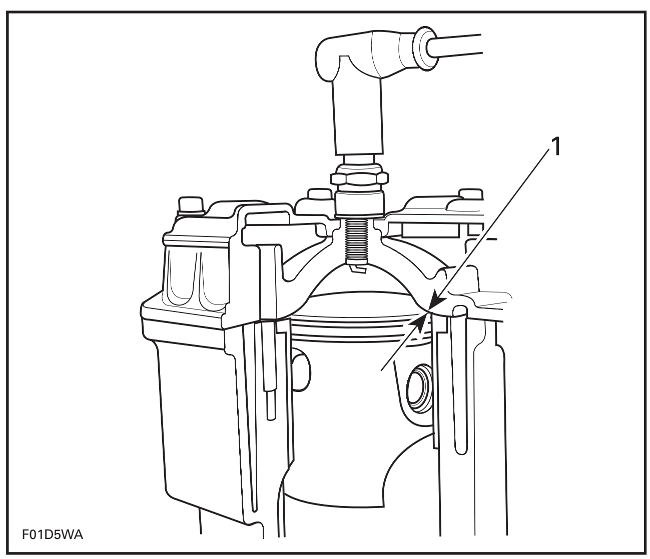
General overheating.

a. Broken fan belt.
b. Loss of coolant.
c. Lack of snow on heat exchangers.

Coolant or water entering combustion chamber.

SQUISH AREA

Rotax cylinder heads incorporate a squish area. This area is basically a **ledge** projecting beyond the combustion chamber area. In operation, as the piston ascends and approaches the ledge, a rapid squeezing action is applied to the air/fuel mixture contained in the area immediately between the piston dome and the ledge. This squashing action forces the entrapped mixture rapidly into the combustion chamber area, creating a greater mixture turbulence. Additionally, the small volume and large surface area of the squish band allow a better cooling of the end gases to help prevent detonation.

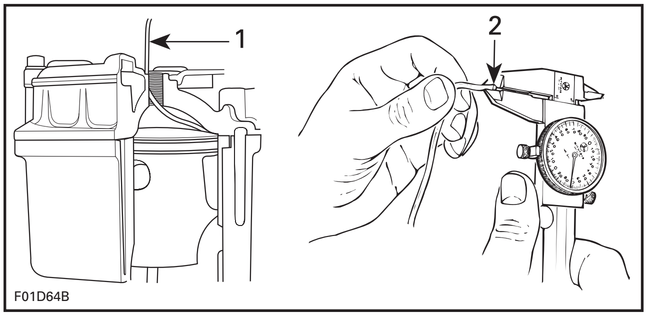


1. *Squish area 1.27 - 1.78 mm (.050 - .070 in)*

If the squish clearance is increased, a loss in power will occur while too small a squish clearance will lead to detonation.

The squish clearance can be measured by inserting a piece of rosin core solder into the combustion chamber, rotating the engine through TDC, removing the solder and measuring the thickness of the compressed solder.

The solder should be inserted above and in line with the wrist pin. Measure the squish on both sides of piston as it may vary from side to side.



1. *Solder*
2. *Flattened area*

CAUTION: Do not use acid core solder; the acid can damage the piston and cylinder.

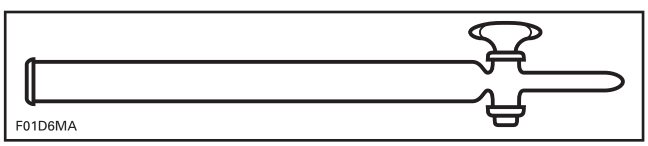
COMPRESSION RATIO

Measuring a Compression Ratio

The minimum combustion chamber volume is the region in the head above the piston at TDC. It is measured with the head installed on the engine.

Remove one spark plug and place piston at TDC.

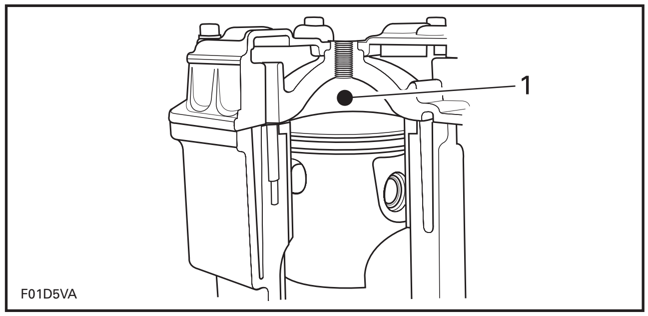
Obtain a CC graduated burette, capacity 0-50 cc and fill with automatic transmission fluid.



Inject the burette content through the spark plug hole until mixture touches the two bottom threads of the spark plug hole.

Read the burette scale and obtain the number of cc injected into cylinder. (example: 21.5 cc).

Record the volume which we will note as V_2.



1. *Combustion chamber (V_2)*

NOTE: When the combustion chamber is filled to top of spark plug hole, subtract 2.25 cc (19 mm reach head; i.e. BR9ES spark plug). Check if fluid level decreases, in that case there is a leak between piston/cylinder. The recorded volume would be false.

Removing the head and measuring the head volume by laying a flat plate across the head will not give an accurate measurement of combustion chamber volume because the dome of the piston protrudes into the head on an assembled engine.

The uncorrected compression ratio of an engine is the volume of the cylinder plus the minimum volume of the combustion chamber divided by the minimum volume of the combustion chamber.

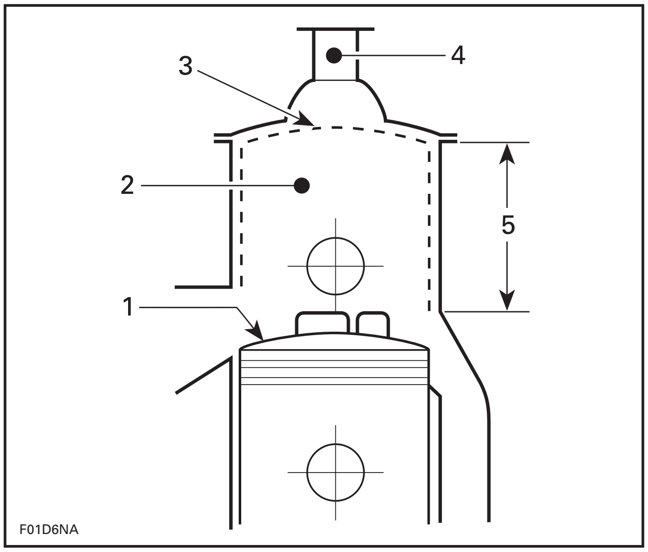
$$C.R. = \frac{V_1 + V_2}{V_2}$$

Where:

C.R. = compression ratio: 1

V_1 = volume of a cylinder = $\frac{B^2 \times S \times \pi}{4}$

V_2 = minimum combustion chamber volume



1. *BDC*
2. *V_1*
3. *TDC*
4. *V_2*
5. *Stroke*

EXAMPLE:

$\pi = 3.14$
B = Bore diameter (cm) = 7.2 (= 72 mm)
S = Stroke (cm) = 6.1 (= 61 mm)
V_2 = 21.5 cc

$$C.R. = \frac{248.4\ cc + 21.5\ cc}{21.5\ cc}$$

C.R. = 12.6:1

In a 2-stroke engine, this is referred to as the uncorrected compression ratio. Because of the exhaust port midway up the cylinder, some designers believe that actual compression does not begin until the piston just closes the exhaust port. This is termed “corrected compression ratio”.

Measuring Corrected Compression Ratio

$$C.C.R. = \frac{V_3 + V_2}{V_2}$$

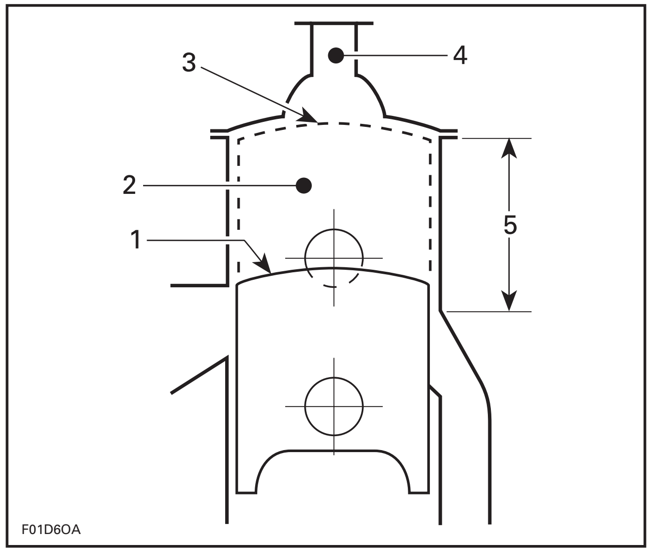
Where:

C.C.R. = corrected compression ratio: 1

V_3 = volume of a cylinder with piston just

closing the exhaust port = $\frac{B^2 \times S_1 \times \pi}{4}$

V_2 = minimum combustion chamber volume



1. *Exhaust port just closed*
2. *V_3*
3. *TDC*
4. *V_2*
5. *Portion of stroke*

EXAMPLE:

$\pi = 3.14$
B = Bore diameter (cm) = 7.2 (= 72 mm)
S_1 = Portion of stroke (cm) = 3.1 (= 31 mm)
V_2 = 21.5 cc

$$C.C.R. = \frac{126.2 + 21.5}{21.5}$$

C.C.R. = 6.9: 1

How to Calculate Machining Cylinder Head Height Versus Combustion Chamber Volume

$$H = \frac{V_M - V_D}{\pi \times \left(\frac{B}{2}\right)^2}$$

Where:

H = material to be machined from face of cylinder head (cm)

V_M = measured combustion chamber volume (cc)

V_D = desired combustion chamber volume (cc)

$$= \frac{V_1}{CR_D - 1}$$

V_1 = Volume of cylinder

CR_D = Desired compression ratio

$\pi = 3.1416$

B = bore of cylinder (cm)

EXAMPLE:

Desired compression ratio (CR_D) = 14.0: 1

$$V_D = \frac{V_1}{CR_D - 1} = \frac{248.4\ cc}{14.0 - 1} = 19.1\ cc$$

$$H = \frac{V_M - V_D}{\pi \times \left(\frac{B}{2}\right)^2} = \frac{21.5\ cc - 19.1\ cc}{3.14 \times \left(\frac{7.2}{2}\right)^2}$$

= .059 cm = .59 mm = (.023")

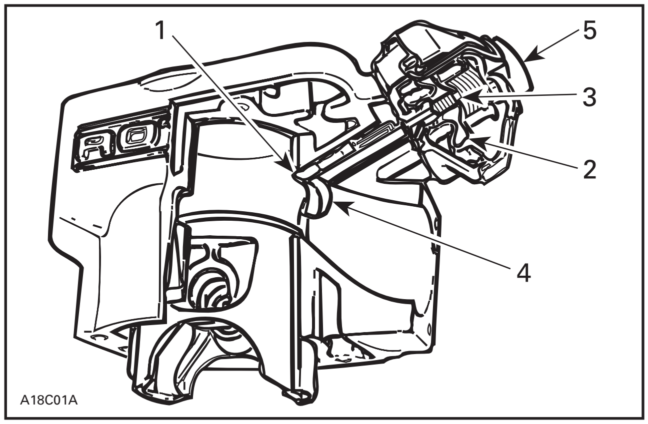
OPERATION OF THE RAVE VALVE
Rave Stands for Rotax Adjustable Variable Exhaust

Theory

For a two-stroke-cycle engine to have high power capacity at high crankshaft speeds, a high volumetric or breathing efficiency is required and the fresh charge losses must be minimized. The result is achieved by opening the exhaust port early (94.5° BBDC) and utilizing the resonant effects of the tuned exhaust system to control fresh charge losses.

When an engine of this design is run at a medium speed, efficiency falls off quickly. The relatively high exhaust port effectively shortens the useful power stroke and because the exhaust system is tuned for maximum power, there is a large increase of fresh charge losses. As a result, the torque decreases along with a dramatic increase of the specific fuel consumption. Higher torque along with lower fuel consumption can be obtained at lower engine speeds if the time the exhaust port is open is shortened.

BOMBARDIER-ROTAX has patented a remarkably simple system to automatically change the exhaust port height based on pressure in the exhaust system.



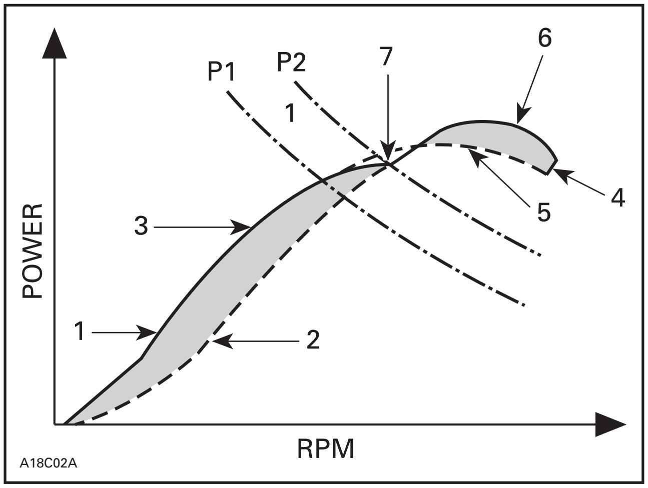
1. Guillotine
2. Diaphragm
3. Return spring
4. Exhaust port
5. Red plastic adjustment knob

Located above the exhaust port is a guillotine-type slide valve (item 1). This rectangular valve is connected by a shaft to a diaphragm (item 2) which is working against the return spring (item 3). Two small passages in the cylinder just outside the exhaust port (item 4) allow exhaust gas pressure to reach the diaphragm. As the throttle is opened and the engine begins producing more power, the pressure against the diaphragm will overcome the pressure of the return spring and the RAVE valve will open.

To the outside of the return spring is a red plastic adjustment knob (item 5). Turning the adjustment in or out changes the preload on the return spring which, in turn, will change the RPM at which the RAVE valve opens and closes. The exhaust port height changes a total of 4 mm to 6 mm (depending on engine type) from the RAVE valve fully closed to fully open.

Operation

The RAVE valve does not allow an engine to make higher peak horsepower than an engine not so equipped, it can make moving the peak higher practical because of its effect on the rest of the power curve. Item 2 in following illustration is the power curve of an engine with the RAVE valve held fully open through its entire RPM range. Item 6 notes the peak power produced. That peak will not change if the exhaust port time of a similar engine without a RAVE valve was the same (with all other features equal).



Item 1 is the power curve of the engine with the RAVE closed through its entire RPM range. The shaded area (item 3) is the improvement in power at lower engine speeds that is gained because of the lower exhaust port. If the port remains at this height, however, the power would peak as noted in item 5. Raising the exhaust port at the proper RPM (item 7) will allow the engines peak power to continue to rise to item 6.

Item P1 in the illustration is the pressure of the return spring against the diaphragm. The exhaust pressure must be high enough to overcome this pressure before the valve begins opening. Item P2 is the pressure required to completely open the RAVE valve. Between P1 and P2, the usable power curve of the engine is moving from power curve 1 to power curve 2. This transition takes place very rapidly at full throttle and from a practical standpoint can be considered to be instantaneous at item 7 which for the type 583 engine is at 6300 - 6400 RPM. Gradual application of the throttle, however, will result in the RAVE valve opening much later, i.e. 7300 - 7500 RPM.

If the RAVE valve opens too late, the engine will bog or hesitate momentarily as the RPM increases. Full peak performance (item 6) is still available. From a functional point of view. it is better to have the valve open a bit early than a bit late. This fact is due to certain dynamic conditions that exist on the snowmobile, i.e., the clutch and torque converter.

Adjustment

The red cap on the RAVE valve cover should be turned all the way in and bottomed in normal use. Backing the red adjuster out will reduce the spring preload and allow the RAVE valve to open at a lower RPM.

At high altitudes, exhaust gas pressures will drop and the spring preload may have to be decreased. It is doubtful that any adjustment will be required up to an altitude of 2400 m (8000 ft). Above that, however, the spring preload can be reduced by turning the red adjustment screw out up to a maximum of four turns.

The only other time adjustment of the spring preload should be considered is if the engine has been modified in any way.

AVAILABLE RAVE SPRINGS

Spring P/N	Wire Dia. mm (in)	Free Length mm (in)	Preload in N (LBF) at Compressed Length of 14 mm (.551 in)
420 239 948	1.0 (.039)	38.0 (1.50)	19.5 (4.37)
420 239 944	0.9 (.035)	48.5 (1.91)	15.9 (3.56)
420 239 942	0.8 (.031)	42.5 (1.67)	7.3 (1.64)
420 239 941	0.8 (.031)	52.5 (2.07)	10.5 (2.36)

Maintenance

There are no wear parts anywhere in the system and there are no adjustments to be periodically checked. The only possible maintenance required would be cleaning of carbon deposits from the guillotine slide. Cleaning intervals would depend upon the user's riding style and the quality of the oil used. Using Ski-Doo oil, we would suggest annual cleaning of the valve. If a customer uses a lower quality, high ash oil, more frequent cleaning may be required.

No special solvents or cleaners are required when cleaning the valve.

Bench Test for Checking RAVE Valve Operation

The operation of the valve can be checked by pressurizing the engine as one would when checking for crankcase leaks.

The engine must be sealed at all exhaust flanges, all carburetor inlets, and at the fuel pump impulse fitting. Depending on the design of your pressure test kit, you may be pressurizing the engine through the crankcase or right at the exhaust flange cover plate. If you are pressurizing through the crankcase, make certain the piston uncovers the exhaust port on the side you are checking.

Install the RAVE valve movement indicator (P/N 861 725 800) in place of the red plastic adjuster on the diaphragm cover so that you can observe the diaphragm movement.

The movement indicator must be turned all the way in to provide maximum spring pre-load. As you begin pressurizing the engine using engine leak tester kit (P/N 861 749 100), you will find the RAVE valve beginning to move at 5 kPa (0.7 PSI or 20 inches of water) and the valve will be fully displaced when you reach 10 kPa (1.4 PSI or 40 inches of water).

NOTE: Due to the low pressure conditions when using the leak tester kit (P/N 861 749 100) to check the RAVE valve operation, install a gauge with a range of 0-200 inches of water (P/N 861 749 100) on leak tester. As reference 6.89 KPa 1 (PSI) = 27.71 inches of water.

Troubleshooting

SYMPTOM	CAUSE	REMEDY
Engine revs 500 to 1000 RPM lower than its maximum operational RPM; Rave valve is not opening.	1. Bent valve rod	Replace
	2. Stuck valve	Clean
	3. Wrong spring tension (too high)	Replace
	4. Clogged passages	Clean
	5. Damaged bellows or clamp(s)	Replace
Engine hesitation in mid RPM range and full peak performance is available only after a while. Rave valve opens too early.	1. Broken or weak spring	Replace
	2. Adjustment screw too far out	Turn until it bottoms
	3. Valve stuck open	Clean

SKI-DOO utilizes cylinder reed induction technology on the new Series 3 twin cylinder engines. This technology is beneficial in three ways.

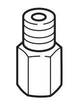
1. It uses less parts, (i.e. shafts, rotary valve discs, etc.). Resulting in a lighten engine package.
2. This technology results in positive control of fuel mixture, while providing a straight pathway to the intake and transfer ports as it is not obstructed by the rotating crankshaft.
3. By locating the carburetors higher on the engine this design allows for lower engine placement in the chassis.

BASE GASKETS		
377	P/N 420 931 781	0.4 mm
443	P/N 420 931 780	0.3 mm
	P/N 420 931 781	0.4 mm
	P/N 420 931 782	0.6 mm
503	P/N 420 831 856	0.3 mm
	P/N 420 831 858	0.4 mm
	P/N 420 831 859	0.6 mm
453	P/N 420 931 580	0.3 mm
	P/N 420 931 581	0.4 mm
	P/N 420 931 583	0.5 mm
	P/N 420 931 582	0.6 mm
	P/N 420 931 584	0.8 mm
493	P/N 420 931 588	0.5 mm
	P/N 420 931 589	0.8 mm
	P/N 420 931 960	0.7 mm
	P/N 420 931 587	0.6 mm
494	P/N 420 931 361	0.4 mm
	P/N 420 931 360	0.3 mm
	P/N 420 931 362	0.6 mm
593	P/N 420 931 582	0.6 mm
	P/N 420 931 962	0.7 mm
	P/N 420 931 583	0.5 mm
	P/N 420 931 584	0.8 mm
693	P/N 420 931 892	0.6 mm
	P/N 420 931 893	0.5 mm
	P/N 420 931 894	0.7 mm
	P/N 420 931 895	0.8 mm
699	P/N 420 931 570	0.3 mm
	P/N 420 931 571	0.4 mm
	P/N 420 931 572	0.6 mm
793	P/N 420 931 838	0.5 mm
	P/N 420 931 837	0.6 mm
	P/N 420 931 964	0.7 mm
	P/N 420 931 839	0.8 mm
809	P/N 420 931 620	0.3 mm
	P/N 420 931 621	0.4 mm
	P/N 420 931 622	0.6 mm

CARBURETION

Carburetor Main Jet Correction Chart

CARBURETOR MAIN JET CORRECTION CHART



FT/METER	°F/°C							
	- 60/ - 50	- 40/ - 40	- 20/ - 30	- 0/ - 20	+ 20/ - 5	+ 40/ - 5	+ 60/ - 15	+ 80/ - 25
0	111.10	107.40	103.70	% 100.00	96.30	92.60	88.90	85.20
2000/ 600	105.77	102.07	98.37	94.67	90.97	87.27	83.57	79.87
4000/ 1200	100.43	96.73	93.03	89.33	85.63	81.93	78.23	74.53
6000/ 1800	95.10	91.40	87.70	84.00	80.30	76.60	72.90	69.20
8000/ 2400	89.7	86.07	82.37	78.67	74.97	71.27	67.57	63.27
1000/ 3000	84.44	80.74	77.04	73.34	69.64	65.94	62.24	58.54

A01C47A

NOTE: When the answer gives an unavailable jet size, select the next highest (richer) jet.

Example:

With a 250 stock main jet, at an altitude of a 600 m (2000 ft) and a temperature of - 5°C (20°F):

$$250 \times \frac{90.97}{100} = 227\text{; use 230 jet.}$$

CAUTION: These values are guidelines only. Specific values/adjustments vary with temperature, altitude and snow conditions. Always observe spark plug condition for proper jetting.

This table is more than adequate for stock engines. Two-stroke engines with high specific outputs that are heavily modified (twin pipes, high compression, large carburetors, etc.) and performing at high RPM are very sensitive to air density changes. The following is a very accurate formula for correcting jetting.

First, a baseline for jetting must be established.

Jetting, horsepower, and B.S.F.C. data can be obtained with dyno testing but also confirmed with field testing. The tried and true method of determining mixture ratio is to inspect the parts of the engine that are directly exposed to the combustion process. The two best indicators are the spark plug and the piston dome. The color and where it is located are the two things to look for. Chocolate brown on the insulator, ground electrode, and piston dome indicate a proper mixture. The ground electrode should show a difference in color just at the radius of the electrode.

The engine must be operated under load for at least one minute to obtain accurate readings.

Establish the C.R.A.D. by using the following formula:

$$\text{C.R.A.D.} = \frac{1737.97 \text{ x C.A.P.}}{460 + T}$$

C.A.P. = Corrected air pressure

C.A.P. = B - E

B = Barometric pressure readings (in – Hg)

$$E = \text{Vapor pressure} = \left(\text{S.P. x } \frac{\text{R.H.}}{100}\right)$$

See saturation pressure (chart 1).

S.P. = Saturation pressure (in – Hg)

R.H. = Relative humidity (%)

Record the C.R.A.D. when correct jetting has been established. This is your base line for future use.

Example: Testing established a 400 main jet at C.R.A.D. of 100%. One week later, the C.R.A.D. at the track is 110%. Use the following formula to establish the new main jet.

$$\text{New main jet} = \frac{\text{New C.R.A.D.} \times \text{Baseline main jet}}{\text{Base line C.R.A.D.}}$$

$$\text{Example: } \frac{110 \times 400}{100}$$

New main jet = 440

Record the C.R.A.D. when correct jetting has been established. This is the baseline for future use. Jetting corrections for a different C.R.A.D. can be obtained with the following ratio:

$$\text{New main jet} = \frac{\text{New C.R.A.D.} \times \text{Base line M.J.}}{\text{Base line C.R.A.D.}}$$

Example: Testing results in a 570 M.J. at a C.R.A.D. of 105.4%. Two weeks later at the race track, the C.R.A.D. is 110.9%.

$$\text{The new M.J.} = \frac{110.9 \times 570}{105.4}$$

New M.J. = 600

Useful Equations

$$\text{C.F.} = \frac{29.92}{B - E} \times \frac{460 + T}{520}$$

C.A.P. = B – E

$$\text{C.R.A.D.} = \frac{1737.97 \times \text{C.A.P.}}{460 + T}$$

Where:

B = barometer reading (in-Hg)

E = vapor pressure (in – Hg) = S.P. × $\frac{\text{R.H.}}{100}$ or use wet bulb/dry bulb temperature and psychrometric chart

T = carb. inlet air temp (°F)

S.P. = saturation pressure (in-Hg)

R.H. = relative humidity (%)

C.A.P. corrected air pressure (in-Hg)

C.HP = Corrected brake horsepower

B.S.F.C. = Brake specific fuel consumption

C.R.A.D. = Corrected relative air density (%)

E.G.T. = Exhaust gas temperature

W.O.T. = Wide open throttle

SATURATION PRESSURE (CHART 1)	
T = TEMP. (°F)	S.P. = SATURATION PRESSURE (in-Hg)
- 40	.004
- 30	.008
- 20	.012
- 10	.020
0	.040
5	.055
10	.070
15	.090
20	.110
25	.140
30	.170
35	.208
40	.247
45	.314
50	.380
55	.450
60	.521
65	.630
70	.739
75	.884
80	1.030
85	1.225
90	1.420
95	1.675
100	1.930

Most racers use an air density gauge. This gauge is fairly inexpensive. It basically establishes C.R.A.D. for you by combining the variables on any given day.

First, establish a base line main jet by testing.

After you have determined the correct main jet, record the jet number and the air density gauge reading.

Example: Base line

Gauge reading 90

Main jet 300

The next day at the track, your air density gauge now reads 105. This means you have gained 15% air density.

New density 105

Base line 90

105 – 90 = 15

Multiply your base line main jet by 115.

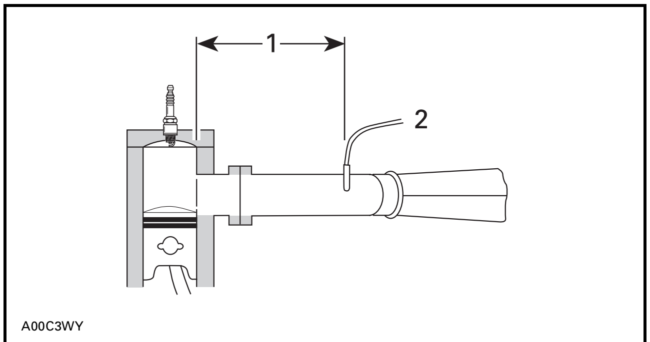
Example: 300 x 115 = 345

Round off to next highest jet size.

New main jet = 350

Air density can change rapidly during the course of the day. Check your gauge frequently. Always use the same gauge for a different gauge may read differently.

Exhaust Gas Temperature Probe Location



Detonation = 720°C (1330°F)

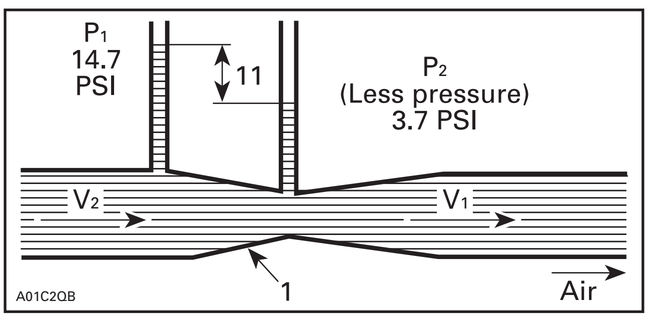
1. 100 mm from piston
2. Probe

NOTE: Temperature at wide open throttle at maximum HP RPM.

Exhaust gas temperatures (E.G.T.'s) can also give an indication of mixture ratio. At wide open throttle (W.O.T.) at maximum HP RPM, a leaner mixture will produce higher E.G.T.'s and a richer mixture will result in lower E.G.T.'s. (E.G.T.'s are not absolute. Engines have seized with E.G.T.'s in the allowable range).

Carburetor Operation

The operation of the carburetor is based on the physical principle that fluids (air is a fluid) under pressure gain speed but lose pressure when passing through a converging pipe (venturi).

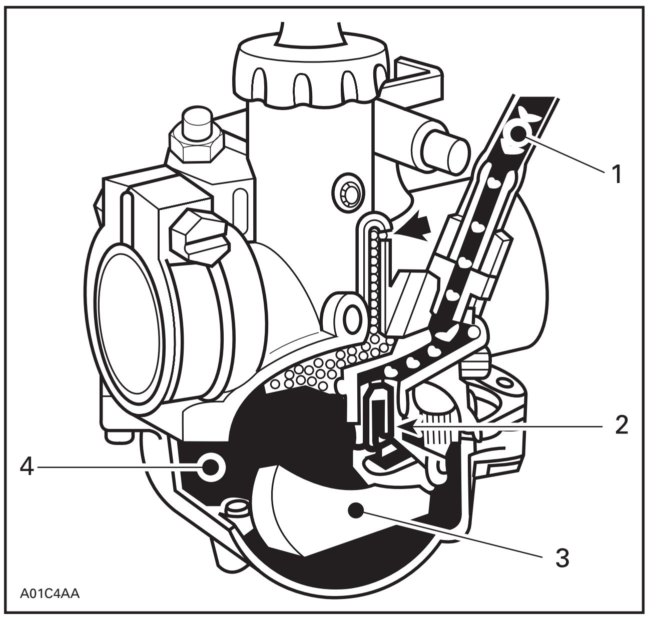


1. Venturi

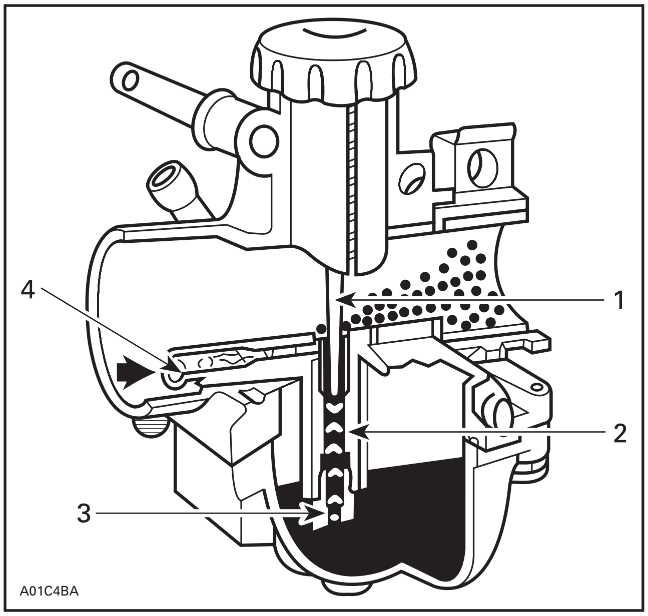
Air entering the bell of the carburetor has a speed of V_1 and pressure of P_1. As the air is forced into the smaller diameter of the venturi, speed increases (V_2) but pressure drops (P_2).

Passages in the carburetor connect the venturi to a reservoir of fuel (float bowl). The float bowl is vented to the atmosphere (P_1). P_1 is greater than P_2 so fuel is pushed from the bowl to the venturi via the jets and passages. Varying the size of jets varies the amount of fuel the engine receives. Engine speed is controlled by varying the amount of air/fuel mixture that the engine receives.

Liquid gasoline does not burn, so for the engine to run efficiently, the fuel must be broken down into small droplets, and mixed with the oxygen molecules in the incoming air. This is referred to as atomization. The shape of the venturi and the shape and location of the jets and fuel delivery passages will determine how well the fuel and air are mixed.



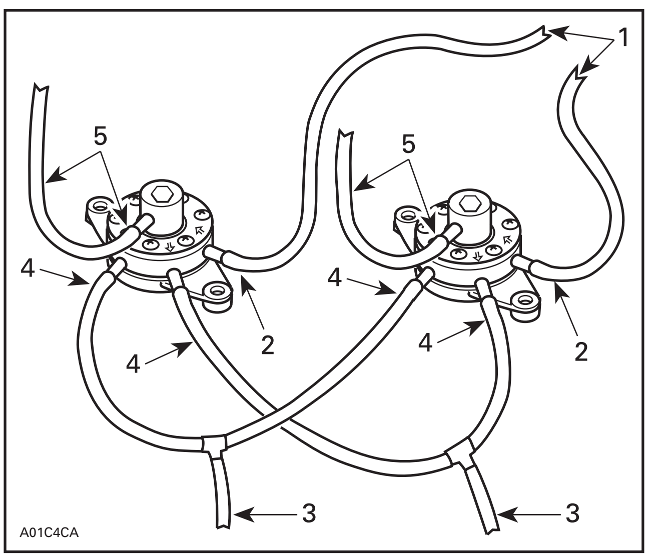
1. Float bowl
2. Needle valve
3. Float
4. Fuel inlet



1. *Jet needle*
2. *Needle jet*
3. *Main jet*
4. *Air jet*

Dual Fuel Pump Installation

With a heavily modified engine, especially when using large bore carburetors, the need for 580 or larger main jets may arise. The capacity of the fuel pump may be exceeded when using these large jets. To eliminate any possibility of starvation, install two fuel pumps as shown below. Be sure to use a separate impulse line to each pump.



1. *From fuel tank*
2. *Fuel inlet line*
3. *To car*
4. *Fuel outlet line*
5. *Impulse line*

Dual outlet, round Mikuni fuel pump equals about 35 liters/hour.

Dual outlet, square Mikuni fuel pump equals about 30 liters/hour.

583 and larger 1995 vehicles use a single large capacity 70 liters/hour fuel pump. The following parts list includes the pieces necessary to install the 70 L/h pump.

LARGE FUEL PUMP PARTS

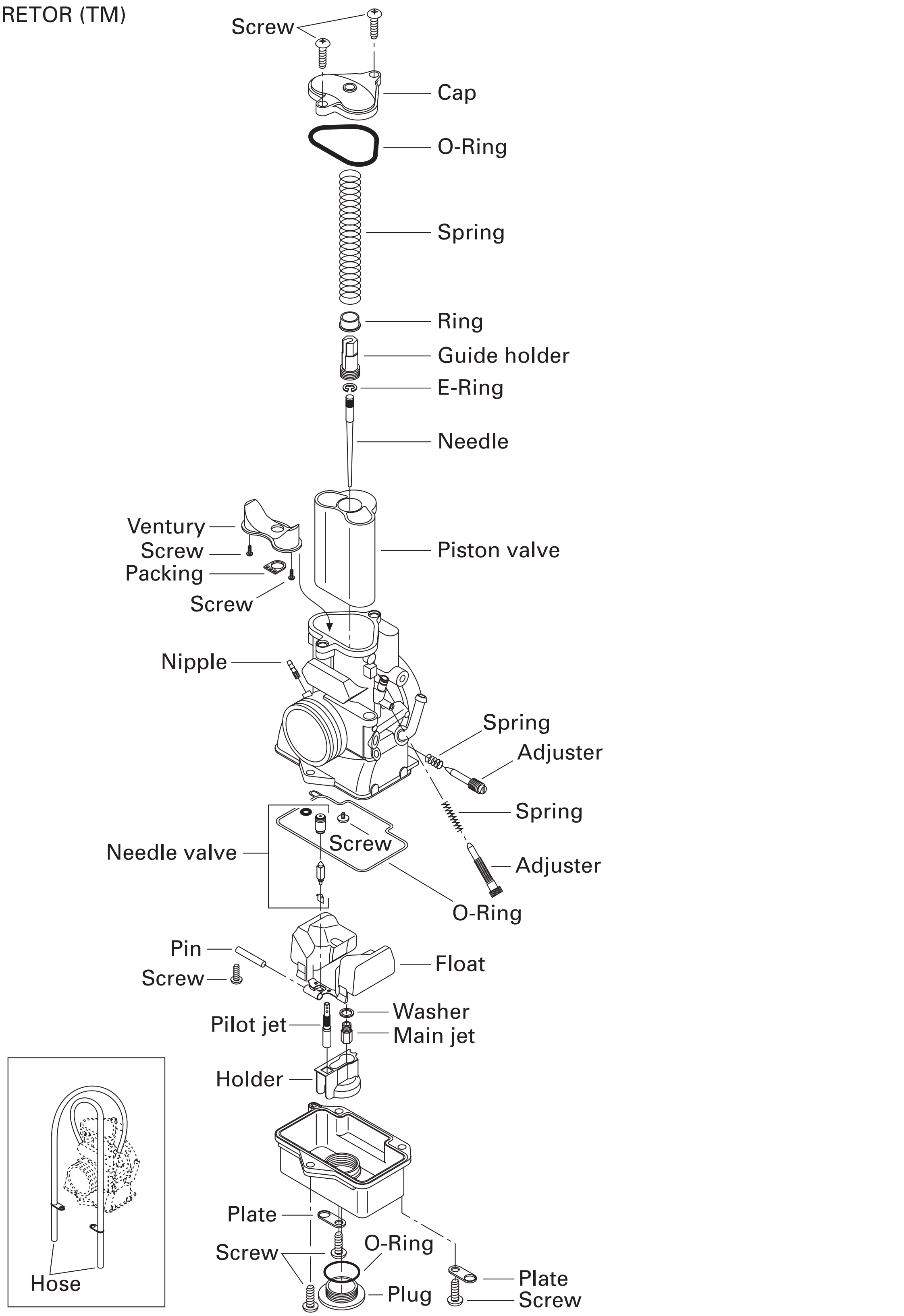
70 Liter/hour fuel pump	P/N 403 901 200
Filter, in-tank	P/N 414 872 100
Fuel line, in-tank	P/N 414 943 700
Grommet, tank	P/N 570 273 900
Connector, tank	P/N 414 872 700
Fuel line, tank to shut off valve	P/N 414 939 900
Shut off valve	P/N 414 872 200
Fuel line, valve to pump	P/N 414 931 400 (roll)
Clamp, fuel line	P/N 414 655 700

MIKUNI VM AND TM TYPE CARBURETORS

Snowmobile engines are operated under a wide range of conditions, from idling with the throttle valve remaining almost closed to the full load (the maximum output) with the throttle valve fully opened. In order to meet the requirements for the proper mixture ratio under these varying conditions, a low-speed fuel system (the pilot system) and a main fuel system (the main system) are provided in Mikuni VM and TM type carburetors.

While this text covers the VM-type carb., the TM flat slide carb. functions the same. The circuits function the same and tuning a TM would be done in the same manner as the VM.

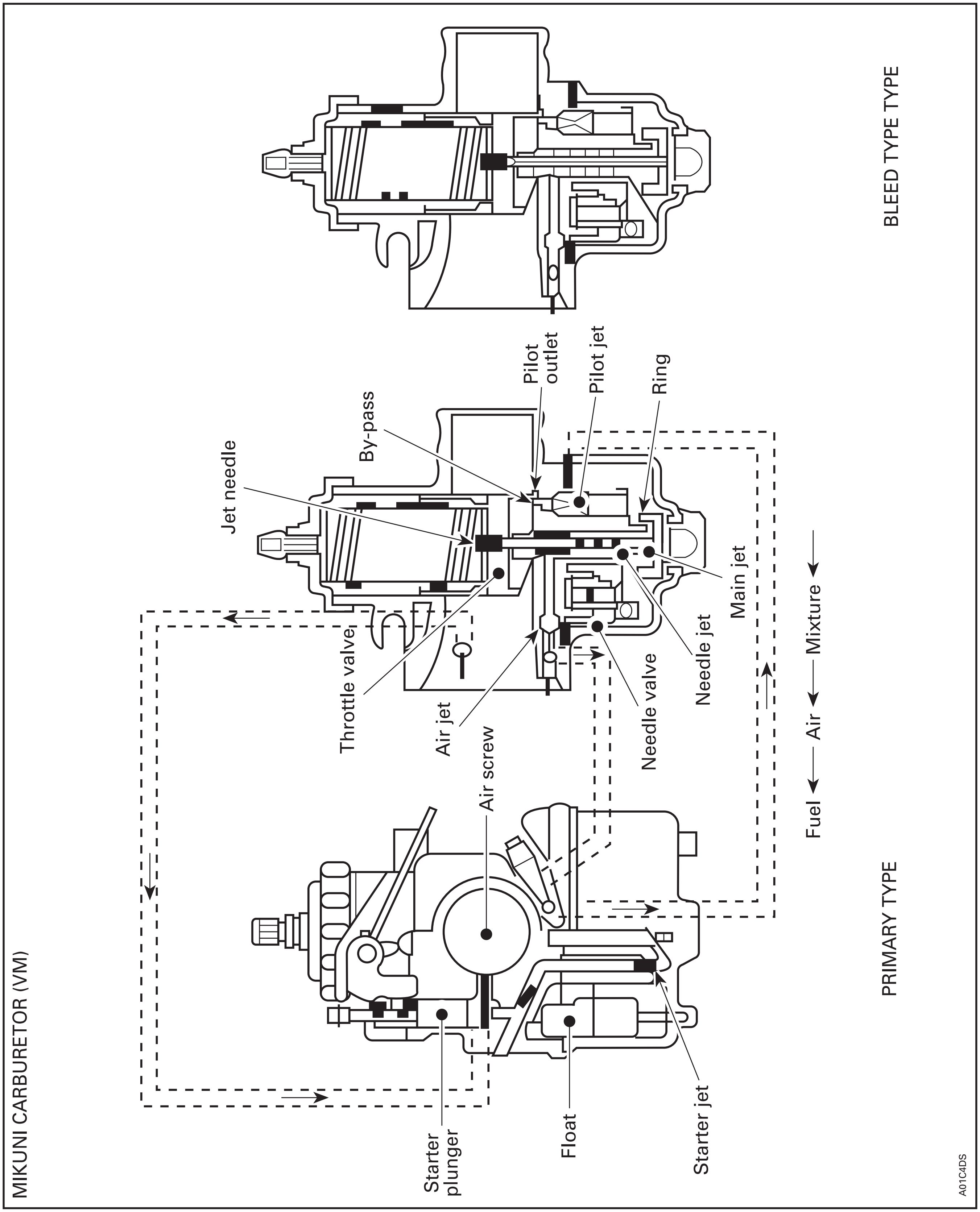
MIKUNI CARBURETOR (TM)



Mikuni TM Carburetor (tuning parts)

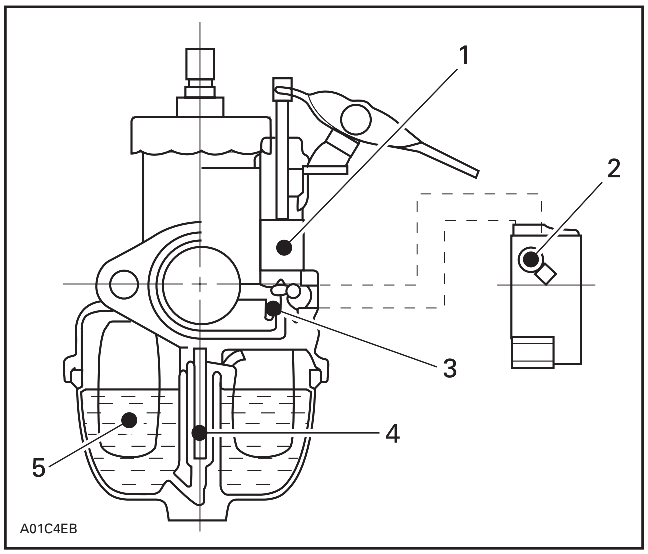
P/N	DESCRIPTION
486 212 400	Pilot Jet, 15
486 212 500	Pilot Jet, 17.5
486 212 600	Pilot Jet, 20
486 212 700	Pilot Jet, 22.5
404 161 870	Pilot Jet, 25
486 212 800	Pilot Jet, 27.5
486 212 900	Pilot Jet, 30
486 213 000	Pilot Jet, 32.5
486 213 100	Pilot Jet, 35
404 144 700	Pilot Jet, 40
486 201 400	Pilot Jet, 45
404 144 800	Pilot Jet, 50
486 201 500	Pilot Jet, 55
404 145 300	Pilot Jet, 60
404 145 400	Pilot Jet, 65
486 213 200	Piston Valve, 3.0
486 213 300	Piston Valve, 3.5
404 161 867	Piston Valve, 4.0
486 213 400	Piston Valve, 4.5
486 213 500	Piston Valve, 5.0
404 161 868	Inlet Needle & Seat 1.5
404 161 871	Needle, J8-6FIY05-58
404 161 872	Needle, J8-6FIY04-59
404 161 873	Needle, J8-6FIY06-57

Part numbers with a 486 prefix must be ordered from Valcourt Race Dept. All others must be ordered from your local Ski-Doo dealer.


MIKUNI CARBURETOR (VM)
Starter plunger
Float
Starter jet
Air screw
Throttle valve
Air jet
Needle valve
Needle jet
Main jet
Jet needle
By-pass
Pilot outlet
Pilot jet
Ring
Fuel
Air
Mixture
PRIMARY TYPE
BLEED TYPE TYPE
A01C4DS

Starting Device (enrichner)

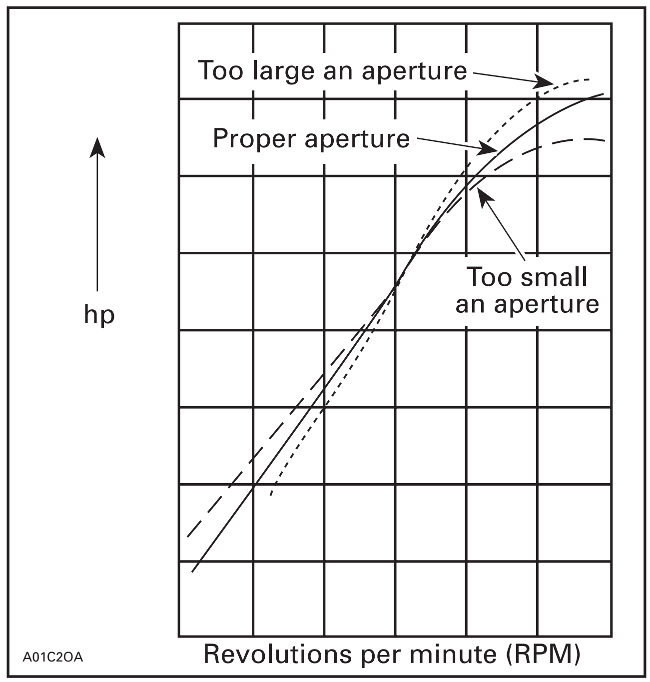
Instead of a choke, the enrichner system is used on some Mikuni carburetors. In the starter type, fuel and air for starting the engine are metered with entirely independent jets. The fuel metered in the starter jet is mixed with air and is broken into tiny particles inside the emulsion tube. The mixture then flows into the plunger area, mixes again with air coming from the air intake port for starting and is delivered to the engine in the optimum air/fuel ratio through the fuel discharge nozzle. The starter is opened and closed by means of the starter plunger. Since the starter type is constructed so as to utilize the negative pressure of the inlet pipe, it is important that the throttle valve be closed when starting the engine.



1. *Plunger area*
2. *Emulsion tube*
3. *Inlet pipe*
4. *Needle jet*
5. *Float*

Selection of the Aperture of Carburetor

One of the prerequisites for improving the output is to use a carburetor with as large an aperture as possible. However, a large aperture alone does not necessarily improve the output. As shown in the following illustration, it is true that a large aperture improves the power output in the high speed range. In the slow speed range, on the other hand, the output drops. The aperture of a carburetor is determined by various factors. These factors include (1) whether the vehicle is intended for racing, (2) the design of the engine, (3) driving technique of the driver, (4) the driver's preference, etc. In addition, the maximum output, the maximum torque and the minimum number of revolutions for stable engine operation must also be taken into account.



Size of Mikuni Carburetors

Mikuni VM-type carburetors come in various sizes, with the main bore ranging from 10 mm (.39 in) to 44 mm (1.73 in) (in even numbers for the most part.) The carburetor body is made of aluminum or zinc.

Carburetor Test

Once the aperture of the carburetor is determined, a test to select the proper jet should be made. The size of the jet is determined by measuring the output in a bench or in a chassis dynamo test. For racing, it is best to determine the proper size of the jet on the racing track, because the following points must be taken into account:

a. The altitude (atmospheric pressure), temperature and humidity of the race track.

b. The operation of the engine based on the topography of the race track.

Checking and Adjusting Float System

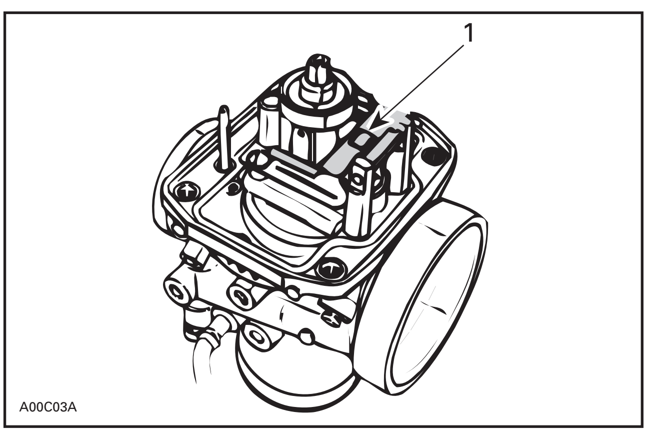
1. Invert the carburetor and check the alignment between the float arm and the base of the carburetor. The float arm should be parallel to the base.
2. Bend the actuating tab as required to make the float arm parallel to the base. Be careful not to bend the float arm.

NOTE: Incorrect float adjustment can prevent proper tuning of a carburetor. Always make sure the float is properly adjusted before attempting adjustment of the other fuel metering system.

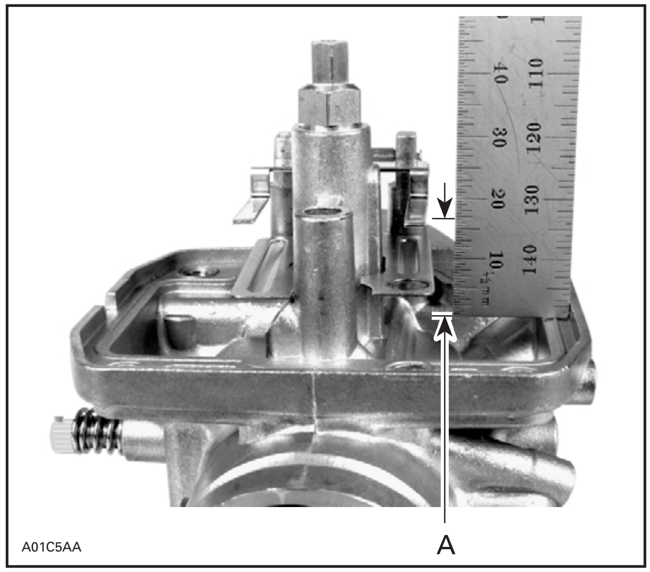
NOTE: Mikuni carburetors used on snowmobiles with fuel pumps require a smaller inlet needle valve (usually 1.5 or 2.0) than carburetors used in gravity feed applications (3.0).

To Adjust Height

– Bend the contact tab of float arm until the specified height is reached.



1. *Contact tab*



TYPICAL
A. Height (refer to table below)

On TM 38, do not turn carburetor up side down. Measure float arm height when it just touches needle valve without moving it.

Float arm height dimensions:

CARBURETOR MODEL	FLOAT HEIGHT ± 1 mm	(± 0.40 in)
VM 30 VM 34	23.9	(.941)
VM 36 VM 38 VM 40	18.1	(.713)
VM 40 MX Z and Summit	22.9	(.901)
VM 44 DPM	22.9	(.901)
TM 38	21.0	(.826)

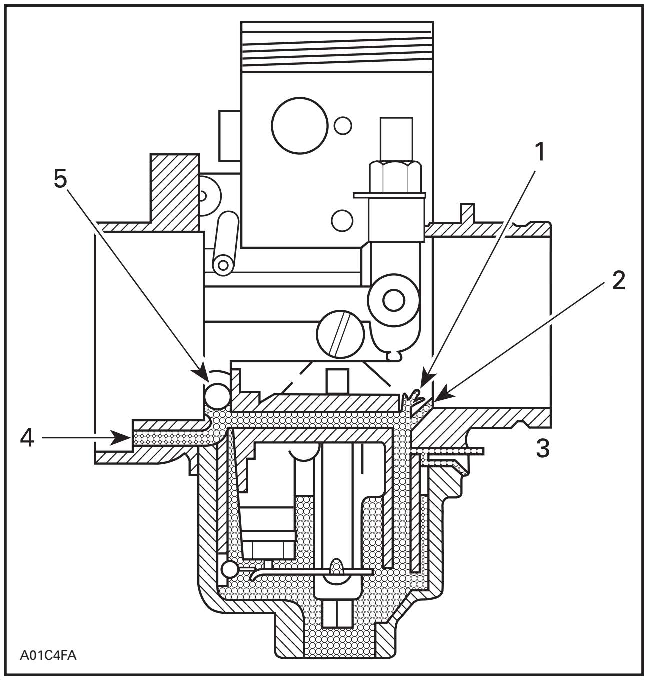
NOTE: To adjust height — bend the contact tab of float arm until the specified height is reached.

Pilot/Air System

PRINCIPLES OF OPERATION

The pilot/air system controls the fuel mixture between idle and approximately the 1/4 throttle position. As the throttle is opened wider for low speed operation, the pilot outlet cannot supply adequate fuel, and fuel then enters the carburetor bore from the bypass as well as the pilot outlet. The pilot/air system is tuned by first adjusting the air screw; then, if necessary, by replacing the pilot jet.

Adjusting Air Screw

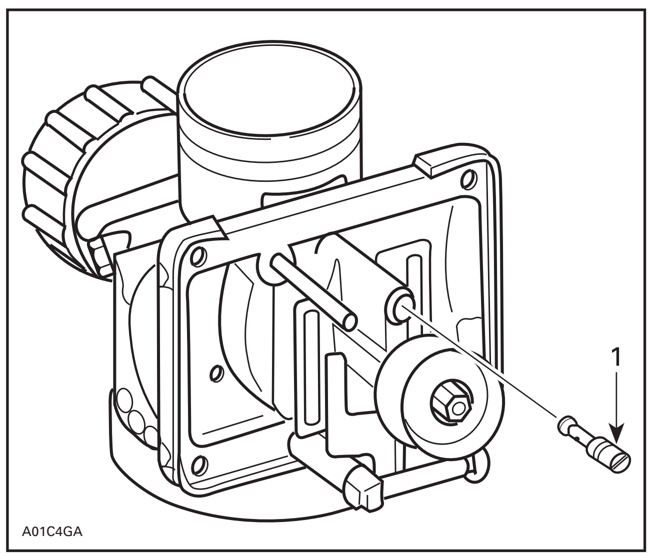


1. *Pilot bypass*
2. *Pilot outlet*
3. *Pilot jet*
4. *Air intake*
5. *Air screw*

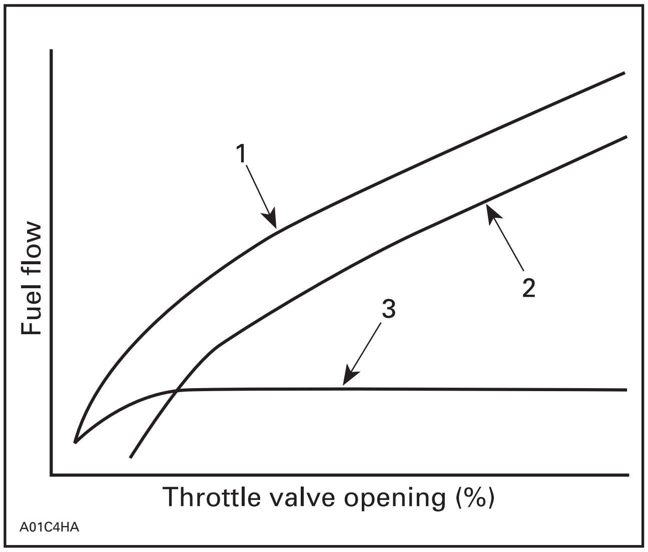
NOTE: This procedure may be performed for single and dual carburetors. Never adjust screws more than 1/4 turn at a time.

1. Turn idle stop screw in until screw contacts throttle valve. Then turn idle stop screw in 2 additional turns.
2. Start and warm up engine. Adjust idle stop screw to 500 RPM above normal idle speed. See **Low-Speed Fuel System**.
3. Turn air screw in or out using 1/4-turn increments until engine RPM peaks or reaches its maximum RPM.
4. Readjust idle stop screw to return engine to normal idle speed. See pages **Low-Speed Fuel System**.
5. Repeat Steps 3 and 4 until engine operates at normal idle speed and air screw is peaked.
6. When air screw is adjusted stop engine. Note the setting of air screw and turn it all the way in. If it takes less than 1 turn, the pilot jet is too small and a larger one must be installed. If it takes more than 2-1/2 turns to set air screw, the pilot jet is too large and must be replaced by a smaller one.
7. Turn the air screw left and right (between 1/4 and 1/2 turn) and select the position where the engine revolution reaches the maximum. Adjust the throttle stop screw to bring down the engine revolution to your target speed for idling. After this adjustment of the throttle stop screw is made, select once more the position where the engine revolution reaches the maximum, by turning the air screw left and right (between 1/4 and 1/2 alternately). At this point, attention should be paid to the following points.
   a. If there is a certain range in the opening of the air screw where the fast engine revolution can be obtained (for instance, the number of revolutions does not change in the range of 1-1/2 to 2.0 turns), it would be better for acceleration to 1-1/2 turns.
   b. To determinate the **fully closed** position of the air screw, turn the air screw slightly. Excessive tightening of the air screw would damage the seat. The position where the air screw comes to a stop should be considered the **fully closed** position. The maximum number of turns in the opening of the air screw must be limited to 3.0. If the air screw is opened over 3.0 turns, the spring will not work and the air screw can come off during operation of the vehicle.

Replacing Pilot Jet



1. *Pilot jet*



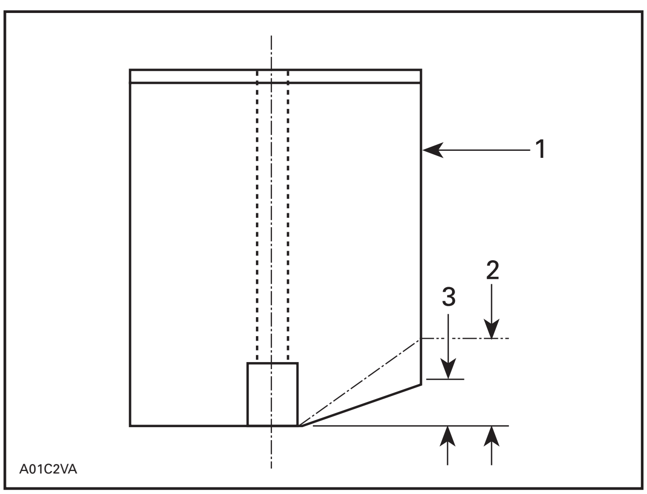
1. *Total amount of fuel flow*
2. *Main fuel system*
3. *Pilot fuel system*

Pilot jets are numbered from no. 15 (the smallest) to no. 80 (the largest). The number corresponds to fuel flow and not necessarily to drill size or through-hole diameter. After changing the pilot jet, check and adjust air screw as described above.

NOTE: Since the pilot/air system provides some fuel up to wide open throttle, changes in this system will affect the throttle valve, jet needle/needle jet, and main jet metering systems.

Throttle Valve

PRINCIPLES OF OPERATION



1. *Throttle Valve*
2. *3.0*
3. *2.0*

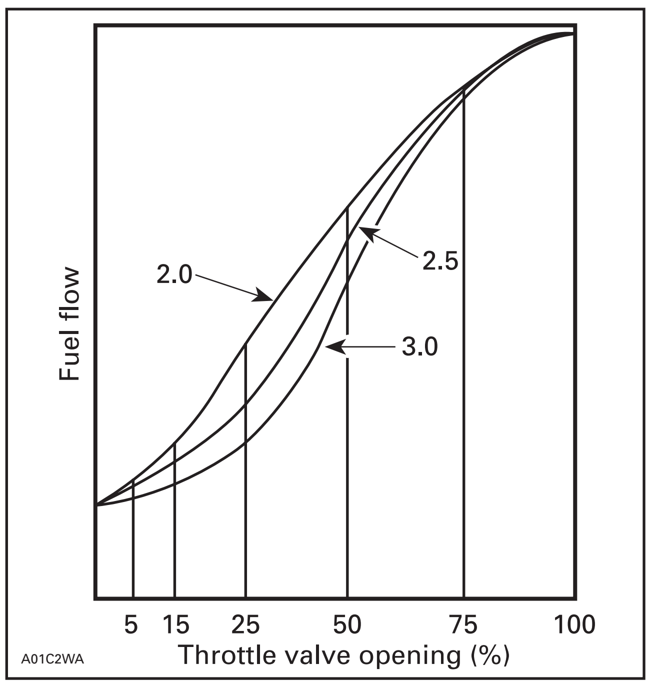
The throttle valve is cut away on the air inlet side to help control the fuel/air mixture at low and intermediate throttle settings. The size of cut-away also affects acceleration.

Throttle valves are numbered from 0.5 to 4.5 in 0.5 increments based on the size of the cut-away. The most commonly used configurations are 1.5 to 3.5. The higher the number, the greater the cut-away and the larger the air flow.

The throttle valve functions in about the same range as the pilot/air system. After the air screw is adjusted, it can be used to check the throttle valve selection.

NOTE: Too lean of a slide cut-away can cause piston seizures during sudden throttle closures from large throttle settings.

CHECKING AND SELECTING THROTTLE VALVE



1. Operate engine at low throttle settings, accelerating from idle to 1/4 throttle.
2. If engine bogs during acceleration, there is probably insufficient fuel. Turn in air screw about 1/4 turn at a time. If engine acceleration is improved, after adjusting air screw, the throttle valve cut-away needs to be decreased.

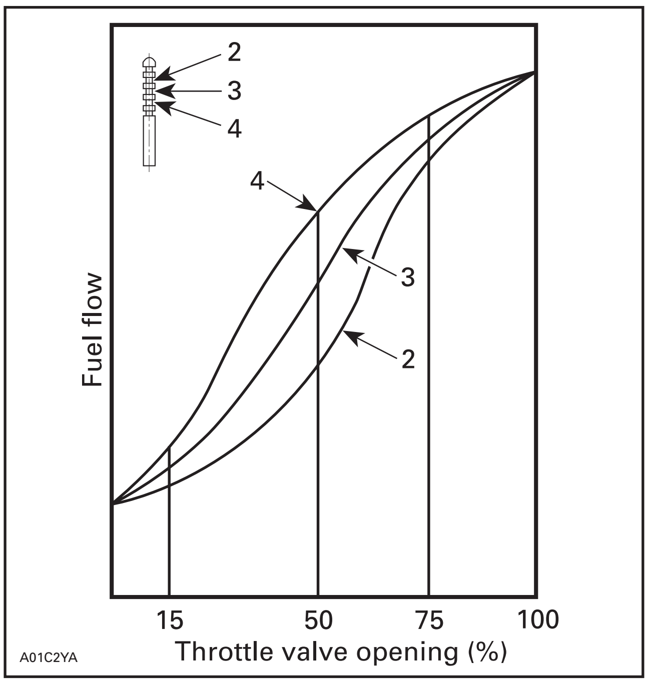
3. If engine runs rough or smokes excessively during acceleration, there is probably too much fuel. Turn out air screw 1/4 turn at a time. If engine operation is improved, the throttle valve cut-away needs to be increased.

NOTE: Illustration above indicates fuel flow according to throttle valve size and the amount throttle valve is opened.

4. Increase or decrease throttle valve cut-away size in 0.5 steps.
5. Return air screw to its original setting and operate engine at low throttle settings. Accelerate engine from idle to 1/4 throttle; engine should accelerate smoothly.
6. As a final check, change the position of the air screw. If this does not significantly affect engine performance (as in steps 2 and 3), the throttle valve is correct.

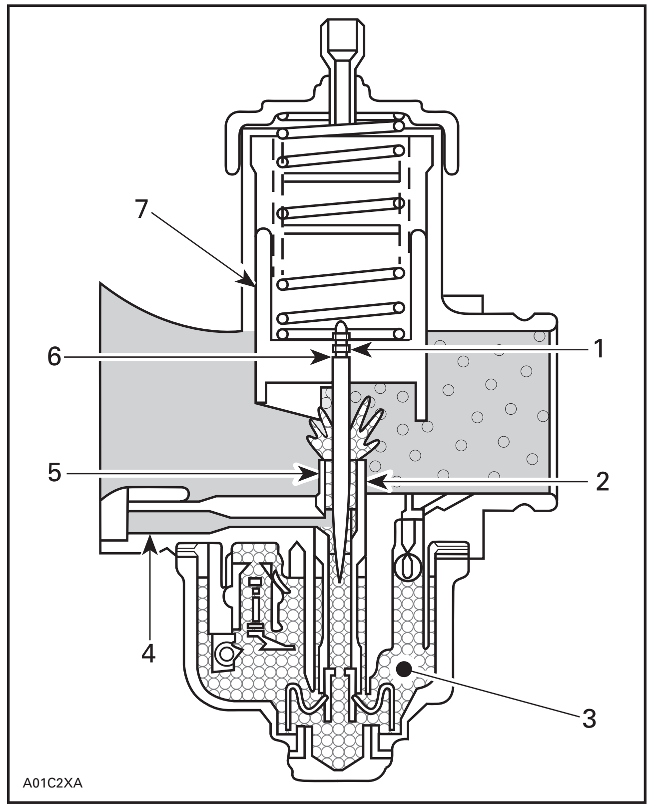
Jet Needle

PRINCIPLES OF OPERATION



The jet needle works with the needle jet to increase the amount of fuel as the throttle valve is raised.

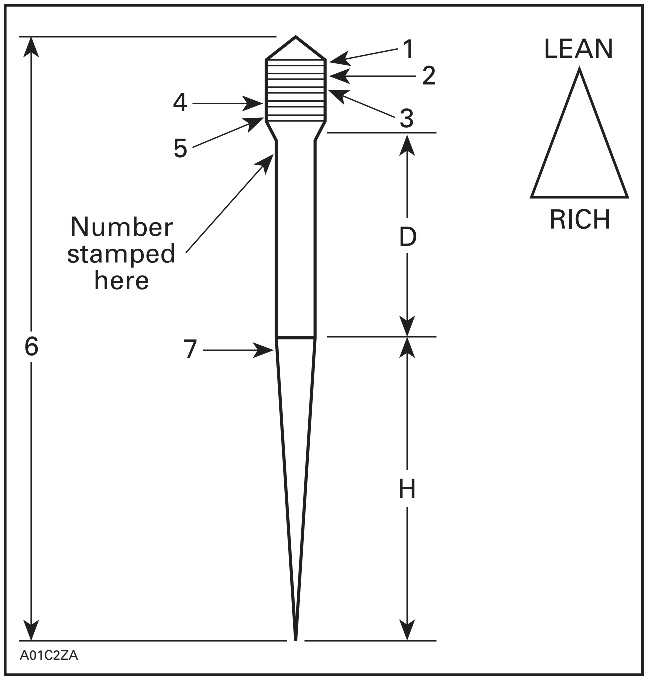
Although the jet needle and needle jet function in the 1/4 to 3/4 throttle range, they also affect the amount of fuel present at wide open throttle. When tuning the jet needle, also check main jet system operation.



1. *E-ring*
2. *Needle jet*
3. *Fuel*
4. *Air*
5. *Metered here*
6. *Jet needle*
7. *Throttle valve*

The jet needle raises and lowers with the throttle valve which changes jet needle position in the needle jet. Because the jet needle is tapered from top to bottom, an increasing amount of fuel is delivered through the needle jet whenever the throttle valve is raised. Increased or decreased air flow, by the throttle valve position, regulates the amount of fuel through the needle jet and around the jet needle.

The jet needle works on combination of length, taper, and E-ring position. Each jet needle has a number and letter series stamped on the body.



Example: 6DH7

6 - Basic length of needle.

DH - A single letter would indicate a single taper of the needle, double letter a double taper, and three letters mean there is a triple taper.

D - Amount of taper at top of needle.

H - Amount of taper at bottom of needle.

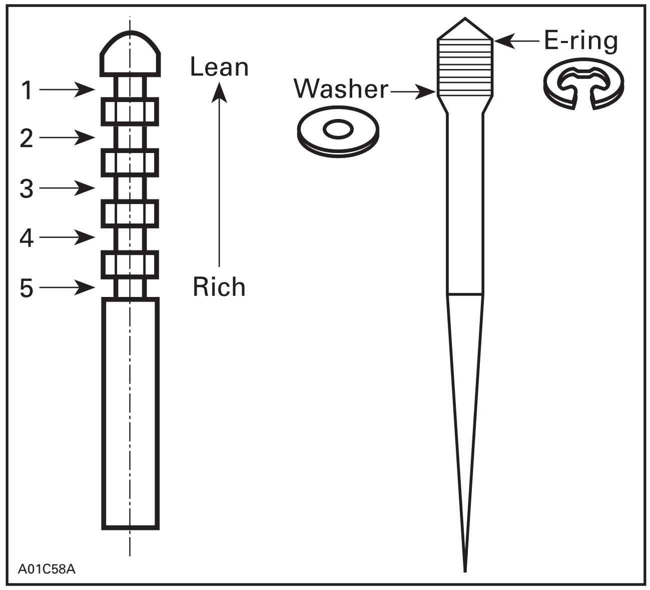
7 - Material, type of coating and start of second taper on needle.

NOTE: Letter designation of the jet needle indicates the angle of taper. Each letter (starting with A is 0.25° greater than preceding letter. Example: D = 1°, E = 1-1/4°, F = 1-1/2°, G = 1-3/4°, and H = 2°. This applies to both single and double taper needles.

At the top of the jet needle are five grooves numbered 1 through 5 from top to bottom. The number 3 or middle groove being the starting point for the E-ring. The E-ring position on any jet needle determines the rich or lean part throttle or mid-range carburetor operation.

Moving E-ring to position 1 or 2 lowers jet needle into needle jet and leans out the fuel/air mixture. Similarly, moving E-ring to position 4 or 5 raises jet needle in needle jet and enriches the fuel/air mixture.

POSITIONING THE E-RING



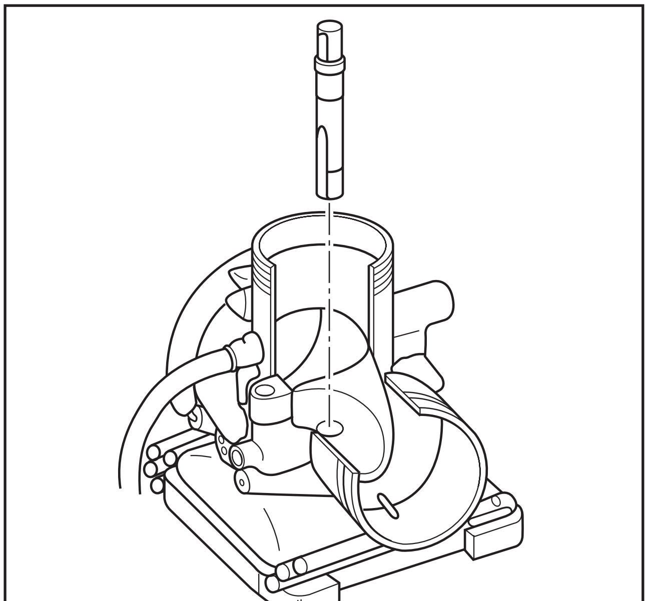
1 to 5 = E-ring position

1. Check for a rich or lean setting by examining exhaust manifold. A very light brown or white color indicates a lean mixture. A very dark brown or black color indicates a rich mixture. The proper color is tan.
2. Move E-ring one groove at a time to correct the fuel/air mixture.
3. If proper operation is obtained at all but the 3/4 throttle setting after the main jet has been tuned, operation may be improved by changing the jet needle taper. Do not, however, change the jet needle until main jet and E-ring position have been thoroughly checked.
4. If the E-ring is in the number 5 position and operation is still lean, a needle jet with a larger orifice may be installed. This may be done only after thoroughly checking the main jet, jet needle, and E-ring positions.

NOTE: Make sure washer is installed under E-ring on vehicles so equipped.

Needle Jet

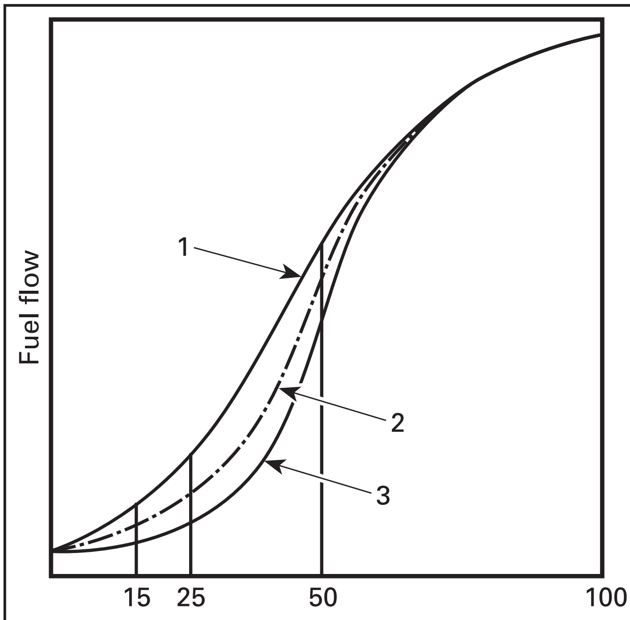
PRINCIPLES OF OPERATION



A01C4IB

The needle jet works in combination with the jet needle to meter the fuel flow in the mid range.

Changes to the needle jet should be made only if the results of changing the jet needle position are unsatisfactory. In stock applications, except for specific calibration changes necessary at high altitudes, the needle jet should not be changed. Selection of the proper needle jet requires much care and experience. Decreasing the needle jet size can prevent the main jet from metering the proper amount of fuel at wide open throttle.



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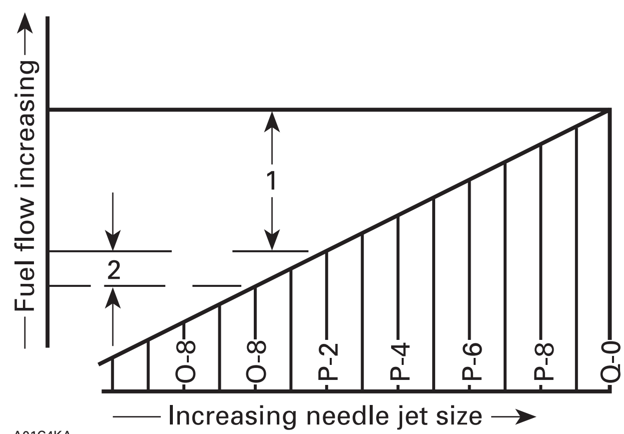


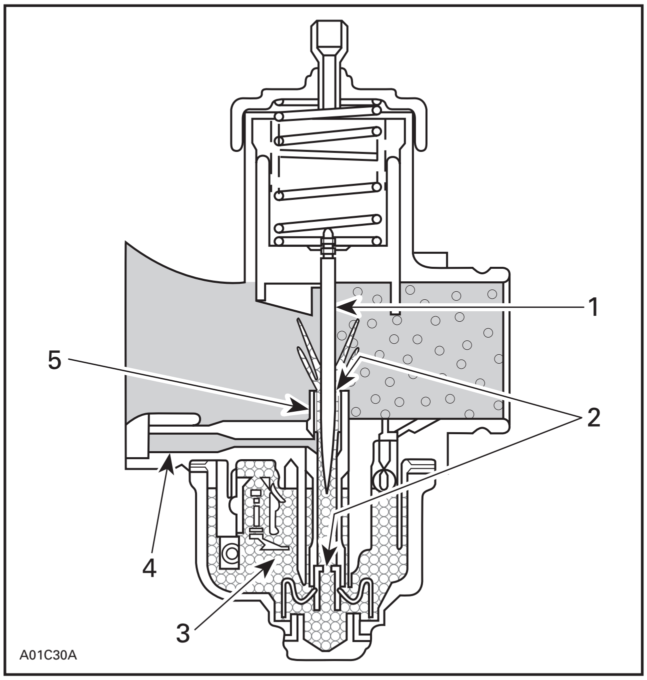
A01C4KA

Needle jets are stamped with an alphanumeric code. The letter indicates a major change in fuel flow. P-2, for example, indicates low flow; P-4, greater flow, and so on. The number indicates minor adjustments in fuel flow. The first diagram shows the relationship between the alphanumeric needle jet size number and fuel flow.

NOTE: Needle jets carrying the numbers 166, 159 or 169 in addition to the P-2 or P-4 and are not interchangeable. Be sure correct needles are used as specified for your snowmobile.

Main Jet System

PRINCIPLES OF OPERATION



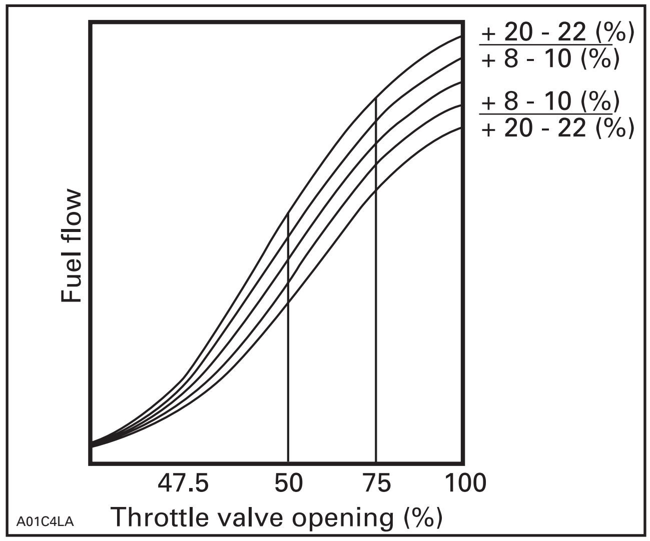
1. Jet needle
2. Metered here
3. Fuel
4. Air
5. Needle jet

The main jet system starts to function when the throttle is approximately 1/4 open. The mid range fuel is supplied by the main jet and regulated by the needle jet/jet needle combination. The main jet meters the fuel when the throttle is in the wide open position.

The main jets are available in sizes from number 50 to number 840. The size number corresponds to flow and not necessarily to hole size.

When experiencing erratic operation or overheating, check the main jet for dirt which can plug the orifice.

TUNING THE MAIN JET SYSTEM



Before operating the snowmobile, make sure all parts, including clutch and drive belt, are in good operating condition.

1. Operate snowmobile at wide open throttle for several minutes on a flat, well packed surface. Change main jet if snowmobile fails to achieve maximum RPM or labors at high RPM.
2. Continue to operate at wide open throttle and shut off ignition before releasing throttle. Examine exhaust manifold and spark plugs to determine if fuel/air mixture is too lean.

NOTE: Do not change jet sizes by more than one increment (step) at a time.

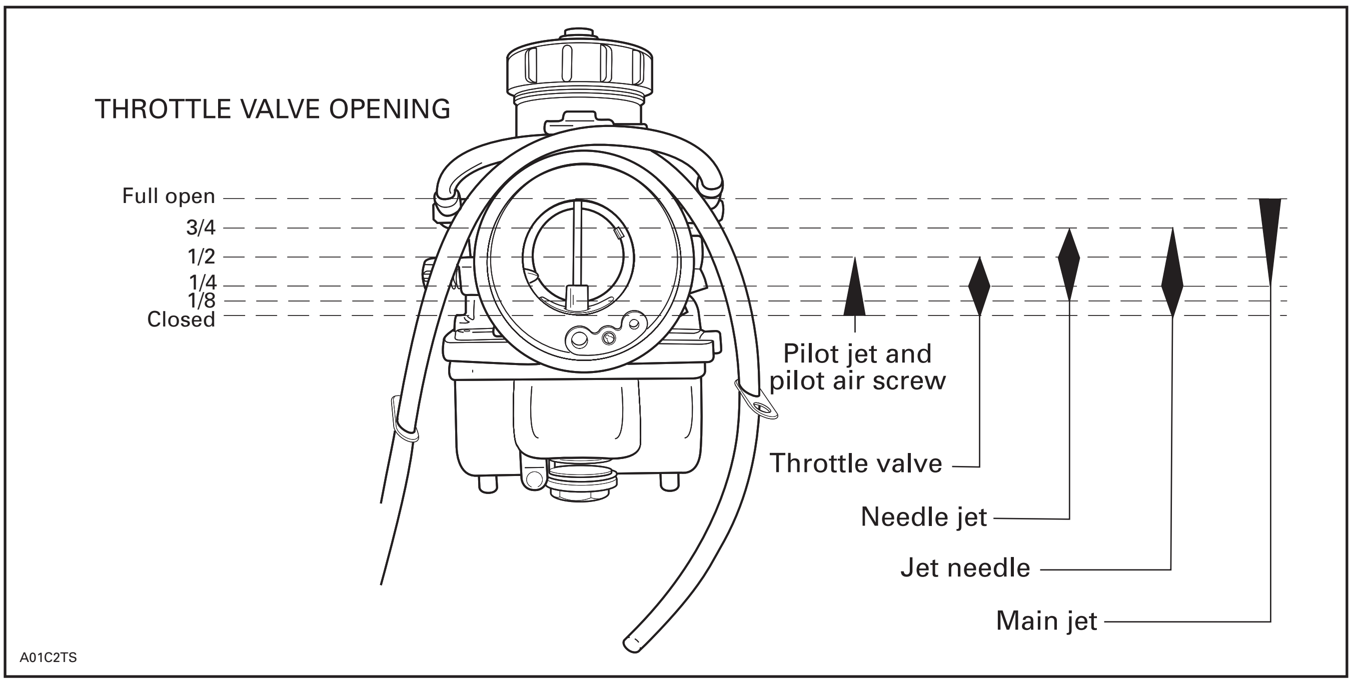
3. If the exhaust manifold or spark plug insulator is dark brown or black, the fuel/air mixture is too rich. Decrease jet size.
4. If the exhaust manifold or spark plug insulator is very light in color, the fuel/air mixture is too lean. Increase jet size.
5. If you cannot determine the color, proceed as if fuel/air mixture were too lean and increase jet size. If operation improves, continue to increase jet size to obtain peak performance. If operation becomes worse, decrease jet size to obtain peak performance.
6. After proper main jet is selected, recheck jet needle and needle jet.

Troubleshooting

When the carburetor setting is not correct for the engine, various irregularities are noticed. These can be traced to two causes as a whole:

1. When the air/fuel mixture is too rich:
   a. The engine noise is full and intermittent (four stroking).
   b. The condition grows worse when the enrichner is opened.
   c. The condition grows worse when the engine gets hot.
   d. Removal of the air cleaner will somewhat improve the condition.
   e. Exhaust gases are heavy.
   f. Spark plug is fouled.
2. When the air/fuel mixture is too lean:
   a. The engine overheats.
   b. The condition improves when the enrichner is opened.
   c. Acceleration is poor.
   d. Spark plug electrodes are melted.
   e. The revolution of the engine fluctuates and a lack of power is noticed.
   f. Piston seizure or scuffing occurs.

Functional Range Effectiveness in Relation to Throttle Opening

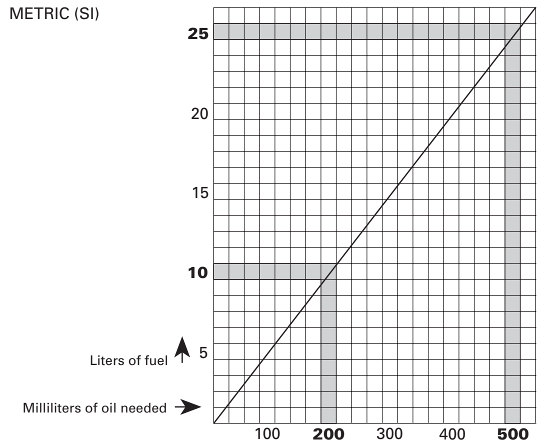


FUEL/OIL RATIO CHARTS

50/1

METRIC (SI)

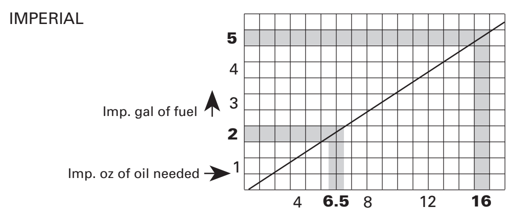
500 mL of oil + **25 L of fuel = 50/1**



IMPERIAL

16 oz of oil + **5 Imp. gal of fuel = 50/1**

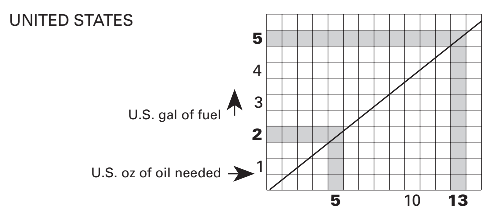
500 mL of oil + **5.5 Imp. gal of fuel = 50/1**



UNITED STATES

13 oz of oil + **5 U.S. gal of fuel = 50/1**

500 mL of oil + **6.6 U.S. gal of fuel = 50/1**



A00A1WJ

40/1

METRIC (SI)

500 mL of oil + **20 L of fuel = 40/1**

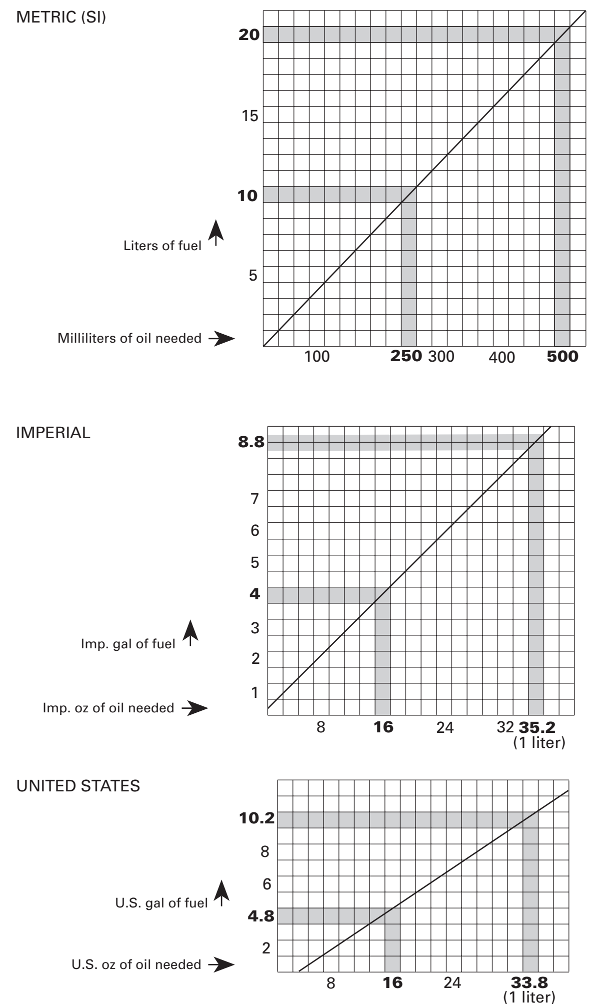
IMPERIAL

16 oz of oil + **4.0 Imp. gal of fuel = 40/1**

500 mL of oil + **4.8 Imp. gal of fuel = 40/1**

UNITED STATES

500 mL of oil + **5.3 U.S. gal of fuel = 40/1**



A00A2WJ

33/1

METRIC (SI)

500 mL of oil + **16.5 L of fuel = 33/1**

IMPERIAL

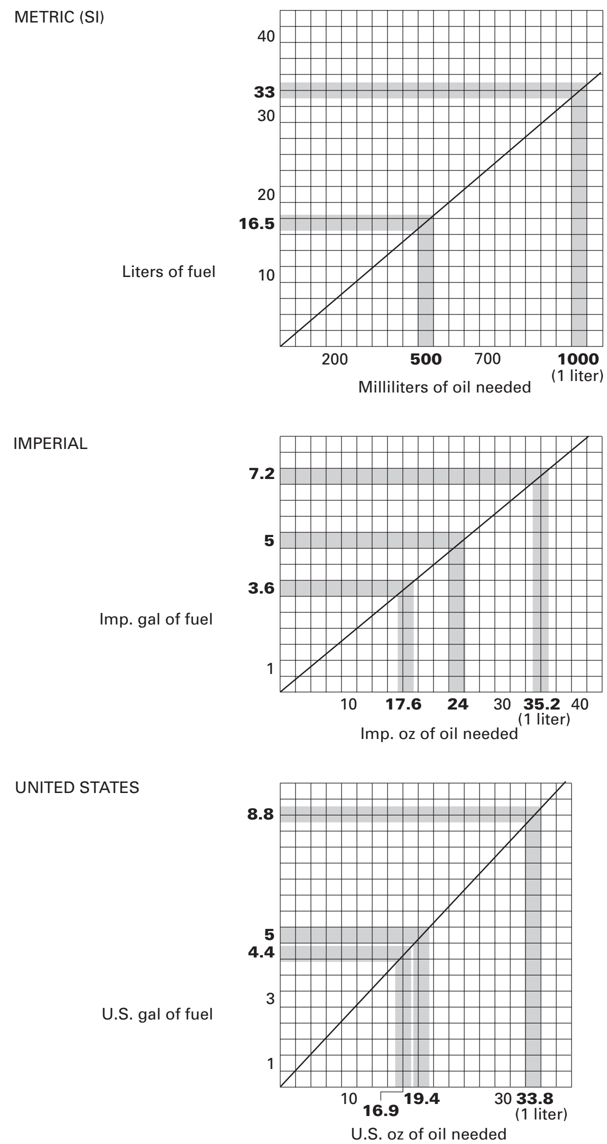
24 oz of oil + **5 Imp. gal of fuel = 33/1**

500 mL of oil + **3.6 Imp. gal of fuel = 33/1**

UNITED STATES

19.4 oz of oil + **5 U.S. gal of fuel = 33/1**

500 mL of oil + **4.4 U.S. gal of fuel = 33/1**



A00A6KJ

25/1

METRIC (SI)

500 mL of oil + **12.5 L of fuel = 25/1**

IMPERIAL

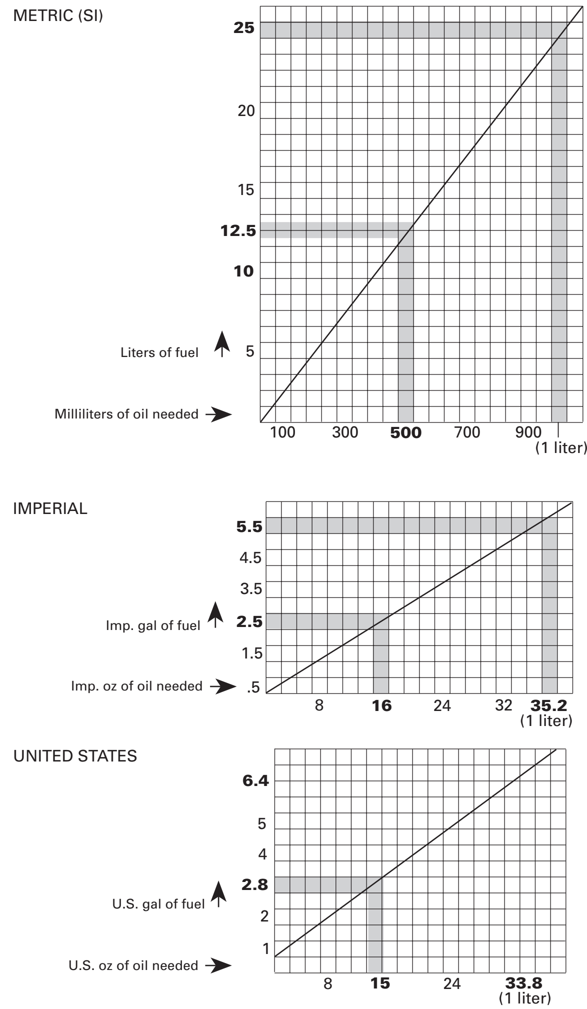
16 oz of oil + **2.5 Imp. gal of fuel = 25/1**

500 mL of oil + **2.7 Imp. gal of fuel = 25/1**

UNITED STATES

15 oz of oil + **2.8 U.S. gal of fuel = 25/1**

500 mL of oil + **3.2 U.S. gal of fuel = 25/1**



A00A2YJ

20/1

METRIC (SI)

500 mL of oil + **10 L of fuel = 20/1**

IMPERIAL

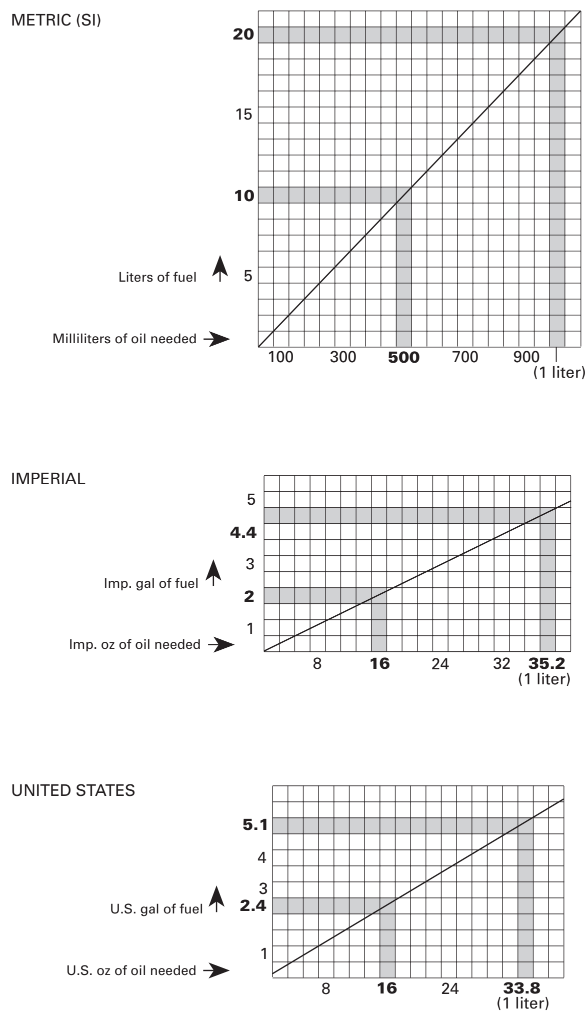
16 oz of oil + **2 Imp. gal of fuel = 20/1**

500 mL of oil + **2.2 Imp. gal of fuel = 20/1**

UNITED STATES

16 oz of oil + **2.4 U.S. gal of fuel = 20/1**

500 mL of oil + **3.2 U.S. gal of fuel = 20/1**



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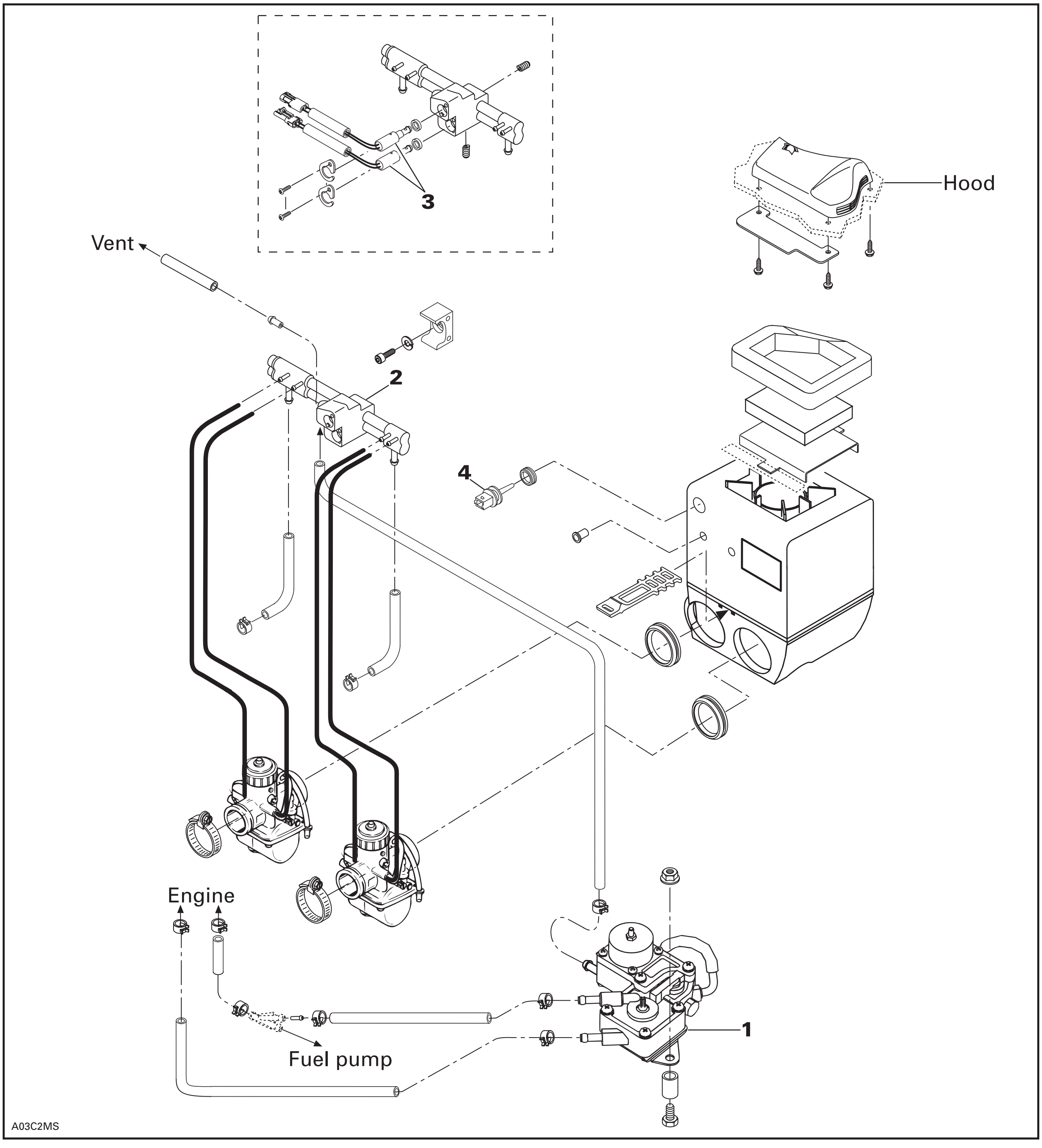
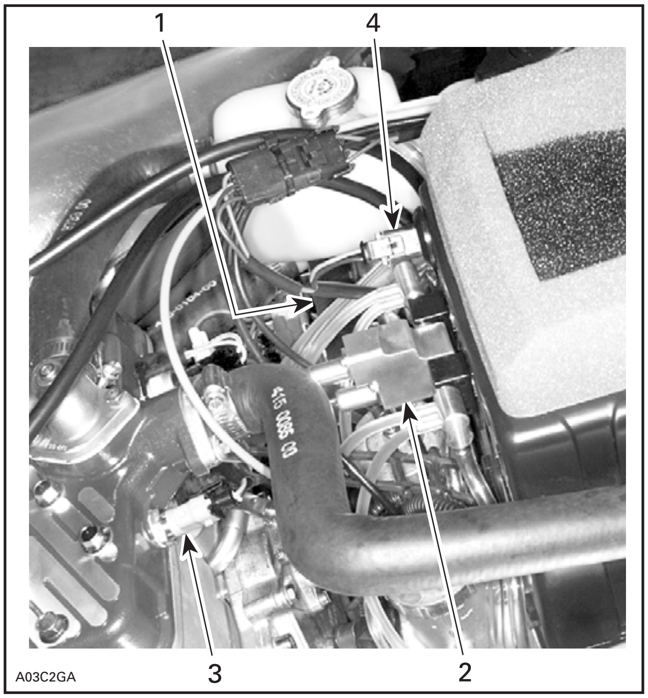
DIGITAL PERFORMANCE MANAGEMENT (DPM) SYSTEM



COMPONENT LOCATION



1. *MPEM module*
2. *Manifold*
3. *Engine temperature DPM sensor*
4. *Air temperature DPM sensor*

THEORY AND OPERATION

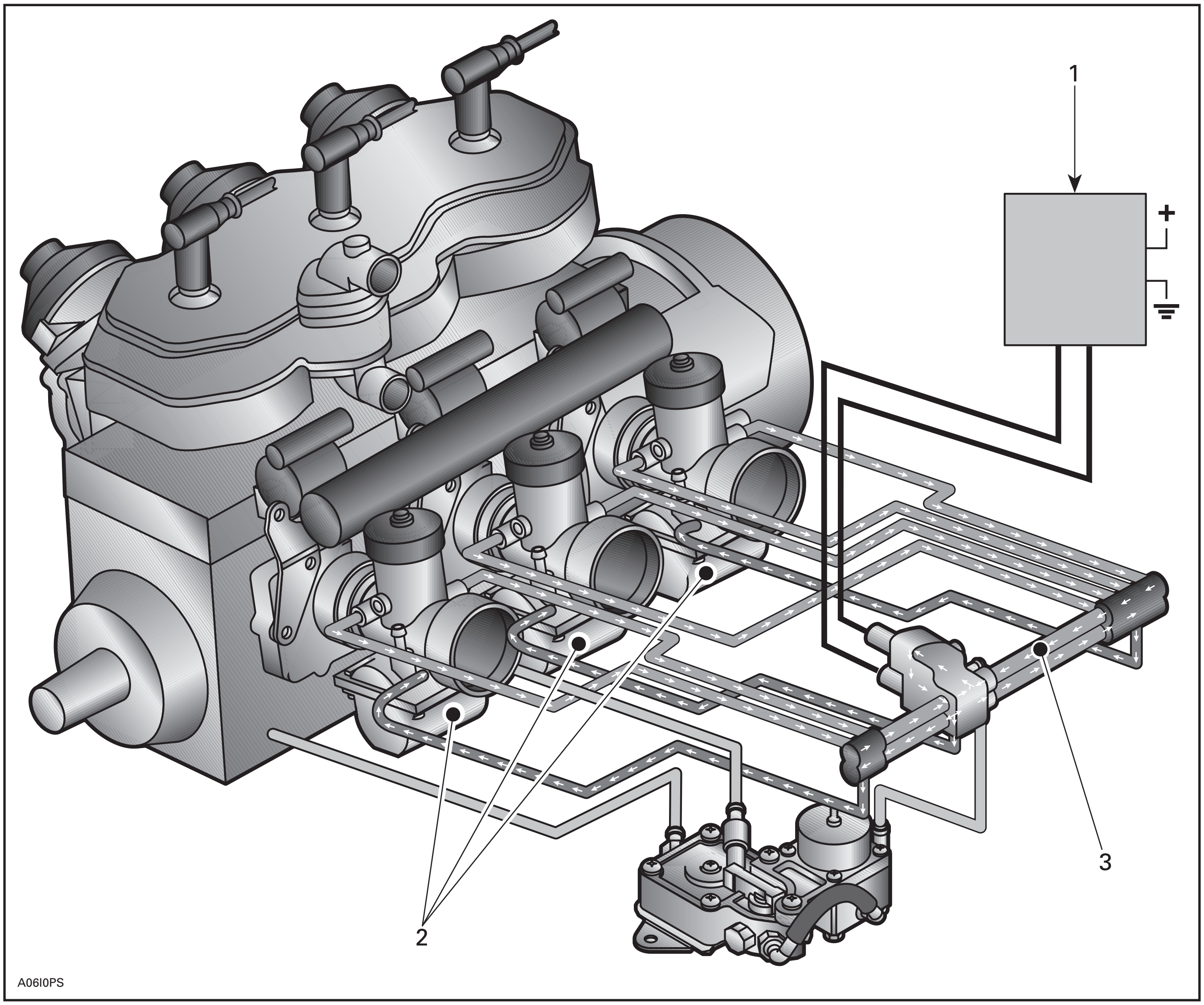
PURPOSE

Calibrate the air/fuel mixture in order to optimize the engine output while reducing fuel consumption.

METHOD

The system makes the pressure vary within the carburetor bowl.

OVERALL SYSTEM OPERATION



3 CYLINDER ENGINE SHOWN — SAME PRINCIPLE FOR 2 CYLINDER ENGINE

1. MPEM module
2. Carburetor bowls
3. Distribution gallery (upper tube)

Introduction

The engine is being started using the manual starter.

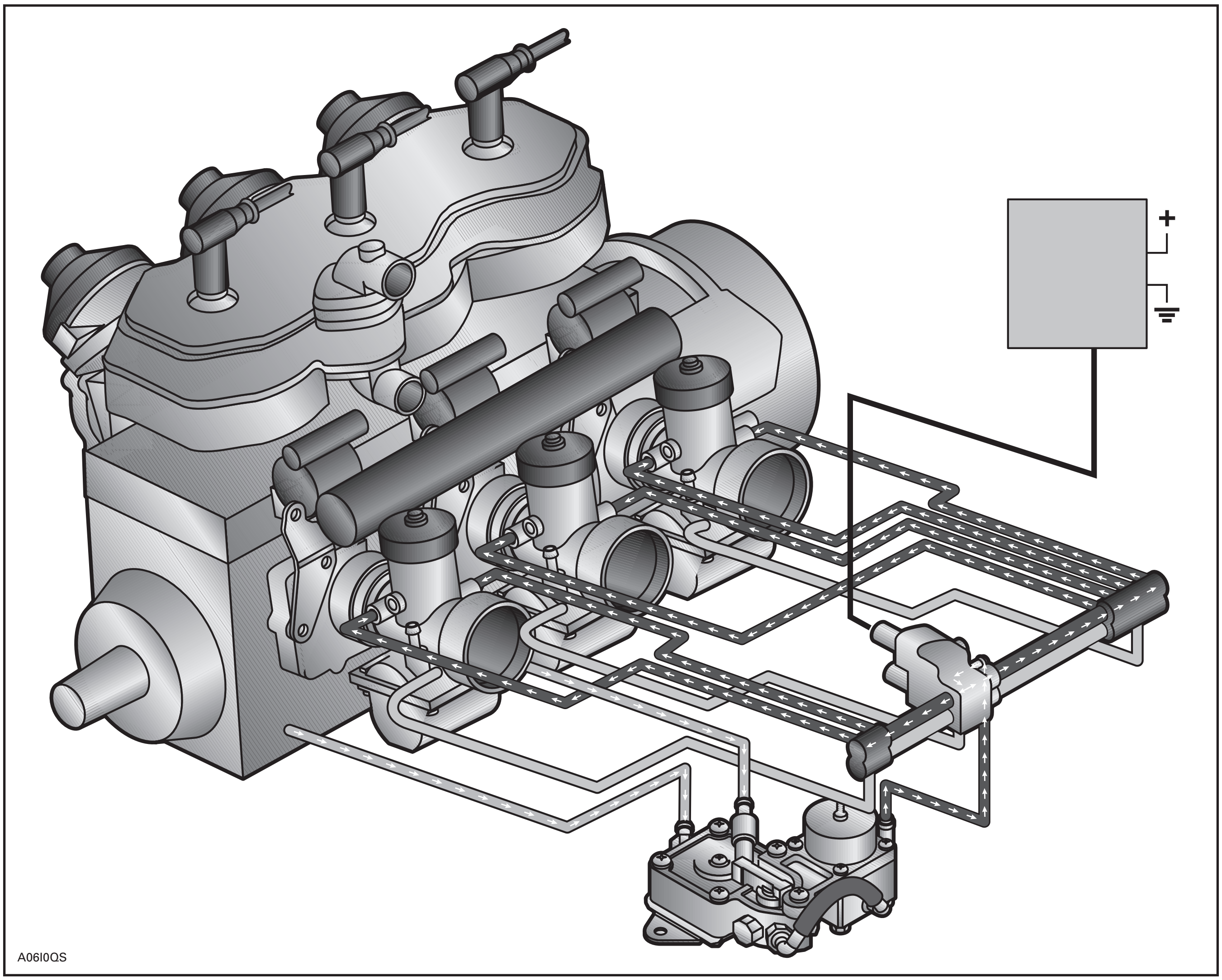
The Digital Performance Management (DPM) system increases pressure within all 2 carburetor bowls thus the air/fuel mixture is enriched. This is what we call the enrichment mode.

NOTE: On Summit x 670, use primer to ease cold starting. See STARTING PROCEDURE at the end of this section.

As soon as the spark plug gives off its first spark, the DPM system calculates the enrichment time and rate based on the engine temperature.

Once enrichment mode is completed carburetor bowls return to atmospheric pressure (DPM in standby mode), and the air/fuel mixture is identical to that of carburetors without the DPM system.

Enrichment Mode (starting)



TYPICAL

Over 3000 RPM, compensation mode is activated but will compensate only if the air temperature exceeds - 20°C (- 4°F) and the air pressure is lower than 1000 mbar.

Float bowls are now under vacuum (lower than atmospheric pressure) and the air/fuel mixture is leaner.

NOTE: On Summit x 670 both modes (enrichment or compensation) **can** operate at the same time.

DPM SYSTEM OPERATION

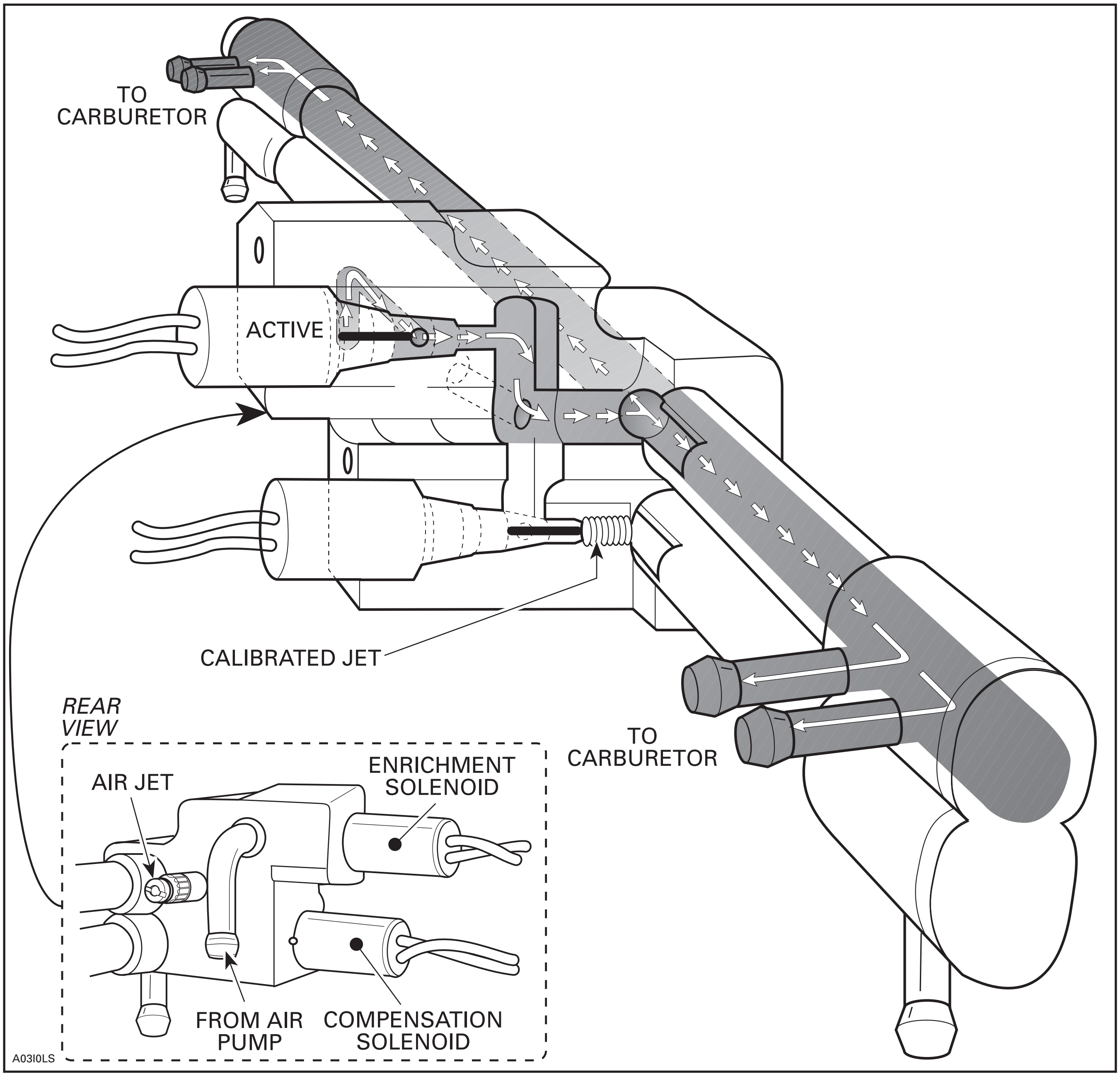
BLACK and WHITE/GRAY wires (2-05 housing) are used for programming by the manufacturer. Nothing must be plugged to this housing.

Turning the ignition key to the ON position will not energize DPM system. The DPM system is energized only.

Once the engine turns over 250 RPM.

The DPM system then comes on by reading the engine temperature through the sensor located on the cylinder head. The DPM system calculates the enrichment solenoid opening time (duty cycle) and the enrichment rate according to the temperature. The air/fuel mixture is then enriched in order to facilitate starting.

The system pressurizes both carburetor bowls in order to enrich the air/fuel mixture. This is accomplished with the help of an air pump.



This enrichment mode of the air/fuel mixture takes place at start-up and during engine warm-up, and it depends on engine temperature.

The higher the engine temperature upon start-up, the leaner the mixture.

This enrichment mode progressively decreases (with time) by reducing the solenoid duty cycle. The warmer the engine, the shorter the enrichment mode.

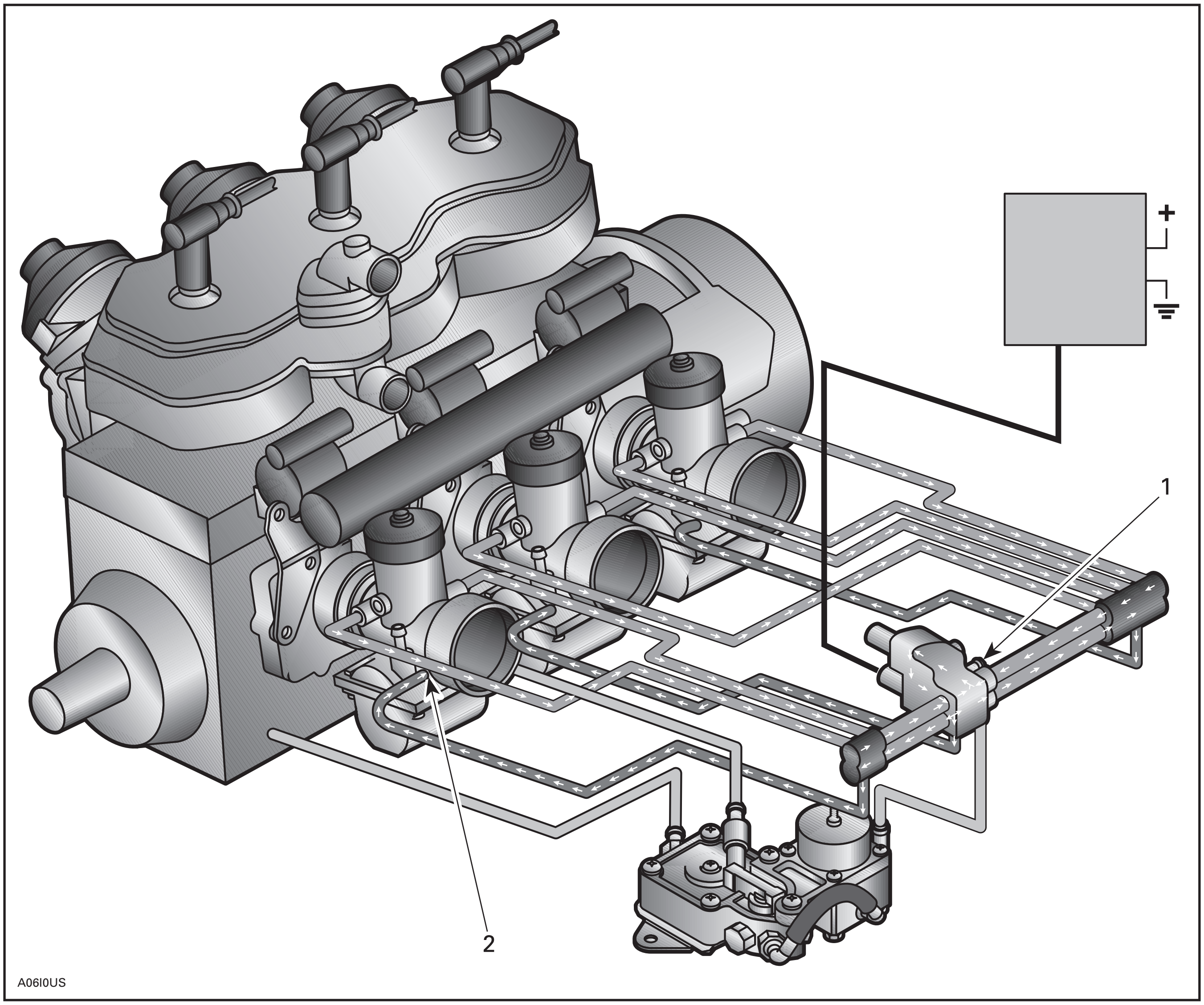
If the throttle opening exceeds one quarter, the enrichment mode is interrupted by a switch during the starting process, which allows unflooding the engine.

However, the enrichment mode is restored when releasing the throttle.

Following the enrichment mode, carburetors are operating normally, i.e. without additional pressure within bowls.

NOTE: Calibration is exactly the same on engines with a DPM system and those without.

Compensation Mode



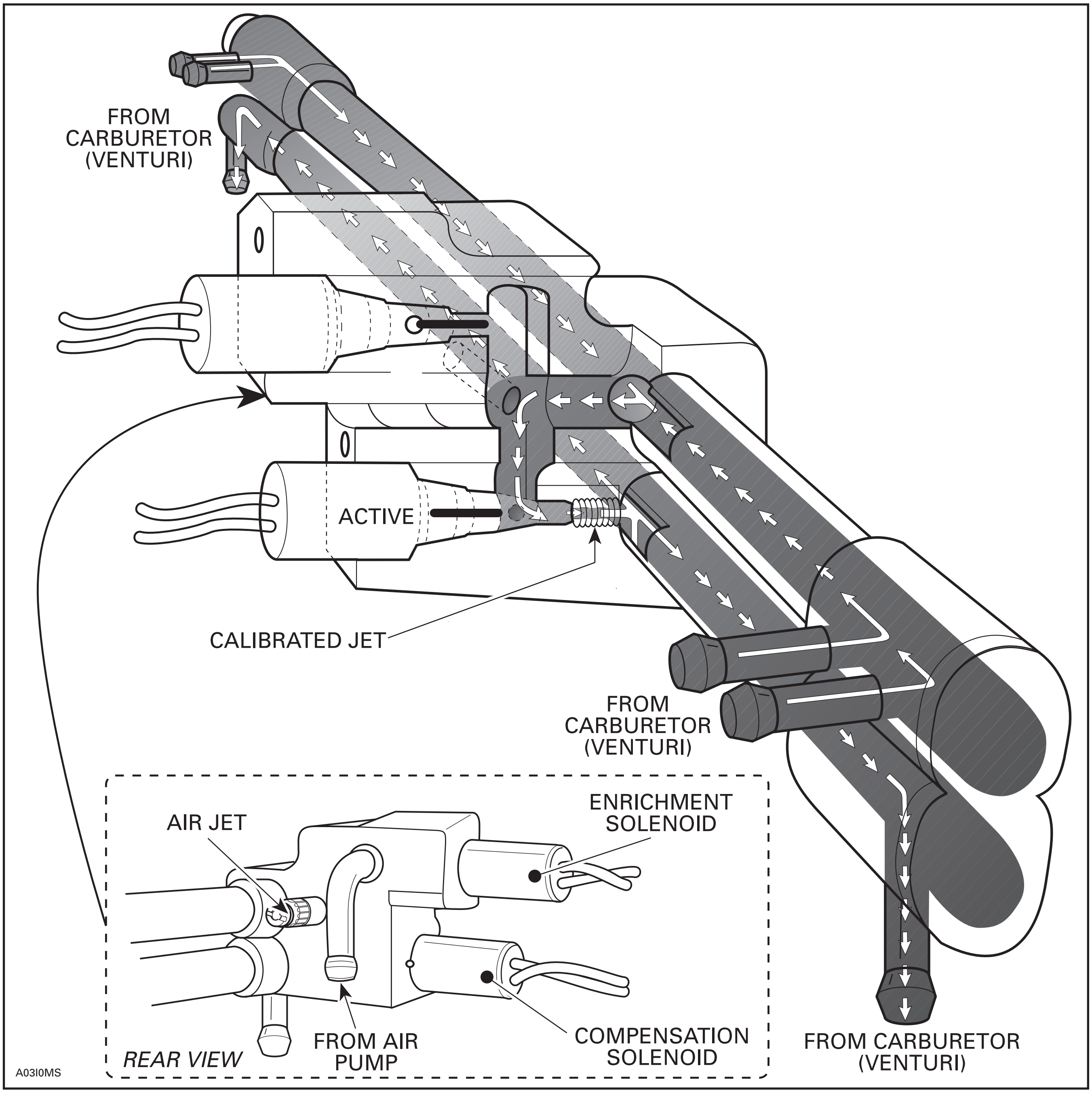
1. Air jet
2. Needle jet air inlet

Three conditions must be met for the compensation mode to operate:

1. Engine must rev over 3000 RPM.
2. Air temperature must exceed - 20°C (- 4°F).

3. Atmospheric pressure must be lower than 1000 mbar.

The compensation system brings both carburetor bowls under vacuum (lower than atmospheric pressure) in order to make the air/fuel mixture leaner. The required vacuum is produced within the needle jet air inlet.



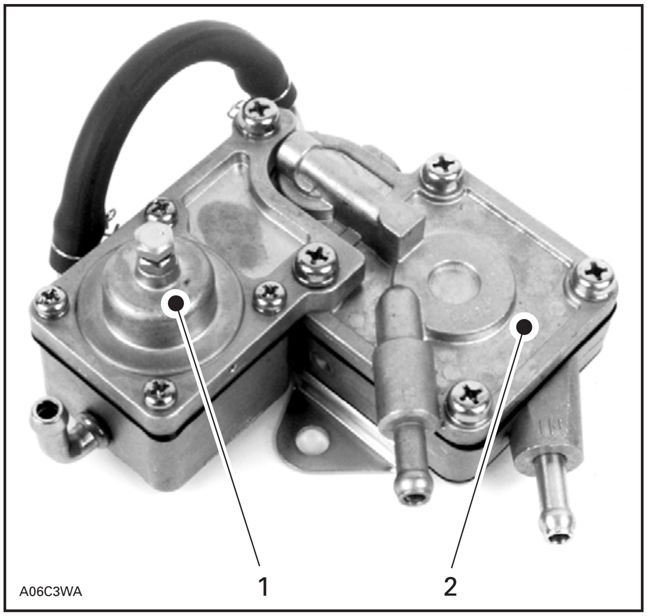
The compensation ratio will depend on the air temperature and the atmospheric pressure.

The higher the air temperature, the leaner the air/ fuel mixture.

The lower the atmospheric pressure, the leaner the air/fuel mixture.

NOTE: The atmospheric pressure decreases as the altitude increases.

AIR PUMP OPERATION



TYPICAL
1. *Regulator*
2. *Pump*

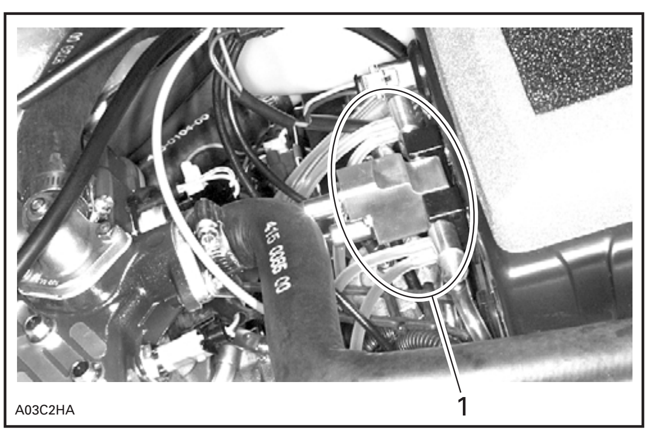
Air pump **no. 1** supplies the distribution gallery through a unique pipe.

Pump diaphragm is activated by the alternating pressure/vacuum within the engine crankcase. Two pipes connect the crankcase (cylinders nos. 1 and 2) to the pump.

A regulator within the pump stabilizes the pump pressure.

Since the pump pressure is insufficient upon starting, the regulator is fed directly by the crankcase pressure.

DPM MANIFOLD OPERATION

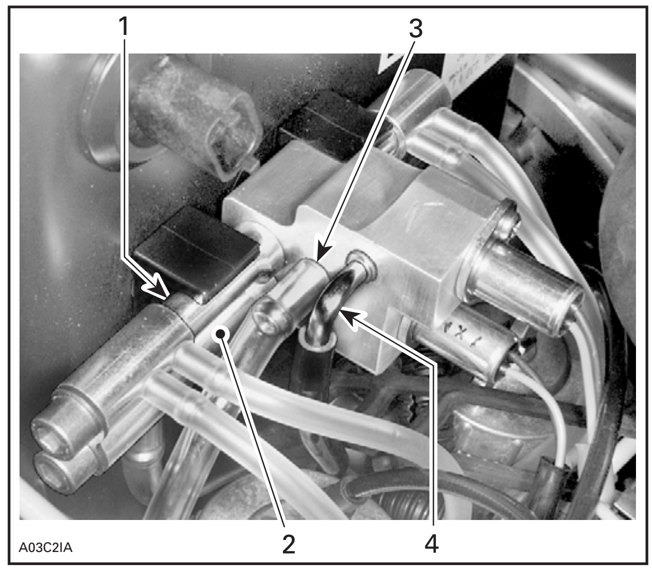


1. *Manifold*

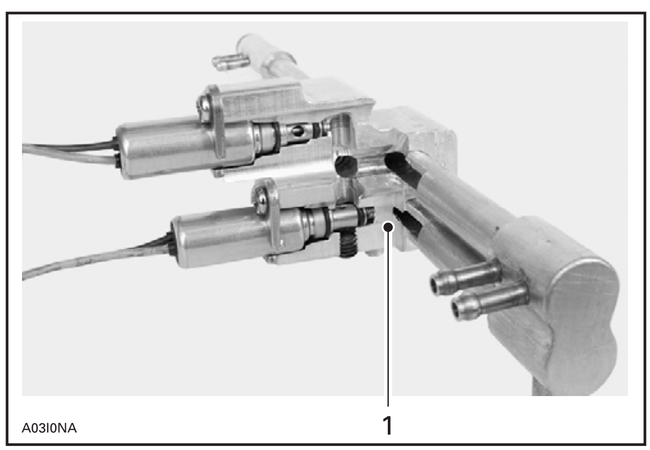
The DPM manifold **no. 2** consists of 2 tubes. Depending on the mode, the upper tube (distribution gallery) distributes pump pressure or vacuum to each bowl through 2 pipes. The passage is then opened by the enrichment or the compensation solenoid, depending on the mode.

The lower tube (vacuum collector) receives the vacuum created by each carburetor within the needle jet air inlet.

An air jet (manifold air jet) also allows the atmospheric pressure to enter.



MANIFOLD ASS'Y
1. *Upper tube: distribution gallery*
2. *Lower tube: vacuum collector*
3. *Manifold air jet (1.2 mm) — atmospheric pressure*
4. *From air pump*



TYPICAL
1. *Compensation solenoid air jet (1.4 mm)*

Enrichment Solenoid

Solenoid Operating Principle

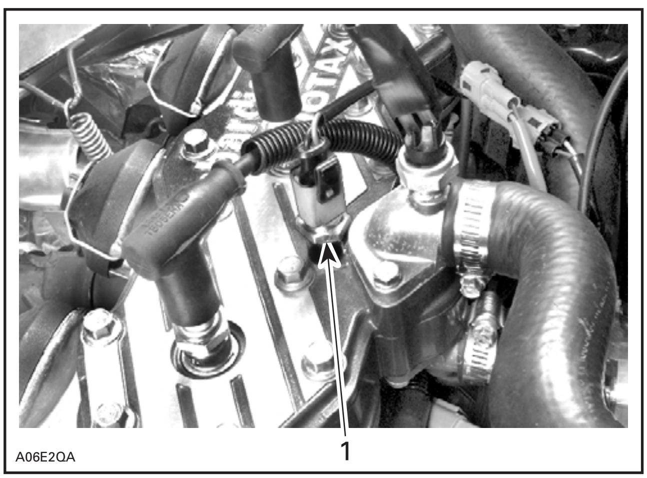
A solenoid is a winding coiled in order to produce a magnetic field. A metal rod crosses the coil and cuts the magnetic field. Each time the coil is activated, the magnetic field attracts the rod. If the supply current is interrupted, a spring pushes the rod.

Solenoid Function within the DPM System

The DPM system turns the solenoid **no. 3** ON and OFF 10 times per second, which means that it operates at 10 cycles/second or 10 Hertz (Hz). The solenoid therefore opens and closes 10 times per second, thus allowing the pump pressure to reach the distribution gallery (upper tube).

For the pressure to vary within the bowls, the solenoid is activated in part by the DPM during each cycle. This is what is called the duty cycle. In other words, the solenoid will not open throughout the whole cycle. The duty cycle depends on the engine temperature.

The colder the engine, the longer the duty cycle. Therefore, the solenoid will stay open longer, thus giving way to pressure.



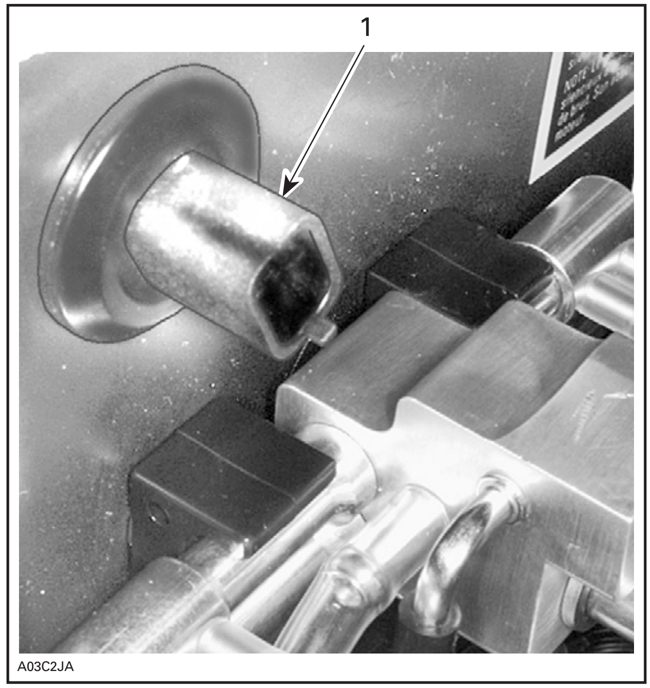
1. *Engine temperature DPM sensor*

Compensation Solenoid

NOTE: Same principle as enrichment solenoid. Read **Solenoid Operating Principle** at the beginning of the chapter concerning the enrichment solenoid.

The duty cycle of the compension solenoid depends on the air temperature and the atmospheric pressure.

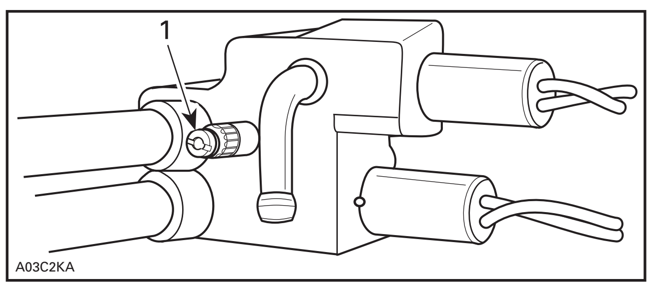
The warmer the air, the longer the duty cycle. Therefore, the solenoid will stay open longer, thus giving way to vacuum. The same applies when the altitude increases.



1. *Air temperature sensor*

Manifold Air Jet

This jet allows the atmospheric pressure to reach carburetor bowls when the DPM SYSTEM is on standby (returned to atmospheric pressure).



REAR VIEW

1. *Atmospheric pressure air jet*

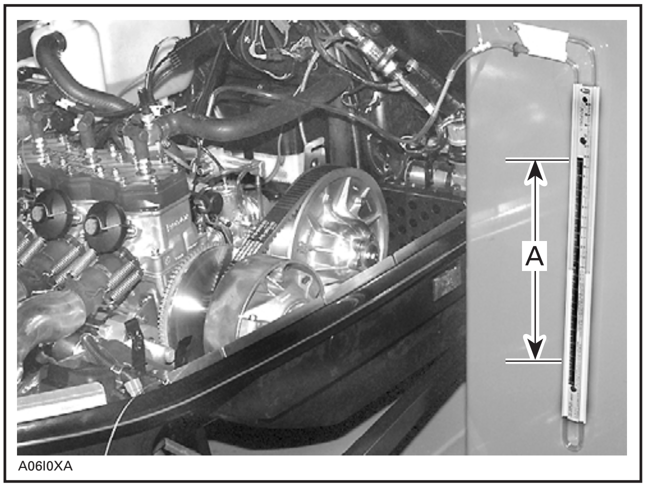
TESTING PROCEDURE

Pump

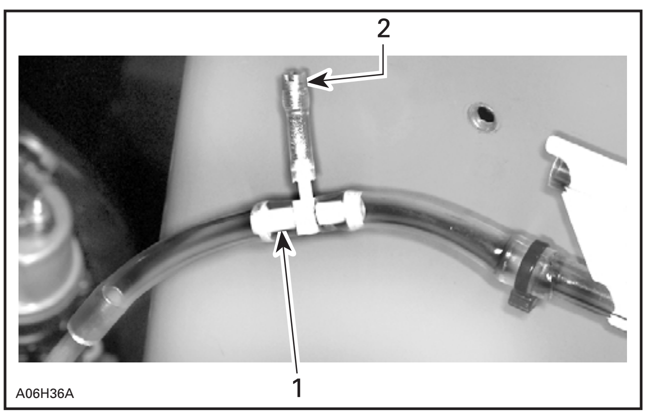
Pressure Test

The pump must create a minimum pressure of 400 ± 50 mm of water.

Connect a jet (P/N 270 500 157) to a hose then connect that little tube to the small nipple of a T-fitting (P/N 414 222 500). Install that T-fitting between a U-tube and air pump outlet.



TYPICAL
A. 400 ± 50 mm of water



1. *T-fitting (P/N 414 222 500)*
2. *Jet (P/N 270 500 157)*

Start engine and note water height.

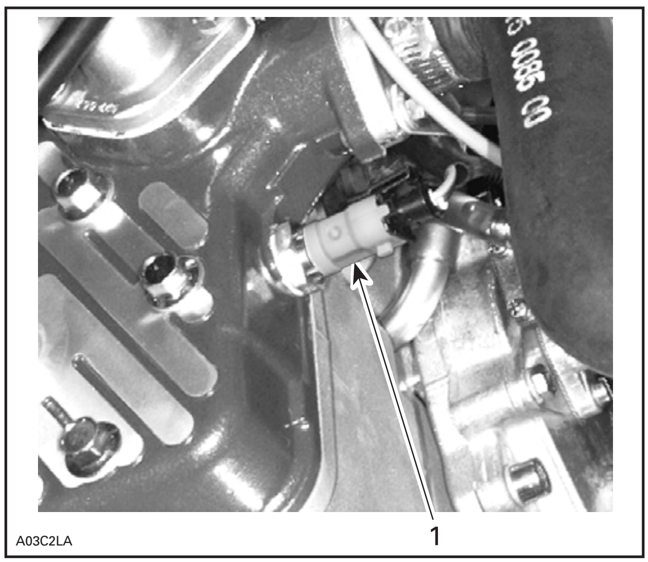
DPM System

Solenoids are supplied by the MPEM module. If this module does not work, there will be no current on compensation solenoid RED/BLUE and BLACK connectors (3-10 housing); and on enrichment solenoid RED/GREEN and BLACK connectors (3-11 housing).

Unplug upper solenoid wire (enrichment). Connect a good solenoid to module output connector. Use adaptor (P/N 529 033 800) as required.

CAUTION: Do not disconnect both DPM connectors. The compensation solenoid must remain plugged.

Disconnect engine temperature sensor connector. The DPM system now operates as though the engine temperature was - 20°C (- 4°F) to allow maximum mixture enrichment.



1. *Engine temperature sensor*

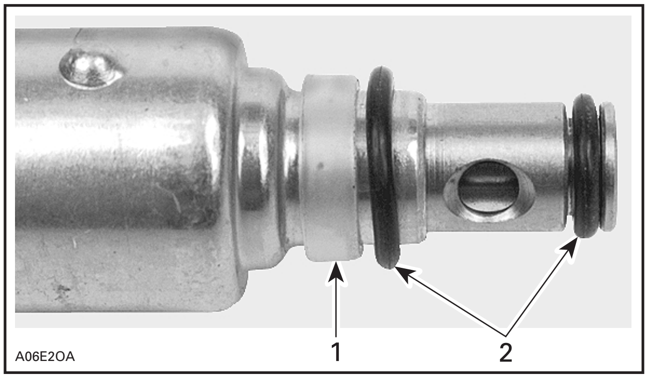
Start the engine and observe the solenoid. A vibrating solenoid indicates that the module is in good working order. If not, replace the module and repeat test.

Solenoid

Static Test

Disassemble the solenoid and connect it to a 12 V battery. The solenoid must open and stay open. Repeat test several times.

At reassembly, ensure that solenoid seals are in place.



1. *Plastic seal*
2. *O-rings*

Dynamic test

When checking the enrichment solenoid, disconnect engine temperature sensor connector. The DPM system now operates as though the engine temperature was - 20°C (- 4°F) to allow maximum mixture enrichment.

Remove the solenoid, hold it in hand and start the engine.

For the enrichment solenoid, check if it vibrates as soon as the engine is started.

For the compensation solenoid, the air temperature sensor **no. 4** must be at room temperature. Operate the engine at 3500 RPM. The solenoid must vibrate.

Temperature Sensor (air and engine)

At room temperature 20°C (68°F), the sensor resistance must be 2500 Ω ± 300.

STARTING PROCEDURE

Apply brake.

Check throttle lever operation. Make sure it returns to idle position when released.

Ensure that the emergency cut-out switch is in the ON position.

Ensure that the tether cut-out cap is on the DESS post and that the cord is attached to your clothing.

Initial Cold Starting

NOTE: Do not operate the throttle lever.

Above Freezing Point Temperature (0°C)

Grasp manual starter handle firmly and pull vigorously to crank engine.

If engine refuses to start, activate the primer button once then crank the engine again.

Below Freezing Point Temperature (0°C)

Activate primer button 2 or 3 times before cranking engine to inject fuel into intake manifold.

In extremely cold temperature, more priming may be required.

After the engine is started, the Digital Performance Management (DPM) system will control the carburation.

Warm Engine Starting

Priming is not necessary when engine is warm.

Crank engine normally without operating the throttle lever.

IMPORTANT: Operating the throttle lever while cranking the engine will deactivate the DPM system.

IGNITION SYSTEMS, SPARK PLUGS

Two-stroke engines in snowmobiles rely on an electric spark to initiate combustion of the fuel/air charge which has been inducted into the cylinder. For the engine to operate efficiently, the spark must be delivered at precisely the right moment in relation to the position of the piston in the cylinder and the rotational speed of the crankshaft.

Additionally, the spark must be of sufficient intensity to fire the fuel mixture, even at high compression pressure and high RPM.

It is the function of the ignition system to generate this voltage and provide it to the spark plug at the correct time.

The Nippondenso capacitor discharge ignition (CDI) system has magnets located on the crankshaft flywheel. AC voltage is induced in the generating coil(s) as the poles of the magnets rotate past the poles of the coils. Timing is controlled by a trigger coil or the position of the coil poles relative to the magnet poles, which are directly related to piston position. The CD (or amplifier) box contains the electronic circuitry to store and control the initial voltage and deliver it to the ignition coil (and then the spark plug) at the correct moment. The ignition coil is a transformer that steps up the relatively low voltage, 150-300 V, of the generating coil to the 20,400 – 40,000 volts necessary to jump the spark plug gap and initiate the burning of the fuel/air mixture in the combustion chamber.

Maximum power from a given engine configuration is produced when peak combustion chamber pressure (about 750 PSI) takes place at about 15° of crankshaft rotation ATDC. Normal combustion is the controlled burning of the air/fuel mixture in the cylinder. The flame is initiated at the spark plug and spreads to the unburned mixture at the edges of the cylinder.

This flame front travels through the cylinder at about 100 feet per second. In order to achieve maximum pressure at about 15° ATDC, the spark must occur about 15° before TDC. Complete combustion will finish at about 35° ATDC. The actual amount of spark advance BTDC is dependent upon bore size, combustion chamber shape, operating RPM, mixture turbulence and the actual flame speed.

Flame speed is directly proportional to piston speed in an almost linear fashion. Though it is not completely understood why this relationship exists, it is thought to be related to intake speed and mixture turbulence. Hence, flame speed increases as RPM increases. It also increases as the air/fuel ratio becomes leaner.

Because the flame speed is slower at lower RPM's, more advance at low RPM is necessary for maximum performance. Advancing the spark too much BTDC for the needs of the engine will cause the engine to go into detonation.

The optimum ignition would then have timing significantly advanced at lower RPM, but would retard the timing at higher RPM to keep the engine out of detonation. Generally, as the ignition timing is advanced, the low end mid range power will be improved and the peak power will be moved to a lower RPM. Retarding the timing will generally reduce low and mid range power but may allow jetting to be leaner and increase peak power. Peak power will be moved to a higher RPM. These are generalizations and ignition timing must be optimized depending on engine design, RPM range and operating conditions.

Ignition advance on Rotax engines is measured by a linear distance of piston travel BTDC. A dimension taken through a straight spark plug hole in the center of the head is a direct measurement. A dimension through an angled plug hole on one side of the head is an indirect measurement. A direct measurement can be converted to degrees of crankshaft rotation by the appropriate formulas. Initial ignition timing procedures can be found in the *Shop Manual* for the particular model being worked on.

Starting with most 1990 Ski-Doo models, a Nippondenso CDI system with only one generating coil was introduced. This system is identified by having only two wires running from the stator plate to the CD box.

Ignition Timing

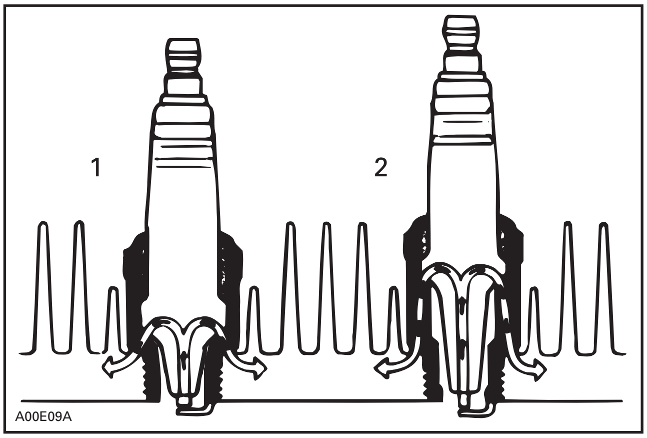
Ignition timing is no longer able to be adjusted mechanically. It must be done by your dealer with an MPEM programmer.

Spark Plug Heat Range

Spark plug heat ranges are selected by measuring actual combustion chamber temperatures. A colder spark plug, one that dissipates heat more rapidly, is often required when engines are modified to produce more horsepower.

The proper operating temperature or heat range of the spark plugs is determined by the spark plugs ability to dissipate the heat generated by combustion.

The longer the heat path between the electrode tip to the plug shell, the higher the spark plug operating temperature will be — and inversely, the shorter the heat path, the lower the operating temperature will be.



1. *Cold*
2. *Hot*

A cold type plug has a relatively short insulator nose and transfers heat very rapidly into the cylinder head.

Such a plug is used in heavy duty or continuous high speed operation to avoid overheating.

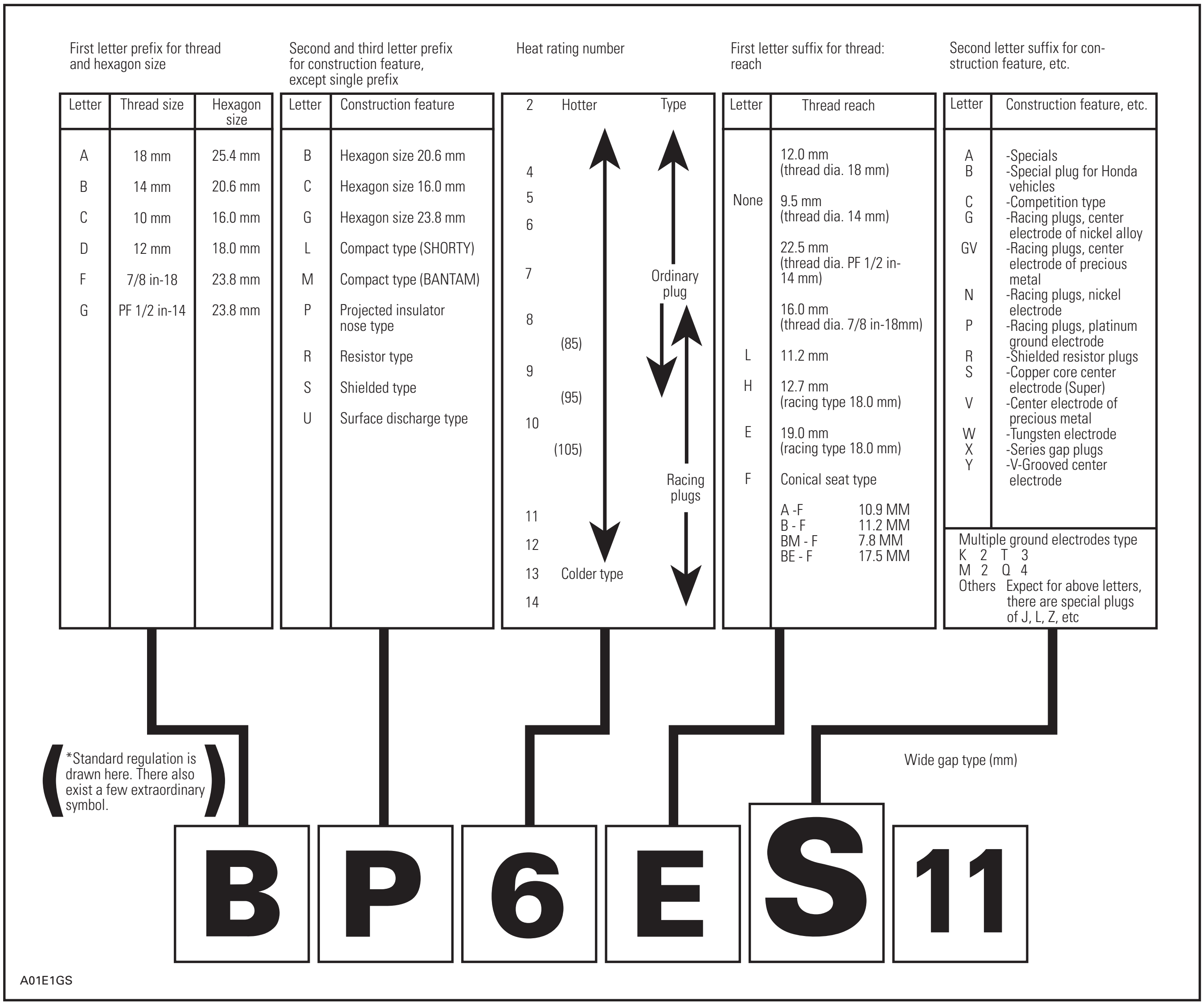
The hot type plug has a longer insulator nose and transfers heat more slowly away from its firing end. It runs hotter and burns off combustion deposits which might tend to foul the plug during prolonged idle or low speed operation.

Generally speaking, if you have increased horsepower by 10-15%, you will have to change to the next colder heat range spark plug.

Most Ski-Doo's are equipped stock with NGK BR-9ES spark plugs.These are resistor-type plugs which help reduce radio frequency interference.

To help prevent spark plug fouling use BR9ECS type plug. Used ONLY resister type plugs.

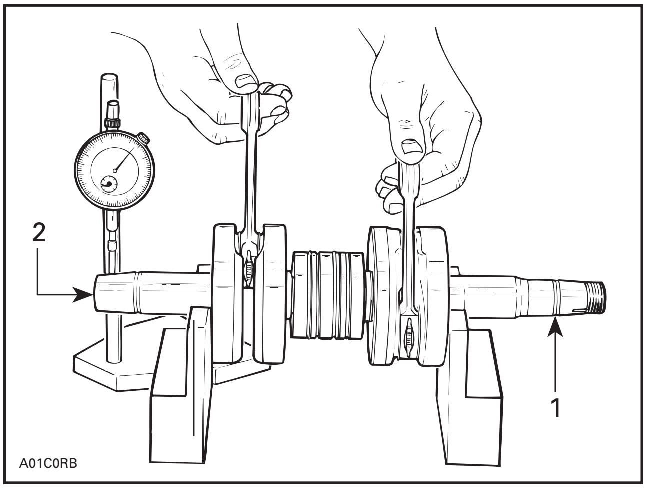
Design Symbols Used on NGK Spark Plugs



STOCK CLASS PREPARATION

NOTE: Any machining and/or grinding is illegal in stock class racing. Keep your machine legal!

1. Remove and disassemble the engine according to correct *Shop Manual* procedures.
2. With the crankshaft resting in the lower half of the crankcase, set up a dial indicator and check the run out of the crankshaft at both ends. You should see no more than 0.05 mm (0.002 in) run out. If you have the capability, adjust the crankshaft as close to perfect as possible.



1. Measure behind the key
2. Measure at 6 mm (1/4 in) from edge

3. Set your cylinder base gaskets and cylinders on the upper half of the crankcase, and lightly torque the cylinders to the half. Be sure to install exhaust manifold on the cylinders before tightening them to the upper crankcase half to ensure the same position of the cylinders on final assembly.

Check the match of the gaskets and cylinders to the base; match them perfectly with a die grinder in the areas of transfer port passages. Also check for any over lap of the exhaust manifold gaskets where the exhaust manifold joins the cylinders. Before reassembling make sure that parts are free of any dust or particles.

4. Check piston to cylinder clearances, ring end gap, cylinder taper and out-of round.
5. Assemble the engine using the correct sealants where needed.

Rotary valve timing should be set with the closing edge as close to specs as possible or slightly higher.

NOTE: Refer to chart page.

6. The engine should be pressure-tested for air leaks. It should hold 6 PSI for 6 minutes with no more than a 1 PSI/min. loss.
7. Lube the rewind and inspect the rope for frays or cuts.
8. Oval racing must use taillight, brake light element on continuously (jumper from taillight wire terminal to brake light terminal on taillight assembly), regulator, tachometer, and temperature gauge.
9. Synchronize carburetors so that they open precisely together and ensure that the cut aways of the slides clear the inlet bores of the carburetors. After carb. adjustment, adjust oil injection pump.
10. On RAVE valve-equipped engines, check for free movement of the RAVE valve mechanism. Check the passageways between valve piston and exhaust port for any carbon buildup.

Adjust RAVE preload. It is better to have the valve open a little earlier than later.

NOTE: Pump fuels can be oxygenated or contain alcohol. Have your fuel tested prior to the race.

Do not use fuel de-icers.

11. Tie wrap ignition wire connectors together.
12. Adjust carburetors for atmospheric conditions. (See carburetion section.)
13. Break in a new engine before racing it. Performance can be gained by getting some run time on the engine. Ten hours of break-in is recommended.

TABLE OF CONTENTS

BASIC FUNCTIONS OF THE SYSTEM

The TRA Clutch

We call it a clutch but that set of pulleys is a lot more than simply a clutch. Once the system reaches its low ratio speed, the clutch function ends and the pulleys become a completely automatic transmission searching for the highest gear ratio that can be pulled at the engine's given output. In the case of our TRA clutch, the pulleys will begin shifting from a 3.8:1 ratio in low gear to a .8:1 overdrive ratio in high gear. That is a lot of ratio change. A typical six-speed motorcycle gearbox, for instance, will change from a 2.38:1 ratio in low gear to a .96:1 overdrive ratio in high gear.

The ratio changing is done by opening and closing a drive and driven pulley and forcing a fixed length drive belt to turn around different diameters on each pulley. The force used to **close** the engine or drive pulley is centrifugal force. It is the job of the ramps, rollers and lever arms to convert and control the centrifugal force.

Each engine will produce its minimum horsepower at a particular RPM. Power will decrease at engine speeds on either side of the peak power RPM. The usable width of the power band will dictate where the clutch must be calibrated to keep the engine performing at its peak. In the power curve the mildly-tuned engine has its peak horsepower of 64 at 5800 RPM and has a usable power band width of 1500 RPM. The race tuned engine produces its peak of 92 horsepower at 9300 RPM, but only has a usable power band width of 400 RPM. The race engine will have to have a much more accurately calibrated clutch to be able to keep the engine running within a 400 RPM range compared to the 1500 RPM wide range of the mildly-tuned engine.

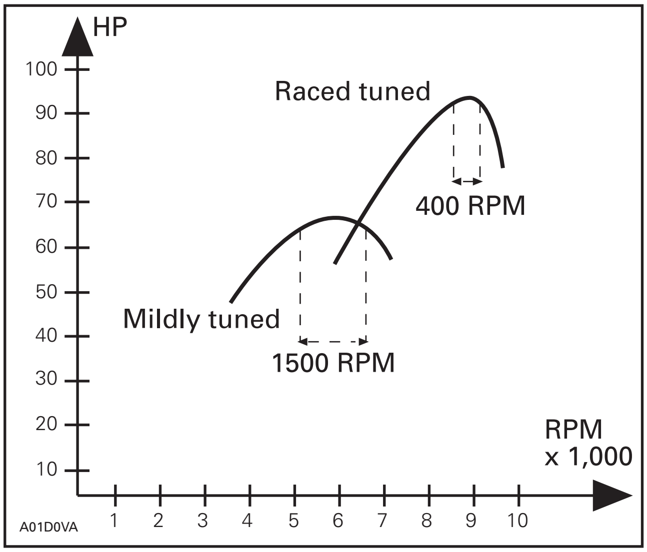
The goal of clutch calibration is to keep the engine, at full throttle at its peak horsepower RPM and, at the same time, to select the highest possible gear ratio as dictated by the load on the drive axle. The speed diagram illustrates what the goal of good clutch calibration is.

In the speed diagram, the inclined line labelled low ratio indicates the vehicle speed at each RPM when locked into the 3.8:1, low gear ratio. At 8000 RPM, the vehicle speed would be just under 20 MPH if held in this ratio. The high ratio line compares vehicle speed with engine RPM when the transmission is locked into the .8 :1 high gear. At this ratio, the vehicle speed would be just under 80 MPH when the engine is turning 8000 RPM. In calibrating the clutches, the objective will be to maintain as horizontal a line as possible between the low ratio and high ratio lines. This transition line or shift speed must be as close as possible to the engine peak horsepower RPM.

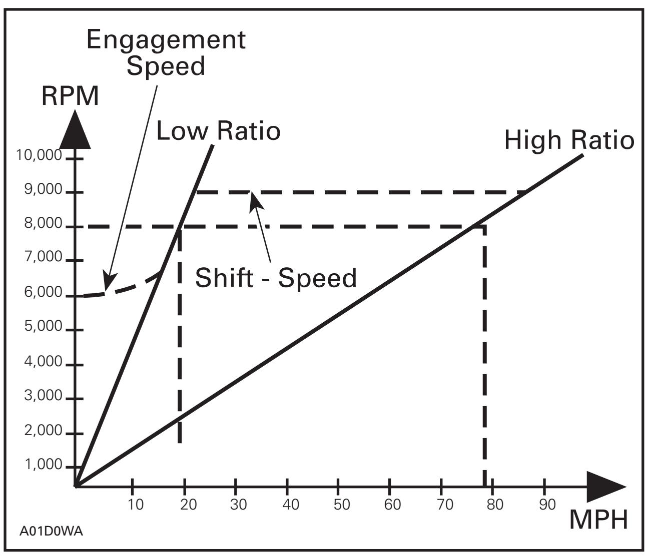
Engagement speed of the clutch is always set as **low** as possible to avoid track slippage and to prolong drive belt life. The clutch must be engaged at an RPM that is high enough, however, that the engine will be producing enough horsepower to overcome drag and allow acceleration without bogging. In the speed diagram, the acceleration period between 0 and about 20 MPH illustrates the actual clutching period of the transmission. During this time the rollers in the clutch are on the initial angles of the clutch ramps and the drive belt is actually slipping in the engine pulley as engine and vehicle speeds increase to about 9000 RPM at 25 MPH. The transmission then begins upshifting to the high ratio at a constant engine RPM. Engine speed should not increase above the calibration RPM until the high ratio is achieved. If the engine RPM exceeds the calibration RPM once the high gear position is achieved, it is an indication that the chaincase gearing is too low. If clutch calibration is accurate, engine speed should never vary more than 50 RPM from the peak power RPM. This is the optimum shift curve.

The following section will discuss each of the tunable components of both the drive and driven pulleys and provides some insight and data necessary for tuning the system.

POWER CURVES MILDLY TUNED VS. RACE TUNED



SPEED DIAGRAM ENGINE SPEED VS. VEHICLE SPEED



EFFECTS OF THE DRIVE PULLEY LEVER ARM, ROLLER AND ROLLER PIN WEIGHT

As you have seen in the formula defining centrifugal force, the force increases directly with the weight of the components involved. If you want to increase the centrifugal force, therefore, the shift force, it is a simple matter to increase the weight of the pressure levers. If the overall RPM is too high, a heavier lever arm or roller pin could be installed. The opposite would apply if the RPM is too low.

The major factor controlling centrifugal force is engine RPM. Because the force increases with the square of this speed, you can quickly have too much force if heavy weights are used on a clutch fitted to a high RPM engine. Because of this relationship, you will find heavy weights used on low RPM, high torque engine types and much lighter weights used on the high RPM engines.

The effect of the weights will always be greater at high RPM, and at higher ratios. This is true because of the relation of the force to the square of the engine speed. Also the radius from the axis of rotation to the center of mass of the counterweights increases as the roller is allowed to move down the ramps. As this radius increases, the centrifugal force increases directly. Addition of weight will affect engagement speed very little compared to the effect the weight will have at mid-range to top speed.

Minor changes in weight are accomplished by using various weight roller pins. The effects of adding weight are illustrated in the following illustration. The three curves show the engine RPM increasing from engagement speed (4000 RPM) to about 6500 RPM which is achieved at about 30 MPH. From this point on, if calibration is accurate, there is no change in engine RPM as the vehicle speed increases. From the machine standing at rest to about 30 MPH, belt slippage and other factors are involved that allow the engine to get on the power.

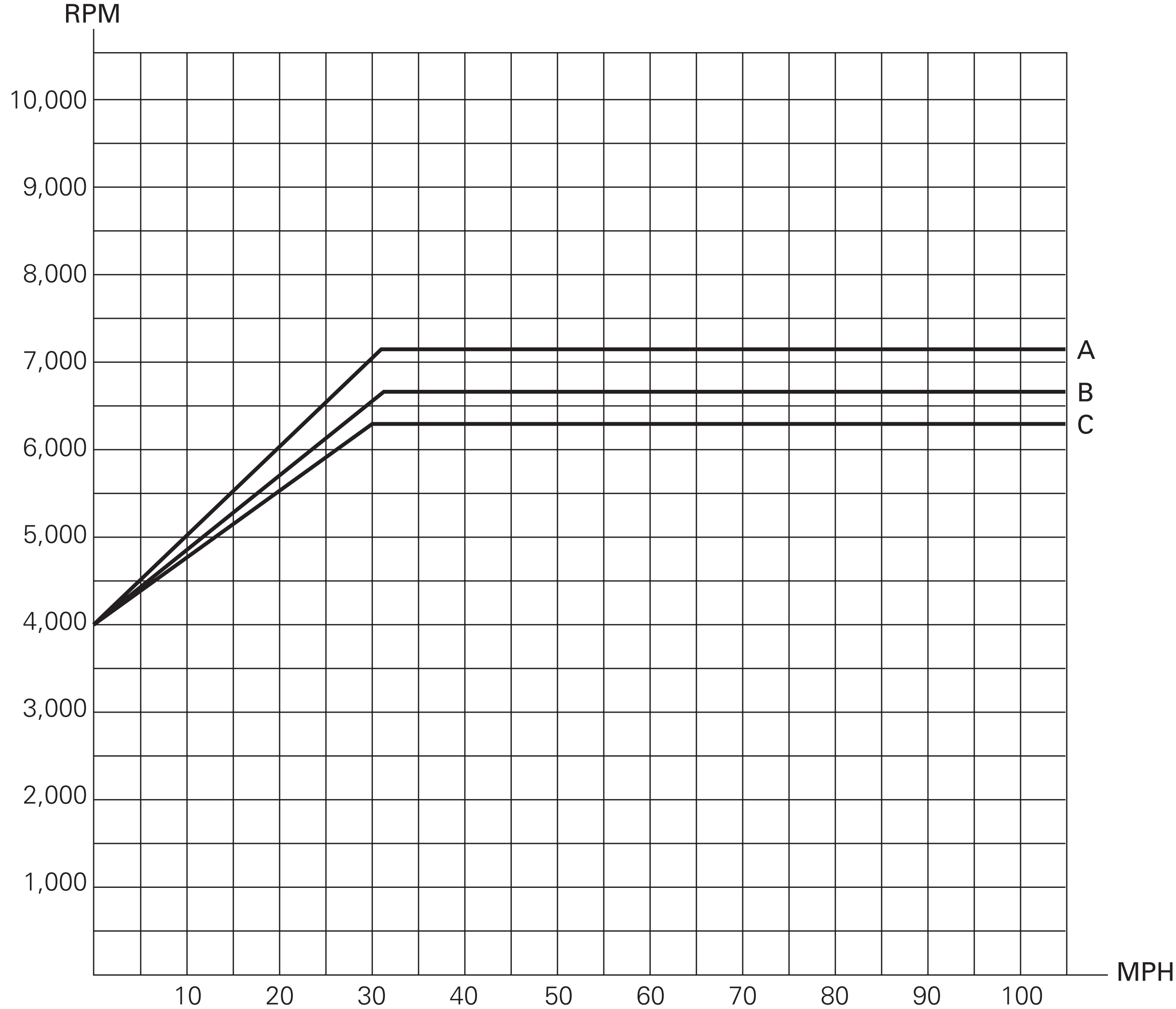
Curve **A** shows a clutch set up with three 10-gram type roller pins. This amount of weight will govern the engine to 7200 RPM and allow engagement of the clutch at 4000 RPM.

Curve **B** illustrates the effect of exchanging the three 10-gram pins for three 14-gram roller pins. The additional weight has virtually no effect on engagement speed but pulls the peak RPM of the engine down to 6800 RPM.

Curve **C** illustrates the effect of using three 16-gram roller pins. Again, the additional weight has little effect on the engagement RPM but further reduces the top RPM to 6400 RPM. For example, by adding 2 grams per arm for a total weight increase of 6 grams on an engine turning at around 7500 RPM, there would be about a 200 RPM decrease in full power engine speed — approximately the same effect as going 1 clicker position lower.

On a high RPM race engine it may only take a 1 gram, increase per arm to see a 200 RPM decrease in peak operating RPM.

Drive Clutch Roller Pins



A: 10 gram roller pins
B: 14 gram roller pins
C: 16 gram roller pins

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The solid steel roller pins can be drilled axially (lengthwise) with various size holes to vary the weight from 16.5 grams down to 10.3 grams (about a 1/4 inch diameter hole), which is the weight of the hollow steel pin. A 1/8 inch diameter hole drilled in the solid steel pin will give you about 14.5 grams. Also available are threaded steel and aluminum pins. These pins are used with set screws to allow for very small weight changes.

The weight of the lever arms will have a similar effect on the shift RPM. Early TRA clutches used an aluminum arm that weighed 37.9 grams. Starting in 1993, a heavier, reinforced aluminum arm was used on larger engine types. This heavier arm is now standard in all TRA clutches. It weighs 39.1 grams. Most of the reinforcing is concentrated at the pivot end of the arm, so the additional weight does not have a major effect on the shift curve, but changing from light aluminum arms to heavy aluminum arms will require small adjustments to the pin weight to obtain the same shift curve. A magnesium arm is also available (P/N 417 003 802) which weighs 27.3 grams.

The location of the center of gravity of the lever arm assembly will also affect the shift curve. Magnesium arms with solid steel pins will feel different than aluminum arms with threaded aluminum pins with 1 set screw. Both of these combinations have a total weight within 0.1 gram of each other, but the center of gravity of the magnesium arm set up is much farther away from the pivot pin than the aluminum arm set up. This magnesium arm set up will be revving higher at low ratios and part throttle openings.

By adding or removing weight to or from the arms, we can fine tune the shift RPM to the engine power peak.

If you increase the horsepower of the engine at the same RPM, you would normally add more weight to keep the engine pulling as hard as possible and not over rev.

If you lighten the weights on the arms, you will be increasing the shifting RPM. However, your vehicle will not **pull** as hard, since less centrifugal force is being generated.

This should be optimized by accurate testing under duplicatable conditions until the best weight is found for your use.

On the newer TRA clutches, the 6 mm allen bolt that the roller arms pivot on is easily removable. However, a steel, gold color tube is left in the clutch holding the arm in place. This tube can be very difficult to remove. A simple solution to this is to remove the 6 mm Allen bolt and coat it with red, Loctite 271 and reinstall the bolt, let it cure, and when fully cured, you can remove the Allen bolt along with the sleeve since the two are now **locked** together.

Heavy aluminum arm	39.1	417 003 801
Magnesium lever arm	27.3	417 011 012
Solid steel roller pin	16.4 (black)	504 259 600
Hollow steel roller pin	10.3	417 004 309
Threaded steel roller pin	10.3	504 151 700
Threaded aluminum pin	3.8	504 260 3 00
Allen set screw 1/4″ – 28 N.F. × 1/4″	0.9	365 202 000
Steel roller	9.8	417 003 900
Steel roller	8.5	417 222 042
Aluminum roller	4.1	860 411 800 (kit)

NOTE: The clutch pins in the 2002 MX Zx 440 are metric threads. Previous years standard 1/4″ 28 NF set screws will not fit. A tuning kit be made available.

EFFECTS OF THE RAMP PROFILE ON THE SHIFT FORCE

The shift force is the component or part of the centrifugal force that is used to actually move the sliding half of the drive pulley. This force is applied to the sliding half at the three lever arm pivot points (following illustration item 49). The ramp profiles are used to control the size of this shift force.

As the clutch rotates around the center line of the crankshaft, the axis of rotation, centrifugal forces begin building and act on the center of mass of the lever arm, roller combination trying to pull the lever away from the axis of rotation. The center of mass of the lever arm assembly is the point where all the centrifugal force acts (following illustration item 70).

The ramp provides an angled surface for the roller to push against and the angle of the ramp at the point of contact with the roller determines how much of the centrifugal force is translated into axial force. The axial force pushes the sliding half in and the remainder of the centrifugal force is unused and absorbed by the integrity of the sliding half. A steeper ramp angle gives less shift force, while a smaller angle gives more shift force.

As you can see in following illustration, the angle of the ramp varies constantly from start to finish. The angle varies to achieve the proper axial force to transmit a given amount of torque through the drive belt at each diameter of the pulley.

As discussed before, the centrifugal force generated by the lever arm assembly increases at higher ratios. This is why the ramp profile is much steeper at the high ratio end. This reduces the shift force in order to maintain the correct load on the belt.

Remember, it is the angle of the ramp at the point of roller contact that will help determine the shift force at any given ratio. Think of the ramp profile as a hill that the roller must climb. A small angle or hill can be overcome easily thus providing a faster shift out to a higher ratio which will lower the engine RPM. If the hill is steeper (the ramp angle is larger) the roller will not be able to climb it as quickly thus staying in a lower ratio longer which will keep the engine RPM higher.

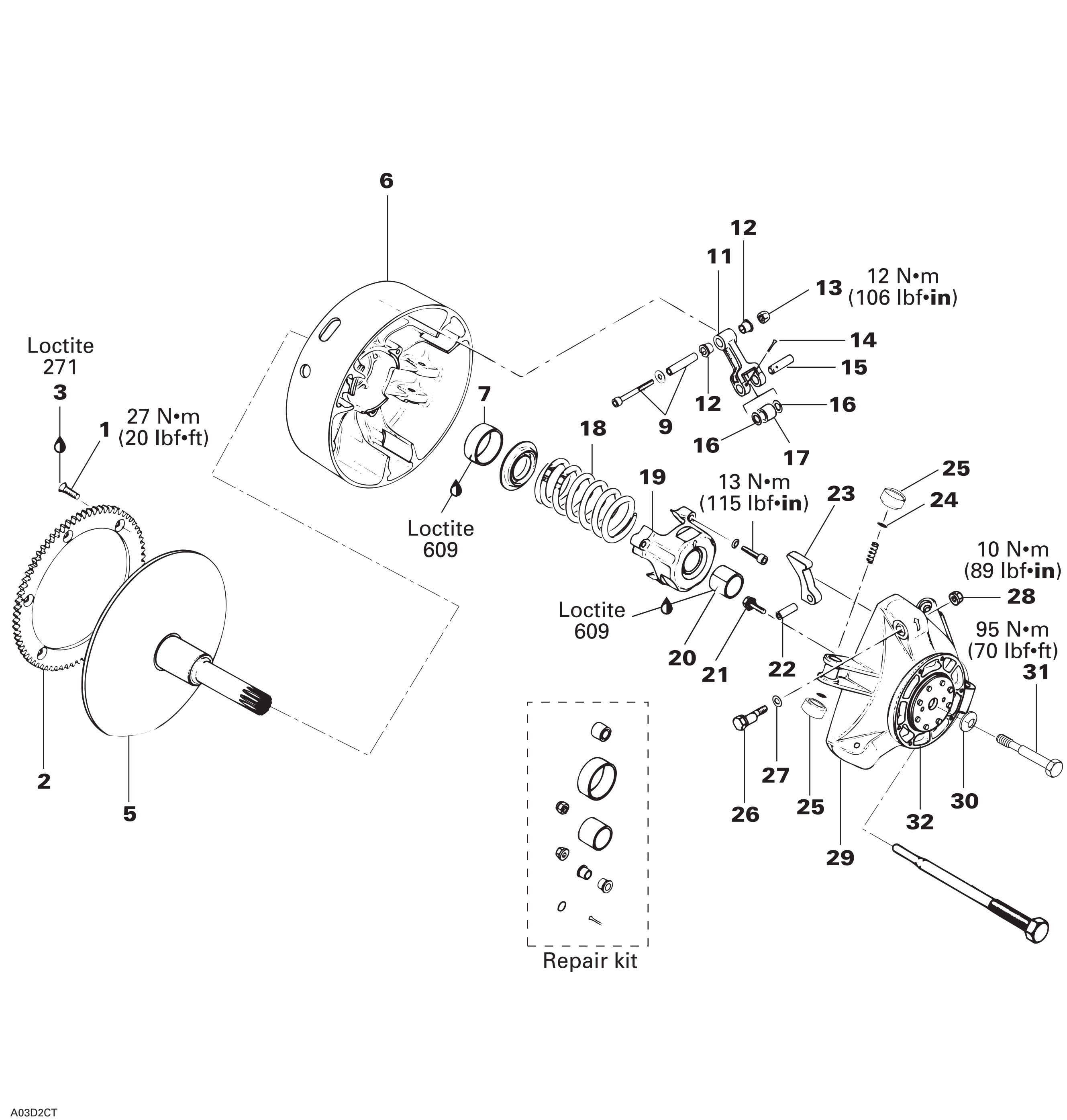
Note that at engagement and very low ratios, many ramp angles actually go downhill. These are generally used on engines with good low RPM power. Engines with narrower power bands and less low RPM power will usually have a flatter angle at engagement and low speed. A ramp with a small bump at engagement is used to raise the engagement RPM. Again, the steeper the "hill" the roller must overcome, the higher the RPM will be before the clutch shifts out. If the spring selection cannot give the desired engagement RPM, then use a ramp with a bump or grind a notch at the point where the roller sits at engagement. Of course if the shift profile was good at higher ratios, then you would want to use a ramp with only changes at the low speed area.

Also, a thicker or taller ramp will provide higher RPM than a thinner ramp with the same profile because the lever arm assembly is tucked in further by the taller ramp.

The TRA clutch allows you to fine tune the ramp profile by using the adjusters provided. The adjusters are cams which allow you to raise and lower the outer end of the ramp through six different positions. Moving the ramp end toward the lever arm makes the ramp angles steeper, thereby raising engine speed and slowing the upshift. As the ramp is adjusted away from the lever arm, the engine speed is lowered and the upshift is faster.

In clinical condition such as on a dynamometer, moving the adjusters up will result in a 150 to 200 RPM increase with each position change. Lowering the adjuster positions will result in a decrease of 150 to 200 RPM with each number. On the snowmobile, however, depending on the operating conditions, a change of one adjuster position may not show up on the tachometer, but the shift speed of the pulley will have changed. The upshift or downshift, depending on which way you moved the adjusters, will be faster and your acceleration rate and top speed will have changed. When using the TRA adjusters, the acceleration rate and speed should be checked as well as the engine RPM.

On the DSA chassis and with the new driven pulley bushing material, the friction in the driven pulley and chassis is reduced, thus a one position change on the TRA adjuster will usually result in a RPM change.



For drag racing and radar running, it is usually better to try to go as low as possible on the adjusters without dropping the engine peak RPM too much as this will give the vehicle its fastest acceleration and top speed.

For oval racing or tight snowcross type courses, you may find you need to be one or two numbers higher on your TRA adjuster to give the best throttle response possible out of the corners.

This will be where the winners spend their time testing different combinations of lever arm weights, TRA adjustments, and ramp profiles until they find the best possible setup.

DRIVE PULLEY

⚠ WARNING

For safety reasons, this kit must be installed by an authorized Ski-Doo® snowmobile dealer. Should removal of a locking device (e.g. lock tabs, self-locking fasteners, etc.) be required when undergoing disassembly/assembly, always replace with a new one. Torque wrench tightening specifications must strictly be adhered to; refer to table at the end of this document. This instruction sheet should be given to the purchaser.

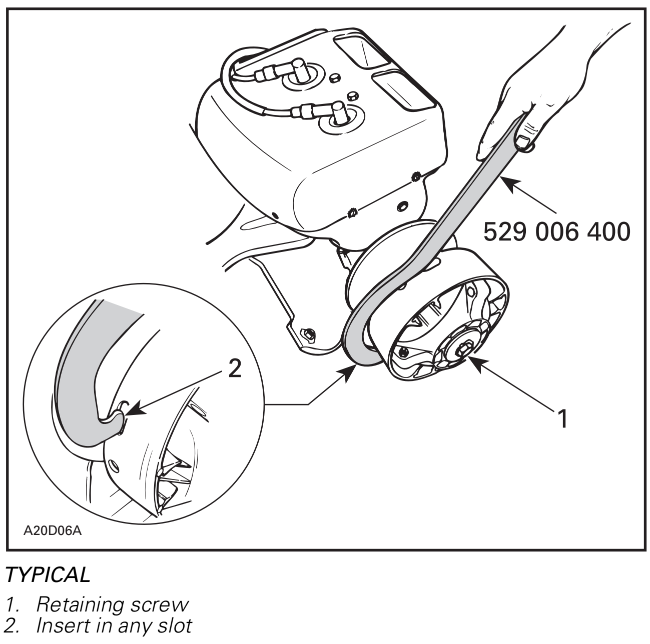
This kit is designed for specific applicable models only (your authorized Ski-Doo snowmobile dealer will confirm models). It is not recommended for units other than those for which it was sold.

This instruction sheet applies to the MX Zx 440 LC only.

INSTRUCTION

Remove belt guard and drive belt.

Use holder (P/N 529 006 400).



TYPICAL
1. *Retaining screw*
2. *Insert in any slot*

⚠ WARNING

Never use any type of impact wrench at drive pulley removal and installation.

Remove retaining screw.

To remove drive pulley ass'y and/or fixed half from engine, use puller (P/N 529 022 400).

CAUTION: These pulleys have metric threads. Do not use imperial threads puller. Always tighten puller by hand to ensure that the drive pulley has the same type of threads (metric vs imperial) prior to fully tightening.

To Remove Drive Pulley Ass'y:

Retain drive pulley with clutch holder.

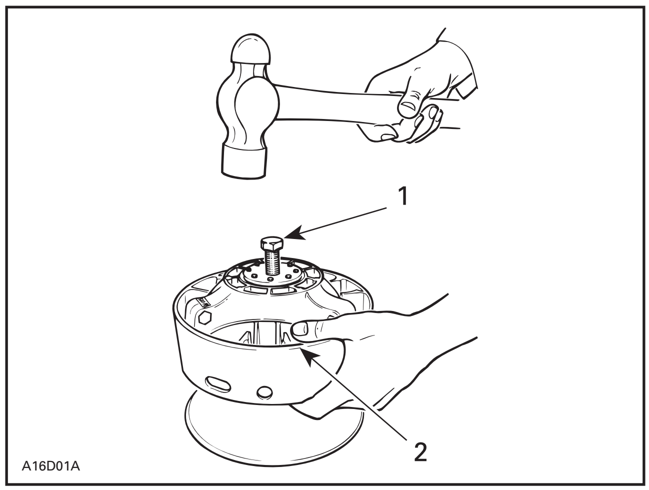
Install puller in pulley shaft then tighten.

DISASSEMBLY

Fixed and Sliding Half

CAUTION: Do not tap on governor cup.

Screw puller into fixed half shaft about 13 mm (1/2 in). Raise drive pulley and hold it by the sliding half while knocking on puller head to disengage fixed half.



1. *Puller*
2. *Holding sliding half*

NOTE: No components marking is required before disassembling this drive pulley since it has factory mark and arrows as indexing reference.

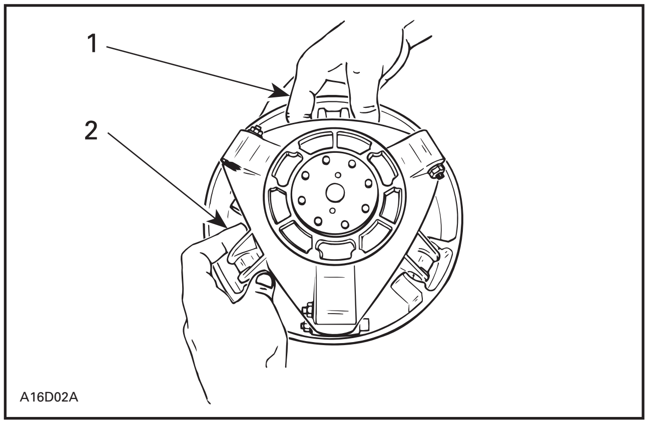
Cushion Drive

CAUTION: Do not disassemble cushion drive. Governor cup and cushion drive are factory balanced as an assembly.

Slider Shoe and Governor Cup

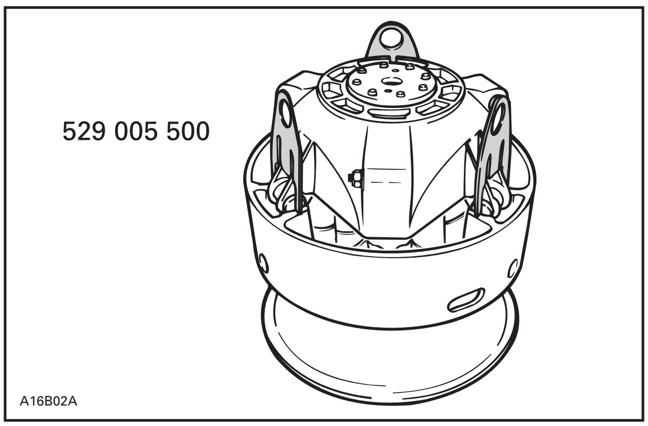
Carefully lift governor cup until slider shoes come at their highest position into guides.

Hold a slider shoe set then carefully lift its housing and remove slider shoes. Proceed the same way for other housings lifting one at a time.



1. *Hold slider shoes*
2. *Lift one housing at a time*

NOTE: To ease disassembly, forks (P/N 529 005 500) should be used to hold slider shoes prior to removing governor cup.



Spring Cover Ass'y

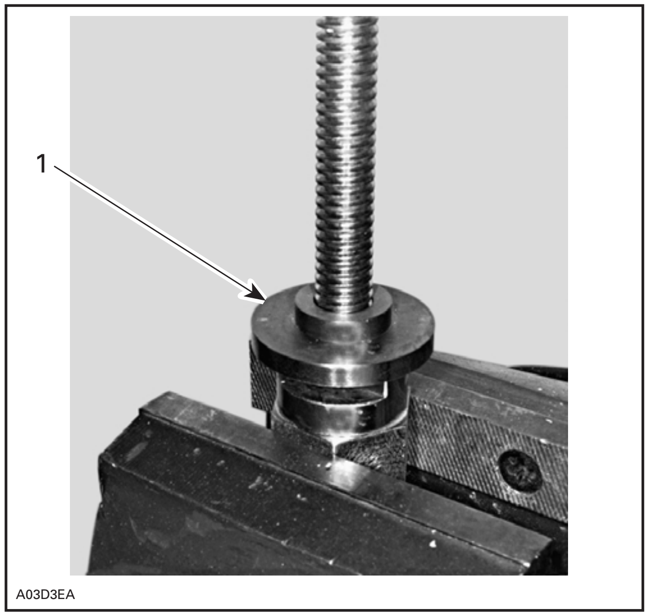
It is pushed by clutch spring pressure.

⚠ WARNING

Clutch spring is very strong. Never attempt to remove spring cover without the recommended tools.

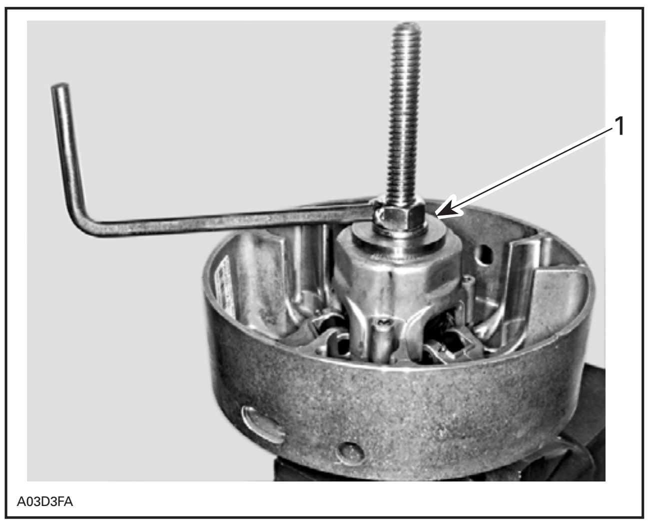
Use spring compressor (P/N 529 035 524).

Install support guide.



1. *Support guide*

Install sliding half then a second support guide. These support guides will prevent bushing damages.



1. *Support guide*

Remove 3 Allen screws retaining spring cover then unscrew compressor.

CLEANING (IF REQUIRED)

Fixed and Sliding Half

Clean pulley faces and shaft with fine steel wool and dry cloth.

Fixed Half and Crankshaft End

Parts must be at room temperature before cleaning.

Using a paper towel with cleaning solvent, clean crankshaft tapered end and the taper inside the fixed half of the drive pulley, crankshaft threads and retaining screw threads.

⚠ WARNING

This procedure must be performed in a well-ventilated area.

CAUTION: Avoid contact between cleaner and crankshaft seal because damage may occur.

Remove all hardened oil deposits that have baked on crankshaft and pulley tapered surfaces with coarse or medium steel wool and/or sand paper no. 600.

CAUTION: Do not use any other type of abrasive.

Reclean mounting surfaces with paper towel and cleaning solvent.

Wipe off the mounting surfaces with a clean, dry paper towel.

CAUTION: Mounting surfaces must be free of any oil, cleaner or towel residue.

Bushing

Only use petrol base cleaner when cleaning bushings.

CAUTION: Do not use acetone to clean bushing.

INSPECTION

Drive pulley should be inspected annually.

Thrust Washer and Roller

Check roller for roundness of external diameter. Check thrust washer for thickness wear. Replace as required.

CAUTION: Ensure rollers are in good condition. Replace as required.

Fitting Bolt Ass'y and Flanged Bushing

Check for wear, replace as required.

O-Ring and Slider Shoe

Check if O-rings are cracked, cut or crushed. Replace as required.

Check slider shoes for wear. Replace if groove is not apparent on top.

Fixed Half and Governor Cup

Inspect splines and free play between both parts. Maximum free play is 0.5 mm (.020 in) measured at calibration screw radius. Replace if required.

Sliding Half and Spring Cover Bushing

Visually inspect coating. Replace if worn.

Sliding Half Bushing Replacement

This bushing is not replacable. If worn out, replace sliding half ass'y.

Spring Cover Bushing Replacement

Under normal use there is no need to replace this bushing.

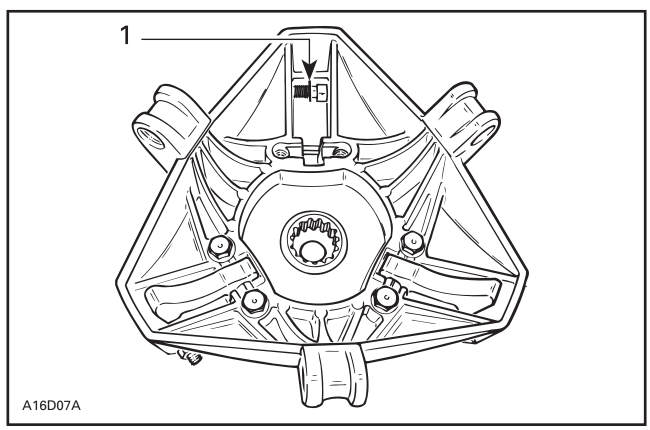
This bushing is not replacable. If worn out, replace spring cover ass'y.

ASSEMBLY

NOTE: This drive pulley is lubrication free. **Do not lubricate** any component.

Calibration Screw, Washer and Locking Nut

When installing calibration screw, make sure to install washer as shown.



1. Washer

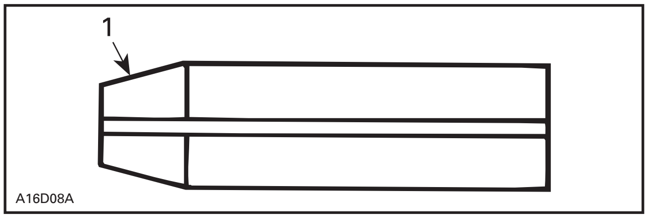
Torque locking nut to 10 N•m (89 lbf•**in**).

Pin

Always use the same type of pin as originally installed when servicing. Different types have different weights for calibration purpose. Refer to TECHNICAL DATA where *Shop Manual* is available.

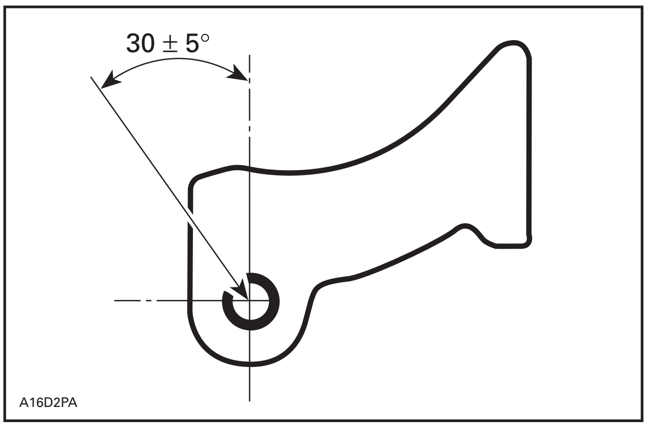
Ramp, Dowel Tube and Screw

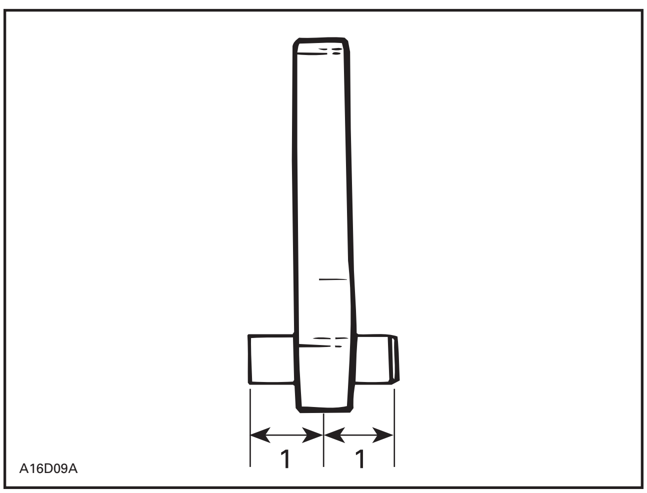
Insert dowel tube from chamfered side. Make sure ramp is centered on dowel tube.



1. *Chamfered side*

Position dowel tube split at the illustrated angle.





1. *Equal distance*

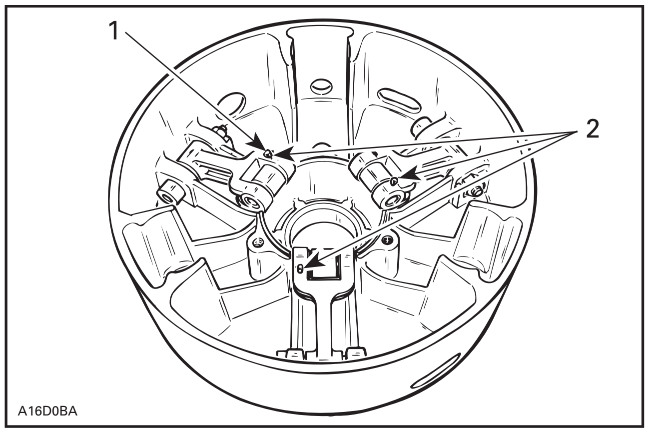
Torque screws to 10 N•m (89 lbf•**in**).

Screw, Lever Ass'y, Nut and Cotter Pin

Always install lever assemblies so that cotter pins are on the shown side. Besides install cotter pin head on top when lever is sat at bottom of sliding half. Bend cotter pin ends to sit perfectly against lever.

⚠ WARNING

Whenever replacing centrifugal levers, always replace all 3 at the same time. Otherwise, drive pulley misbalancing will occur because of levers difference.



1. *Head on top*
2. *All on the same side*

CAUTION: Lever assemblies must be installed so that cotter pins are on the same side.

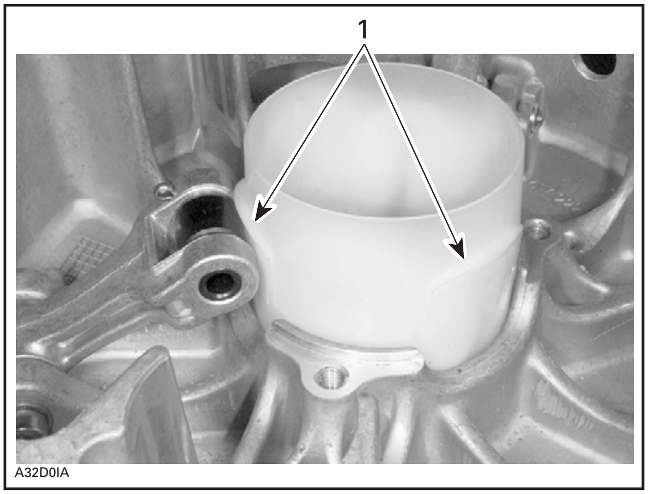
Torque nuts to 12 N•m (106 lbf•**in**).

CAUTION: Lever ass'y and rollers must move easily after installation.

Guard

Some Models Only

Install guard with its reinforcements in line with levers.



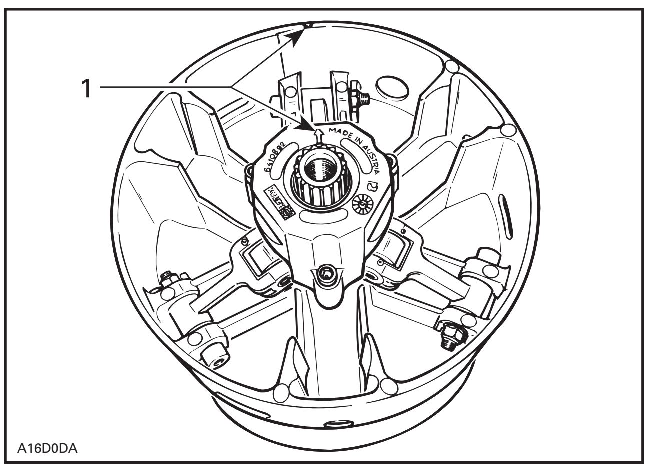
1. Reinforcements

Fixed Half, Sliding Half, Spring, Spring Cover and Screw

Install titanium spring.

To install spring cover, use spring compressor (P/N 529 035 524). Align indexing arrows.

Assemble fixed and sliding halves.

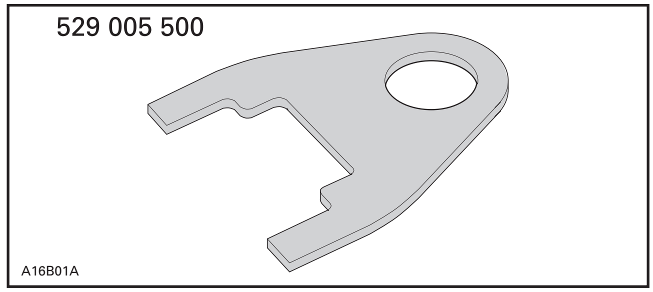


1. Align

Install and torque screws to 13 N•m (115 lbf•**in**) for 593 engine equipped models and to 16 N•m (142 lbf•**in**) for 693 and 793 engine equipped models.

Sliding Half, Slider Shoe and Governor Cup

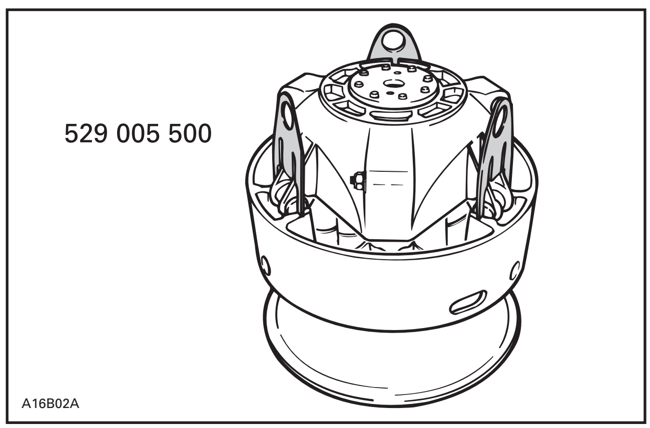
To install governor cup, use following tool:



Insert spring and slider shoes into governor cup so that groove in each slider shoe is vertical to properly slide in guides.

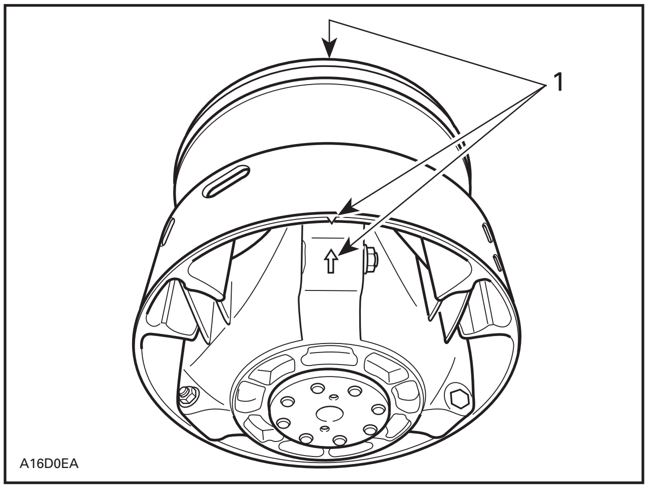
CAUTION: Make sure O-rings are installed on slider shoes and their grooves are positioned vertically.

Install fork (P/N 529 005 500) into slider shoe grooves to maintain them for governor cup installation. Proceed on 3 set of slider shoes.



Make sure to align governor cup arrow with sliding half and fixed half mark.

NOTE: If fixed half has no mark, align governor cup mark with segment no. 1 of inner half. Segments are identified on engine side.



1. Align

Carefully slide governor cup into sliding half. Align mark of governor cup with mark of fixed half.

Remove forks and push governor cup so that its splines engage with fixed half shaft splines.

CAUTION: Make sure splines of both parts are fully engaged.

INSTALLATION

> **⚠ WARNING**
>
> **Do not apply anti-seize or any lubricant on crankshaft and drive pulley tapers.**

> **⚠ WARNING**
>
> **Never use any type of impact wrench at drive pulley removal and installation.**

Clean mounting surfaces as described in CLEANING above.

Drive Pulley Ass'y

The installation procedure must be strictly adhered to as follows.

Install drive pulley on crankshaft extension.

Install conical washer with its concave side towards drive pulley then install screw.

> **⚠ WARNING**
>
> **Never substitute conical washer and/or screw with jobber ones. Always use Bombardier genuine parts for this particular case.**

Use holder. See removal procedure.

Torque screw to 80 to 100 N•m (59 to 74 lbf•ft).

Install drive belt and guard.

Titanium spring installation is now done but proper procedure also requires the following.

Raise and block the rear of the vehicle and support it with a mechanical stand.

> **⚠ WARNING**
>
> **Ensure that the track is free of particles which could be thrown out while track is rotating. Keep hands, tools, feet and clothing clear of track. Ensure nobody is standing near the vehicle.**

Accelerate the vehicle at low speed (maximum 30 km/h (20 MPH) and apply the brake, repeat 5 times.

Recheck the torque of 90 to 100 N•m (66 to 74 lbf•ft).

> **⚠ WARNING**
>
> **After 10 hours of operation the transmission system of the vehicle must be inspected to ensure the retaining screw is properly torqued.**

DRIVE PULLEY ADJUSTMENT

The drive pulley is factory calibrated to transmit maximum engine power at a predefined RPM. Factors such as ambient temperature, altitude or surface condition may vary this critical engine RPM thus affecting snowmobile efficiency.

This adjustable drive pulley allows setting maximum engine RPM in the vehicle to maintain maximum power.

Calibration screws should be adjusted so that actual maximum engine RPM in vehicle matches with the maximum horsepower RPM given in TECHNICAL DATA.

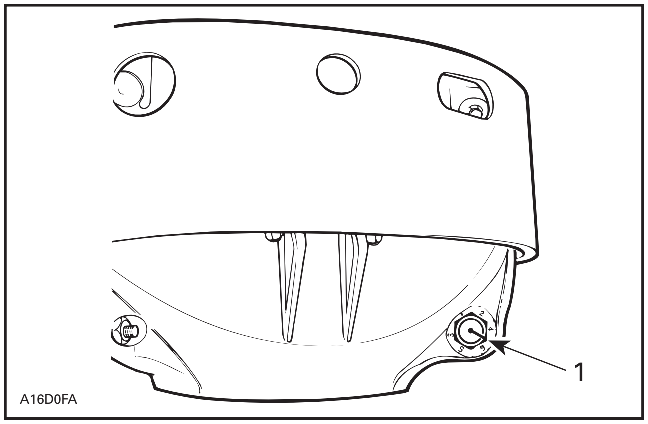
NOTE: Use precision digital tachometer for engine RPM adjustment.

NOTE: The adjustment has an effect on high RPM only.

To adjust, modify ramp end position by turning calibration screws.

Calibration Screw, Locking Nut and Governor Cup

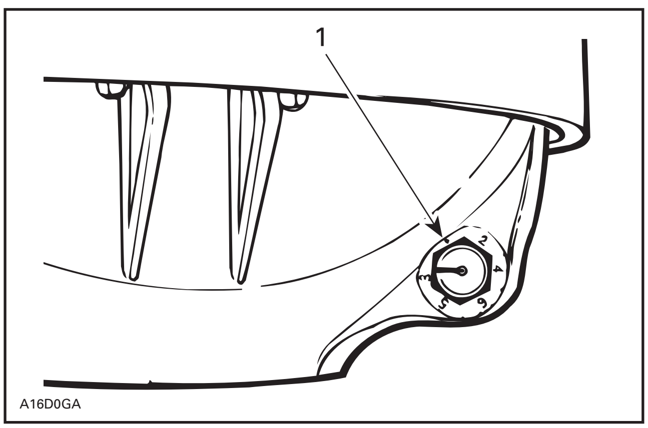
Calibration screw has a notch on top of its head.



1. *Notch*

Governor cup has 6 positions numbered 2 to 6. Note that in position 1 there is no stamped number (due to its location on casting).

See TECHNICAL DATA for original setting where a *Shop Manual* is available.



1. *Position 1 (not numbered)*

Each number modifies maximum engine RPM by about 200 RPM.

Lower numbers decrease engine RPM in steps of 200 RPM and higher numbers increase it in steps of 200 RPM.

Example:

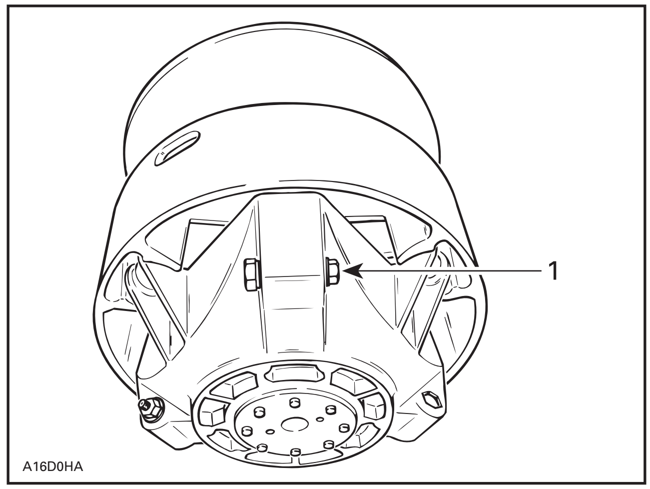
Calibration screw is set at position 3 and is changed to position 5. So maximum engine RPM is increased by about 400 RPM.

To Adjust:

Just loosen locking nut enough to pull calibration screw **partially** out and adjust to desired position. Do not completely remove the locking nut. Torque locking nuts to 10 N•m (89 lbf•**in**).

CAUTION: Do not completely remove calibration screw otherwise its inside washer will fall off.

CAUTION: Always adjust all 3 calibration screws and make sure they are all set at the same number.



1. *Loosen just enough to permit rotating of calibration screw*

PULLEY DISTANCE AND ALIGNMENT

GENERAL

The pulley distance we will refer to in this section, is the space separating the drive and driven pulley outside diameters (Z measurement).

This basic distance is provided as an assembly guide and indicates the dimensions between which satisfactory belt deflection will be obtained.

Both pulley distance adjustment and pulley alignment must be carried out to ensure the highest efficiency of the transmission system. Furthermore, optimum drive belt operation and minimal wear will be obtained only with proper pulley alignment.

CAUTION: Before checking pulley adjustment, the rear suspension must be mounted on the vehicle and track tension/alignment must be done. Always check pulley adjustment after suspension is adjusted.

⚠ WARNING

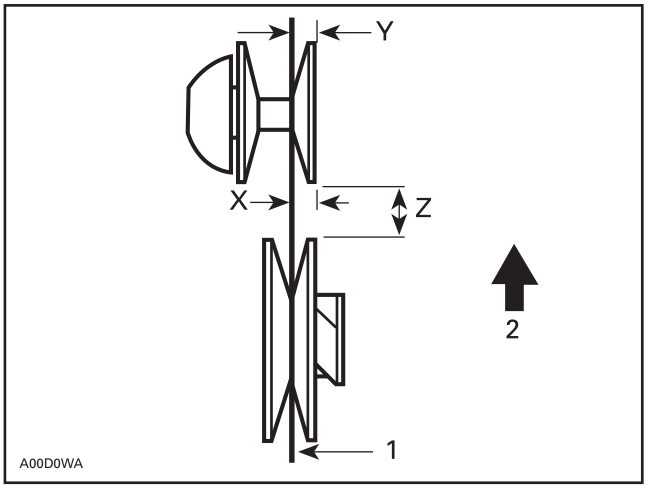
Failure to correctly perform pulley alignment may cause the vehicle to creep forward at idle.

All Pulley Alignment Specifications Refer to:

X = Distance between straight bar and drive pulley fixed half edge, **measured between pulleys**.

Y = Distance between straight bar and drive pulley fixed half edge, **measured at the end of straight bar**.

Z = Distance between outside diameter of pulleys.



TYPICAL
1. Straight bar
2. Front of vehicle

The distance Y **must** exceed distance X to compensate for the twist due to the engine torque.

GENERAL PROCEDURE

Remove guard and drive belt.

By turning and pushing the sliding half, open the driven pulley. Insert a straight bar 9.5 mm (.375 in) square, 48 cm (19 in) long or the proper alignment template into the opened driven pulley.

Measuring Procedure

Using Straight Bar

Always measure distances X and Y from the farther straight bar side (including its thickness to the fixed half edge).

Drive Belt Deflection

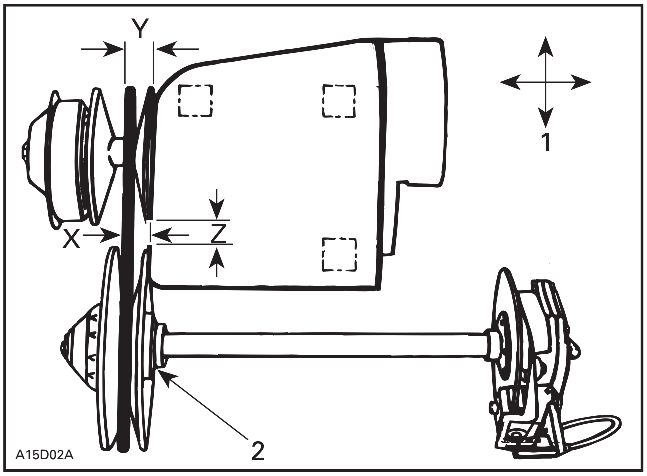
NOTE: When pulley distance and alignment are adjusted to specifications, refer to DRIVE BELT (where a *Shop Manual* is available) to adjust drive belt deflection.

CAUTION: This section deals mainly with adjustment procedures. For complete assembly requirements, refer to the proper ENGINE or TRANSMISSION installation section.

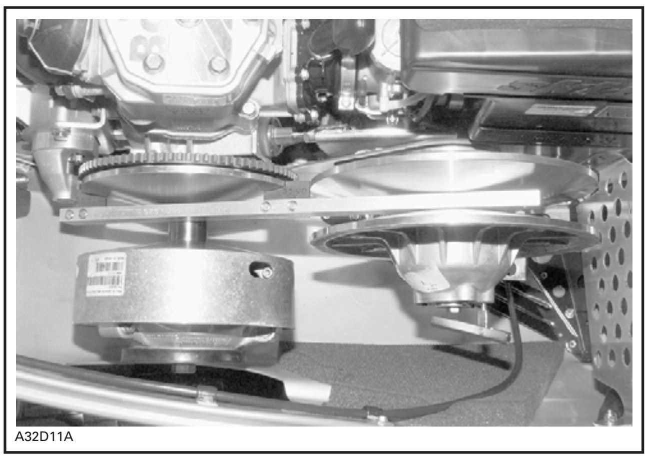
PULLEY ALIGNMENT AND DISTANCE SPECIFICATIONS CHART

MODEL	PULLEY DISTANCE	OFFSET		ALIGNMENT TEMPLATE ① P/N
	Z	X	Y-X	
	± 0.50 mm (.020 in)	± 0.50 mm (.020 in)	± 0.50 mm (.020 in)	
All	16.5 (.650)	35.50 (1.398)	1.5 (.060)	529 026 700

① Alignment templates have been made according to pulley alignment nominal values. However, they do not take into account allowed tolerances for alignment specifications. They are used as GO/NO GO gauges for quick alignment and pulley distance check and as templates to reach alignment nominal values.

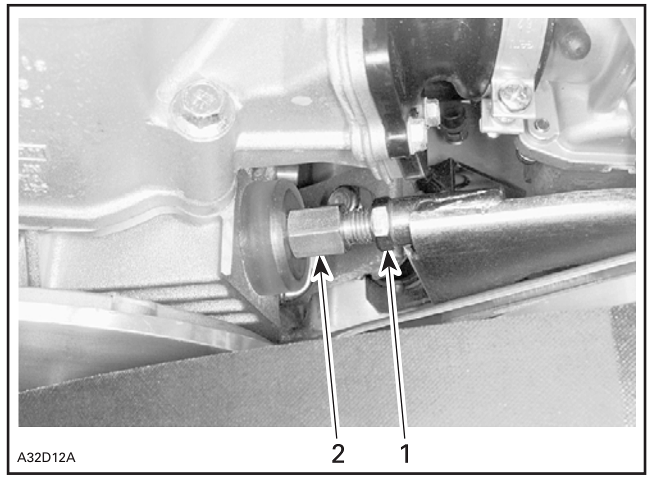


TYPICAL
1. *Engine movement*
2. *Contact*



ALIGNMENT BAR IN PULLEYS

NOTE: Prior to performing pulley adjustment, loosen torque rod nut to allow engine movement. Engine supports have tendency to stick to frame, work engine loose prior to aligning.



1. *Loosen lock nut first*
2. *Loosen*

Pulley Distance Adjustment Method

Engine Movement

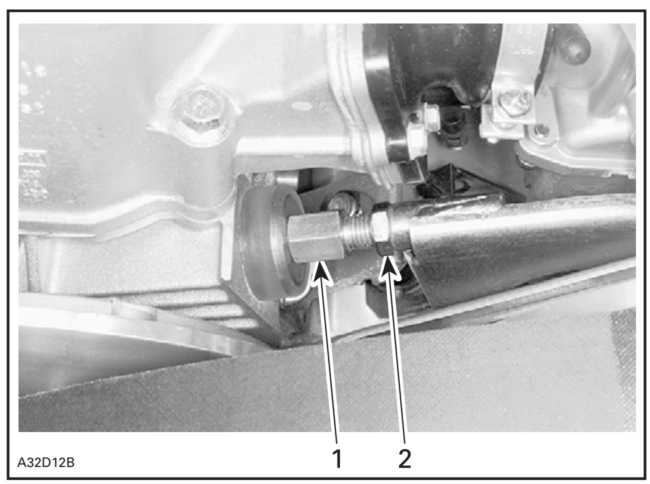
The engine support has slotted mounting holes. Move engine to obtain specified distance between pulleys.

Pulley Alignment Method

Engine Movement

Loosen the 4 bolts retaining engine support to the frame. Position engine to obtain the specified alignment.

NOTE: After alignment, adjust torque rod so it slightly contacts stopper plate. Do not over tighten, it will disalign pulleys.



1. *Slightly tighten*
2. *Retighten*

Reinstall drive belt and belt guard.

The following table is to be consulted if and when a tightening torque is required but not specified.

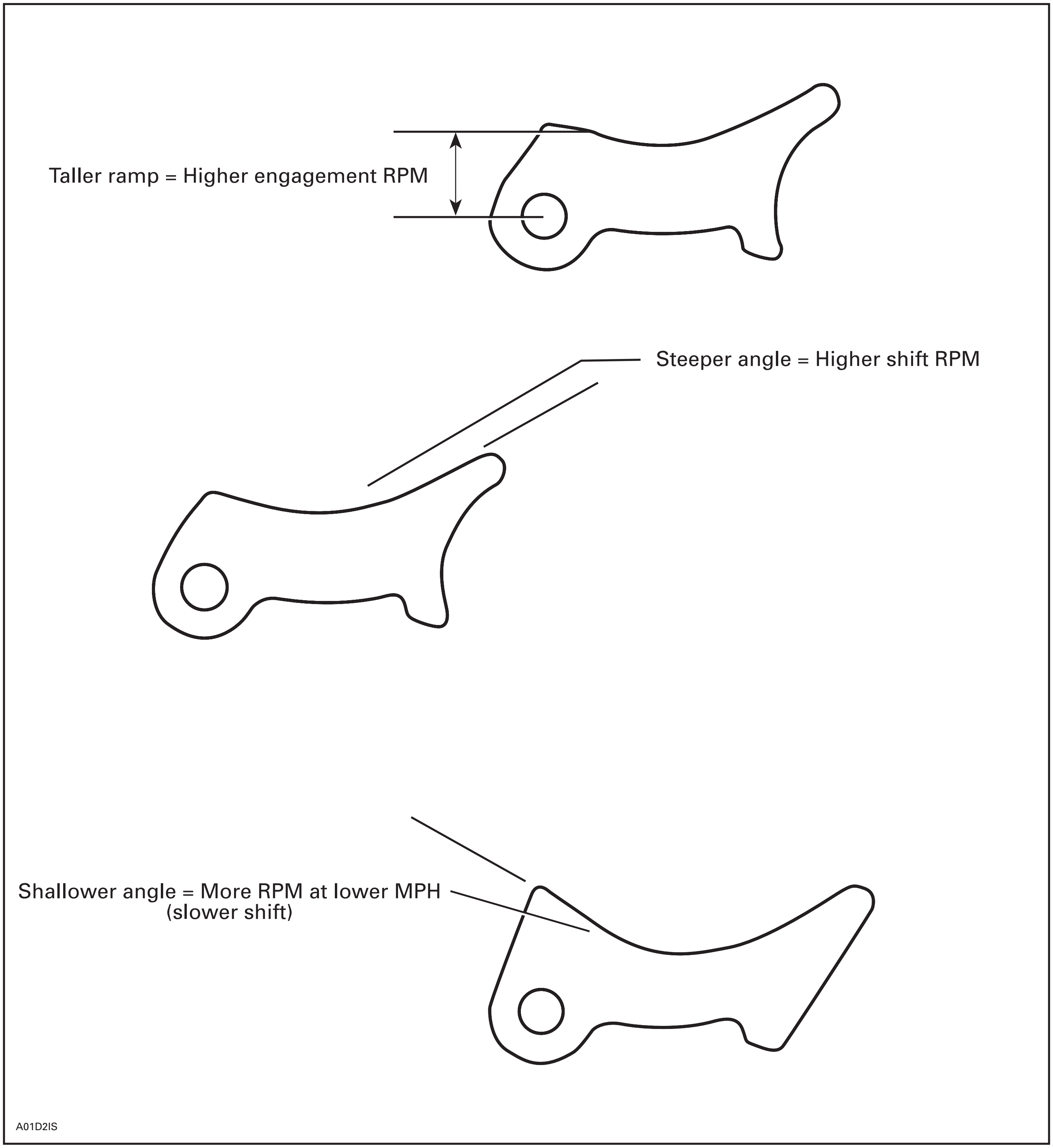
Bold face size indicates nominal value (mean value).

N•m	FASTENER SIZE (8.8 GRADE)	Lbf•**in**
2	**M4**	18
3	M4	27
4	**M5**	35
8	M6	71
9	M6	80
10	**M6**	89
11	**M6**	97
12	**M6**	106

N•m	FASTENER SIZE (8.8 GRADE)	Lbf•ft
21	M8	15
22	M8	16
23	**M8**	17
24	M8	18
25	M8	18
43	M10	32
44	M10	32
45	M10	33
46	M10	34
47	M10	35
48	**M10**	35
49	M10	36
50	M10	37
51	M10	38
52	M10	38
53	M10	39
76	M12	56
77	M12	57
78	M12	58
79	M12	58
80	**M12**	59
81	M12	60
82	M12	60
83	M12	61
84	M12	62
121	M14	89
122	M14	90
123	M14	91
124	M14	91
125	M14	92
126	M14	93

N•m	FASTENER SIZE (8.8 GRADE)	Lbf•ft
127	M14	94
128	M14	94
129	M14	95
130	M14	96
131	M14	97
132	M14	97
133	M14	98
134	M14	99
135	**M14**	100
136	M14	100
137	M14	101
138	M14	102
139	M14	103
140	M14	103
141	M14	104
142	M14	105
143	M14	105
144	M14	106
145	M14	107
146	M14	108
147	M14	108
148	M14	109
149	M14	110
150	M14	111

RAMP CHARACTERISTICS



TRA RAMP PROFILES

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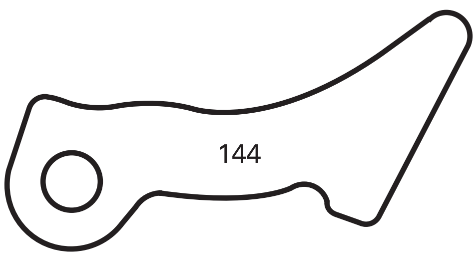

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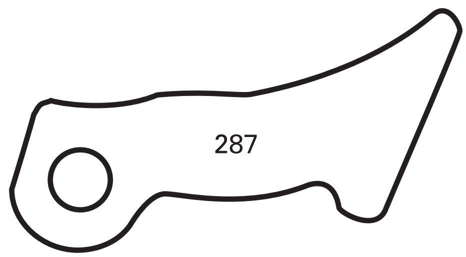

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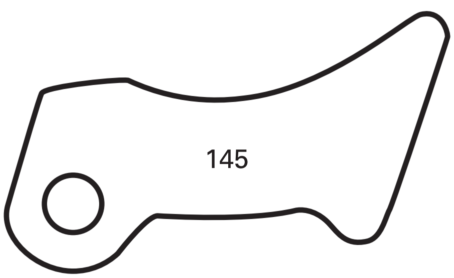

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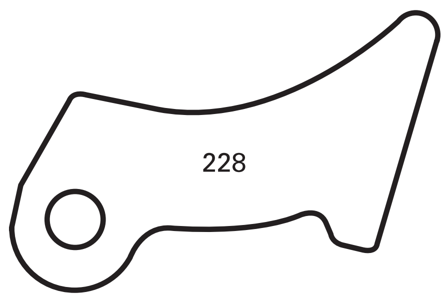

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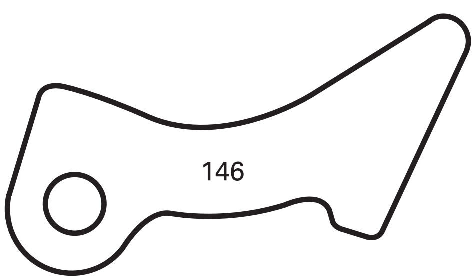

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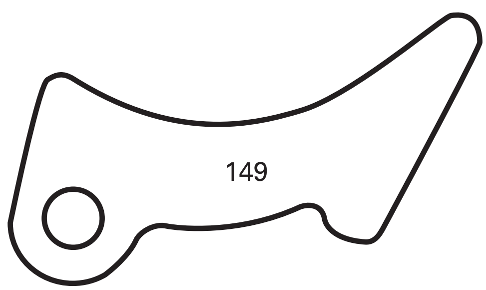

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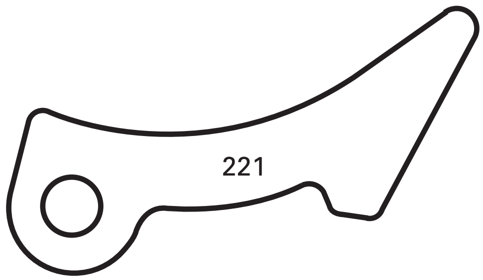
417 005 221



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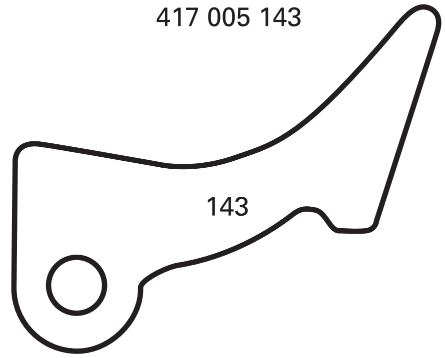

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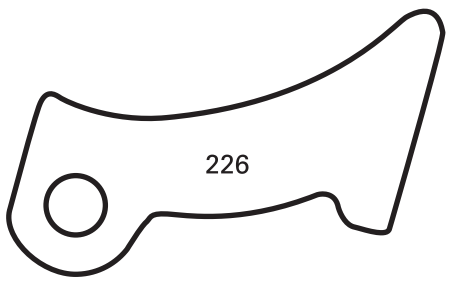

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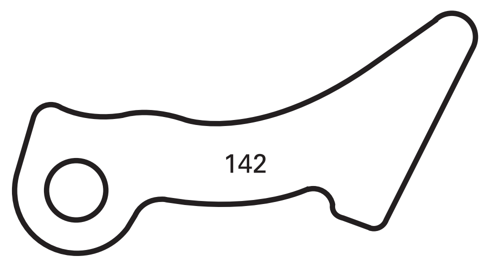

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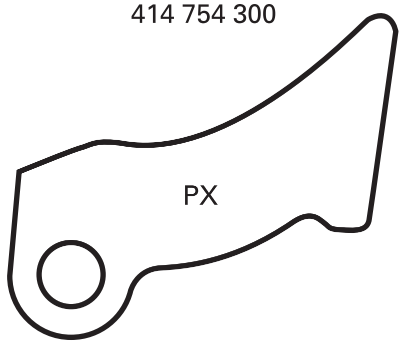

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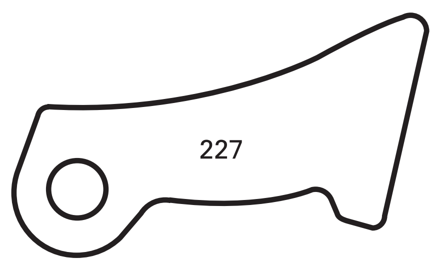

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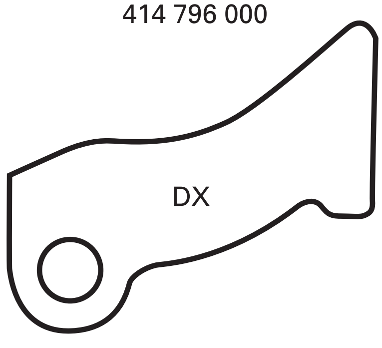

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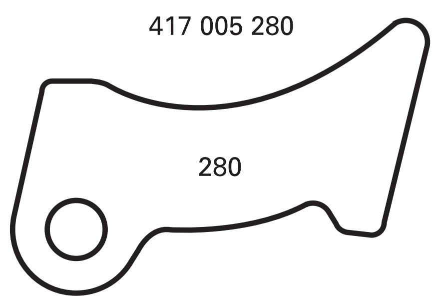

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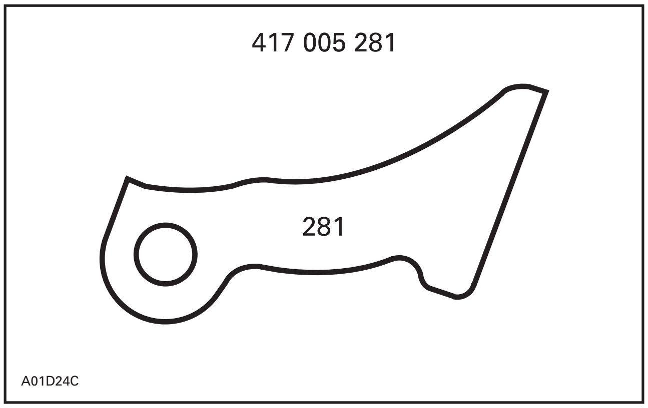
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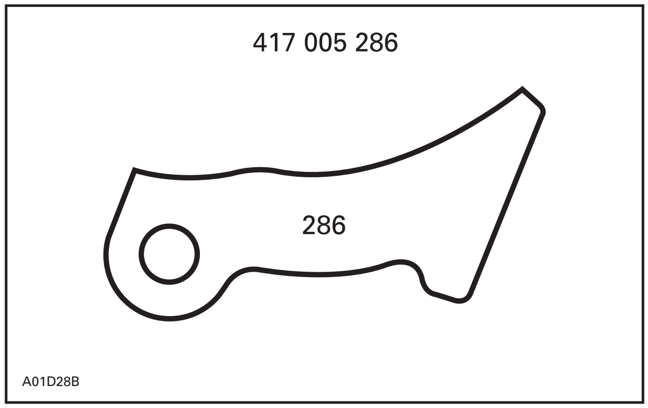
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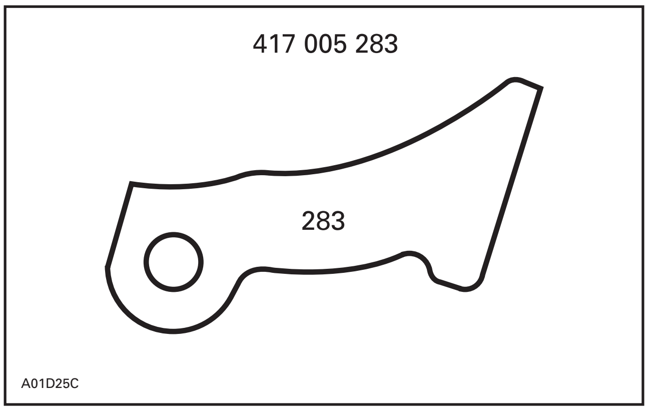
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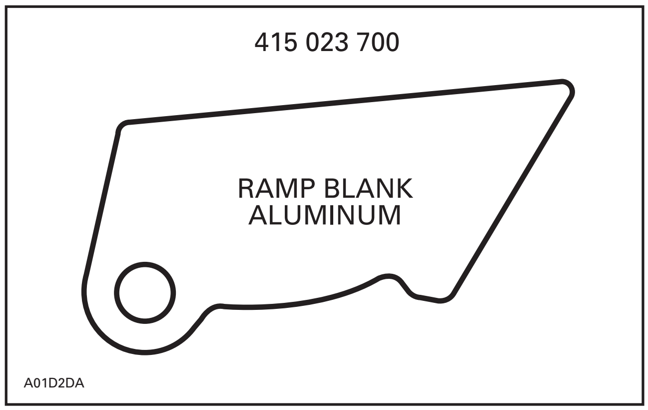
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ALUMINUM
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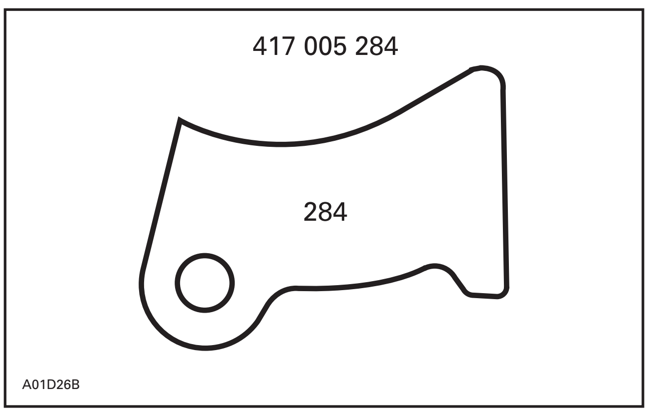
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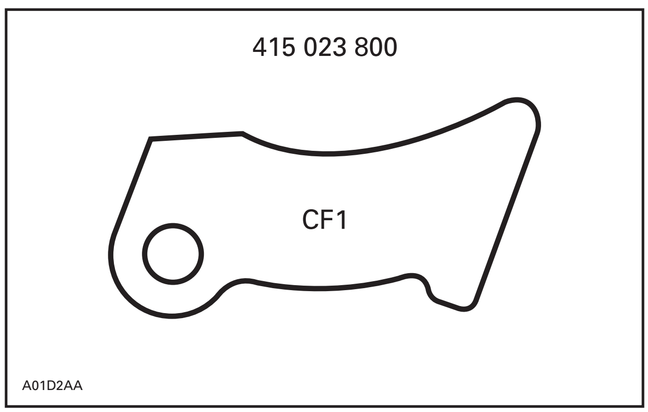
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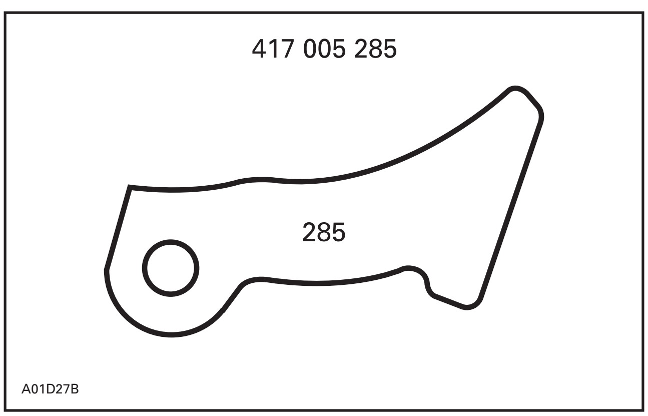
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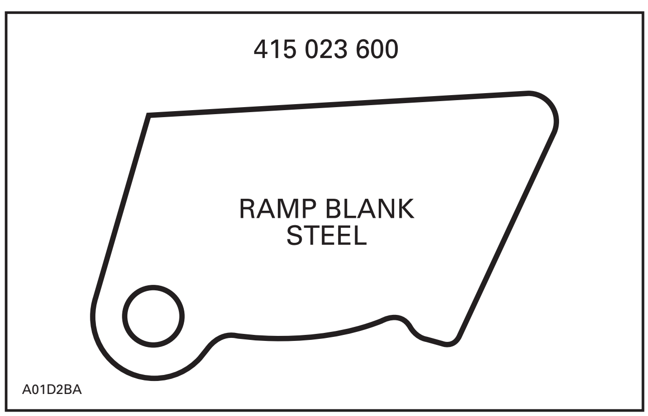
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RAMP BLANK
STEEL
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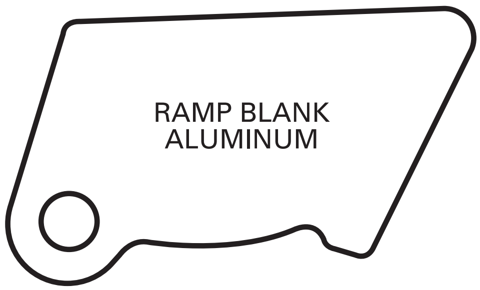
415 023 500



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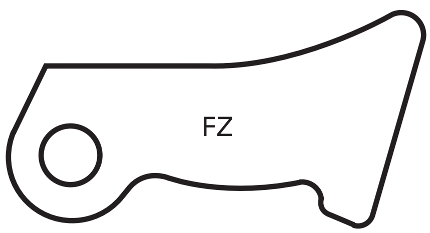

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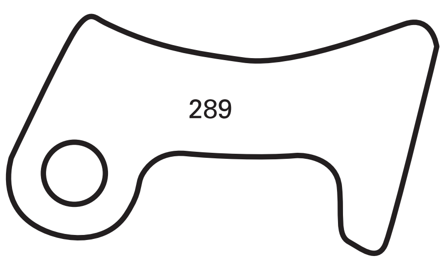

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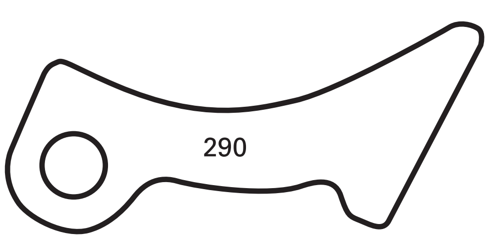

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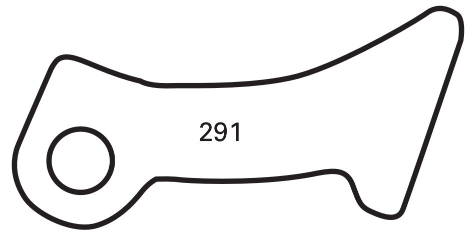

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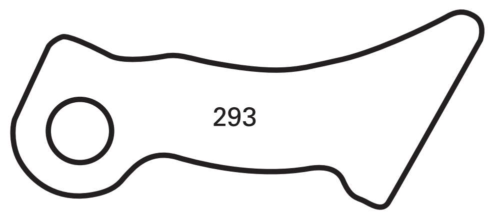

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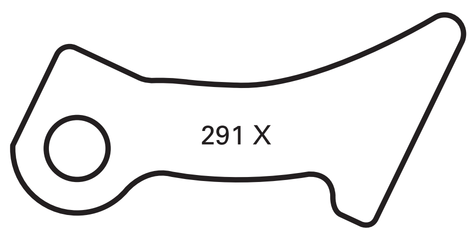

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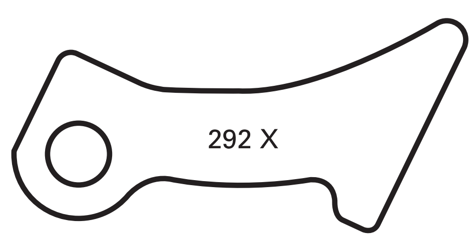

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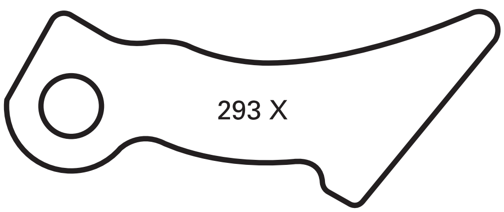

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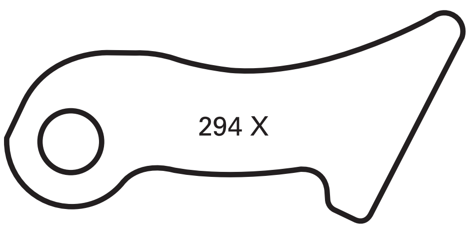

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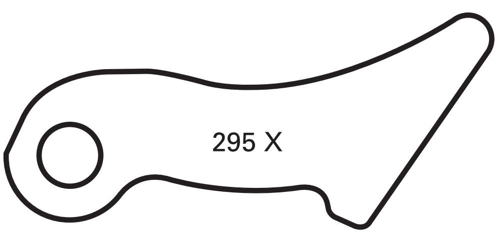

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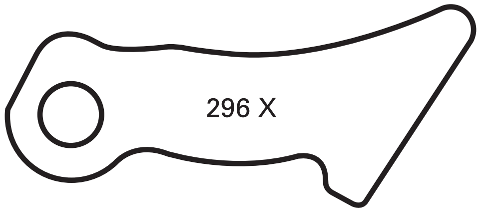

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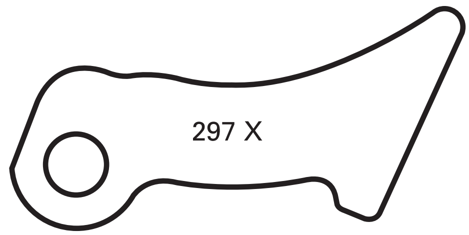

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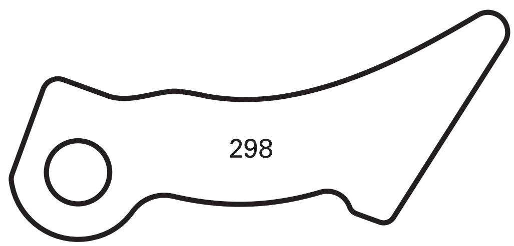

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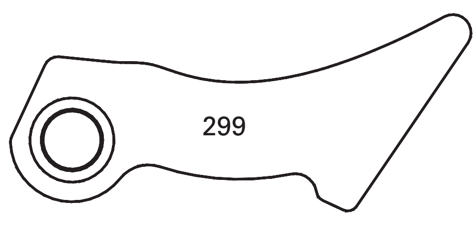

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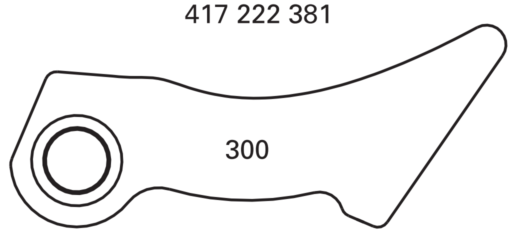

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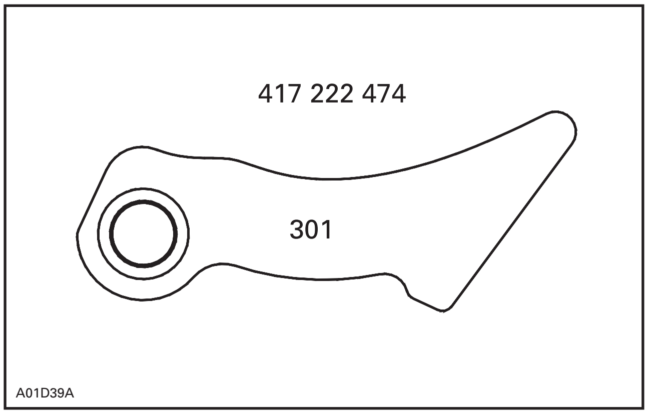


EFFECTS OF THE DRIVE PULLEY SPRING

The purpose of the clutch release spring is to return the sliding half of the engine pulley and the associated moving parts to the disengaged or neutral position at low engine RPM. The spring tension is calibrated to work with the pressure levers and ramp angles to allow clutch engagement at the desired RPM. As the engine speed increases, centrifugal forces increase and eventually overcome the tension of the release spring and allow the pulley halves to contact the drive belt. As engine speed decreases, centrifugal forces decrease and the clutch spring returns the sliding half toward the neutral position.

As the clutch shifts out to a higher ratio, the spring balances the shift forces being generated by the levers and ramps.

The spring tension will affect the entire shifting sequence of the engine pulley. The effect that it has will depend upon the construction of the spring. Three things must be known about the spring to be able to predict its effect in the clutch: 1. The spring free length; 2. The spring pressure when compressed to 74 mm (2.9 in); 3. The spring pressure when compressed to 41 mm (1.6 in). These three factors are listed on the accompanying sheet.

The spring free length will give you an idea of the condition of the spring. If the spring has lost more than 6.35 mm (1/4 in) of its listed free length, the spring is fatigued or has taken too great a set. The spring should be replaced. The free length of the spring is its overall length when resting freely on a table top.

In the TRA clutch, the installed length of the clutch release spring is 74 mm (2.9 in) This is the length of the spring when the pulley is in its neutral position. The pressure that the spring applies at this length is the factor that controls the engagement speed (all other things kept constant). When the engine pulley is in its highest ratio position, the spring will be compressed to 41 mm (1.6 in). The pressure the spring applies at this length will determine the RPM required to reach high gear; again, with all other tunable factors kept constant.

As you look through the spring chart, you will see that springs are available with equal pressures at 74 mm (2.9 in), but very different pressures at 41 mm (1.6 in). You will also note varying pressures at 74 mm (2.9 in) and equal pressures at 41 mm (1.6 in). Simply by working with the spring charts, one can easily see how the shift speed (the speed with which the change from one gear ratio to the next is made) and the engagement speed can be altered.

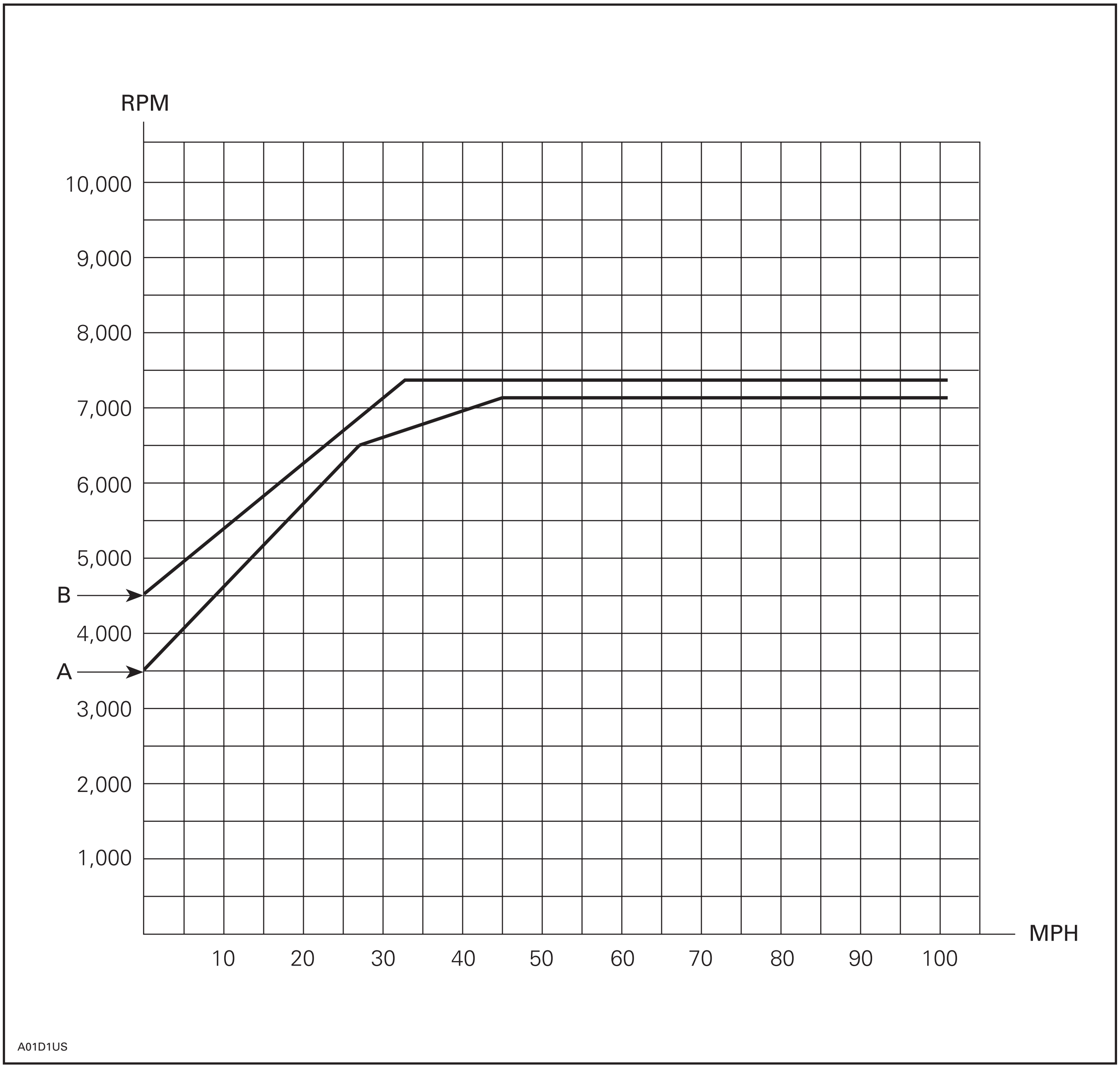
As the pressure of the spring when 74 mm (2.9 in) long is increased, the clutch engagement speed will increase. As the spring rate is increased, the engine will be required to turn more RPM to achieve a given gear ratio. Again, these facts hold true when all other tunable components are kept constant.

On chart 1, spring **A** has a pressure of 311 N (70 lb) at 74 mm (2.9 in) and a pressure of 1157 N (260 lb) when compressed to 41 mm (1.6 in). With no other changes made in the clutch, spring **B** was installed. The spring has a preload of 712 N (160 lb) at 74 mm (2.9 in) and a pressure of 1201 N (270 lb) at 41 mm (1.6 in). As the chart indicated, the engagement RPM increased 1000 RPM while the shift curve from 30 MPH up remained relatively unchanged.

Chart 2 illustrates the effect of keeping the spring preload pressure at 74 mm (2.9 in) constant and increasing the pressure at the 41 mm (1.6 in) length. In this example, spring **A** has a pressure of 311 N (70 lb) at 74 mm (2.9 in) and a pressure of 756 N (170 lb) at 41 mm (1.6 in). Spring **B** also has a pressure of 311 N (70 lb) at 74 mm (2.9 in) but increases to 1157 N (260 lb) at 41 mm (1.6 in). The projected effect of this spring change is shown on chart 2. Since the preload pressure at 74 mm (2.9 in) is equal for springs **A** and **B**, the engagement speed is not affected. At 95 MPH, however, there is a loss of RPM with spring **A** in place.

Drive Clutch Spring

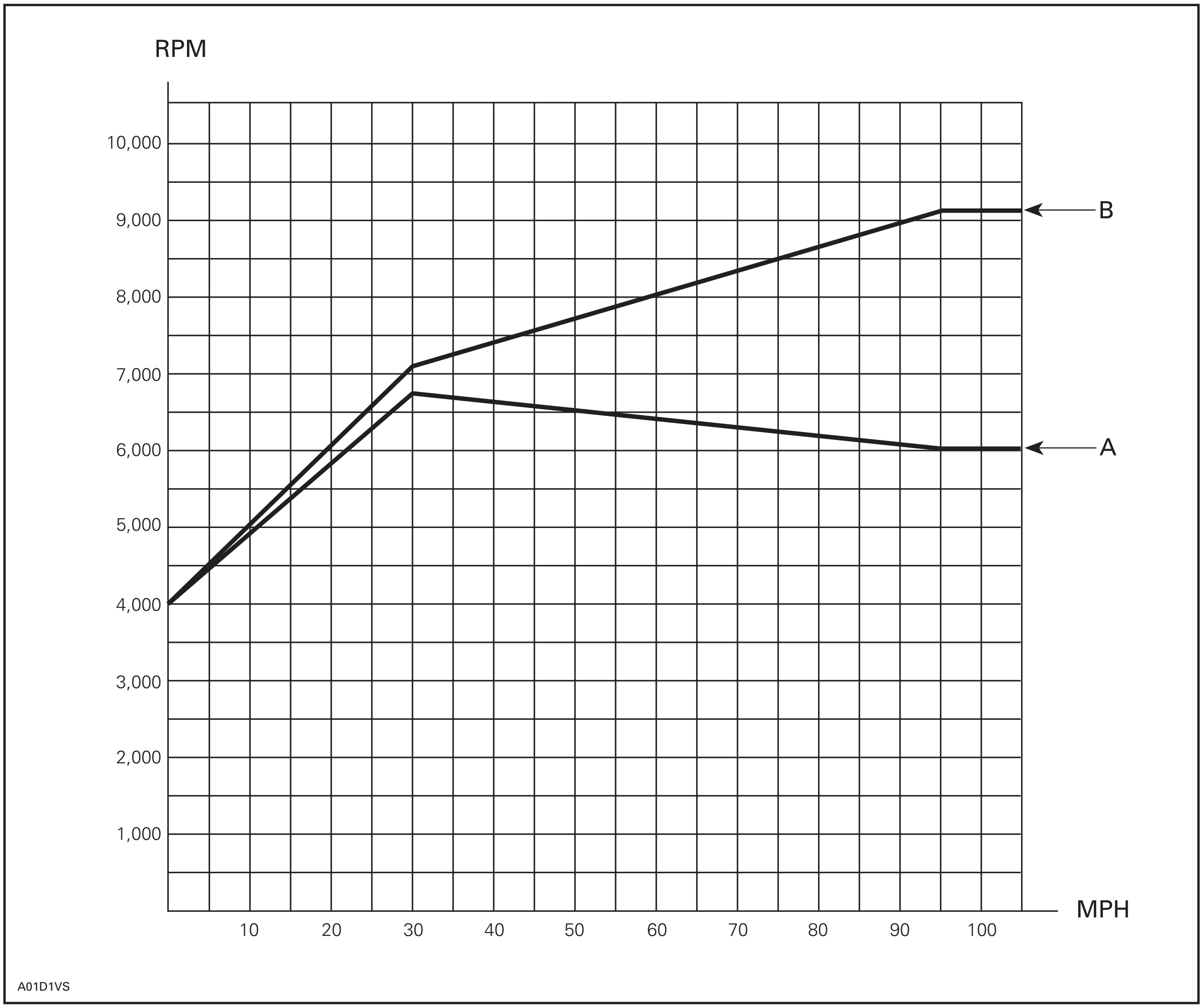
Effect at Engagement



	LOAD AT 74 mm (2.9 in)	LOAD AT 41 mm (1.6 in)
A	311 N (70 lb)	1157 N (260 lb)
B	712 N (160 lb)	1201 N (270 lb)

Drive Clutch Spring

Effect at Top Speed



	LOAD AT 74 mm (2.9 in)	LOAD AT 41 mm (1.6 in)
A	311 N (70 lb)	756 N (170 lb)
B	311 N (70 lb)	1157 N (260 lb)

TRA SPRINGS CHART

FORCE @ POUNDS ± 5% 74 mm - 41 mm 2.9 in - 1.6 in	P/N BOMBARDIER	COLOR CODE	WIRE DIA.		FREE LENGHT	
			mm	in	mm	in
70 - 170	414 689 800	RED - RED	5.26 5.00	0.207 0.197	99	3.9
70 - 200	415 015 200	RED - ORANGE	5.26	0.207	94	3.7
70 - 230	414 817 500	RED - YELLOW	5.54	0.218	89	3.5
70 - 260	414 689 200	RED - GREEN	5.94	0.234	88	3.5
70 - 290	414 691 500	RED - BLUE	5.94	0.234	86	3.4
70 - 320	414 701 000	RED - PURPLE	6.35	0.250	85	3.3
100 - 170	414 993 000	YELLOW - RED	4.88	0.192	128	5.0
100 - 200	414 689 700	YELLOW - ORANGE	5.26	0.207	110	4.3
100 - 230	414 748 600	YELLOW - YELLOW	5.54 5.41	0.218 0.213	102	4.0
100 - 260	414 742 100	YELLOW - GREEN	5.72 5.94	0.225 0.234	96	3.8
100 - 290	414 818 000	YELLOW - BLUE	5.94	0.234	97	3.8
100 - 320	414 678 400	YELLOW - PURPLE	6.35 6.17	0.250 0.243	93	3.7
130 - 200	414 639 000	BLUE - ORANGE	4.88 5.00	0.192 0.197	145	5.7
130 - 230	414 689 500	BLUE - YELLOW	5.26	0.207	125	4.9
130 - 260	414 817 700	BLUE - GREEN	5.54	0.218	109	4.3
130 - 290	414 689 400	BLUE - BLUE	5.94	0.234	104	4.1
130 - 320	414 817 800	BLUE - PURPLE	6.17 5.94	0.243 0.234	98	3.9
130 - 350	414 916 300	BLUE - PINK	6.35 6.17	0.250 0.243	96	3.8
150 - 240	414 605 600	WHITE	5.26	0.207	135	5.3
160 - 230	415 015 300	PURPLE - YELLOW	4.88	0.192	158	6.2
160 - 260	415 015 400	PURPLE - GREEN	5.26	0.207	133	5.2
160 - 270	414 605 500	YELLOW	5.26 5.54	0.207 0.218	130	5.1
160 - 290	415 034 900	PURPLE - BLUE	5.54 5.72	0.218 0.225	120	4.7

FORCE @ POUNDS ± 5% 74 mm - 41 mm 2.9 in - 1.6 in	P/N BOMBARDIER	COLOR CODE	WIRE DIA.		FREE LENGHT	
			mm	in	mm	in
160 - 320	414 817 900	PURPLE - PURPLE	5.72 5.94	0.225 0.234	111	4.4
160 - 350	414 949 500	PURPLE - PINK	5.94 6.17	0.234 0.243	105	4.1
185 - 410	415 019 500	"ALL" BLACK	6.35	0.250	105	4.1
200 - 290	414 768 200	GREEN - BLUE	5.26	0.207	156	6.1
200 - 320	414 762 800	GREEN - PURPLE	5.54 5.72	0.218 0.225	135	5.3
200 - 350	414 756 900	GREEN - PINK	5.72	0.225	126	5.0
200 - 380	414 222 371	GREEN - WHITE	5.94	0.234		
230 - 350	415 074 800	PINK - PINK	5.54	0.218	143	5.6
230 - 380	414 991 400	PINK - WHITE (OLD) RED - WHITE	5.94 5.72	0.234 0.225	128 134	5.0 5.3
230 - 390	415 019 600	GREEN	5.94	0.234	126	5.0
230 - 410	415 019 700	RED	5.94	0.234	120	4.7
240 - 430	415 019 800	BLUE	5.94	0.234	120	4.7
250 - 380	417 222 004	WHITE - WHITE (OLD) GREEN - WHITE	5.72	0.225	140	5.5
250 - 460	415 019 900	PINK	6.17	0.243	116	4.6
260 - 420	417 222 164	WHITE - SILVER (OLD) ORANGE	5.94	0.234	135	5.3
280 - 420	415 020 100	GREEN - GREEN	5.72	0.225	146	5.7
280 - 460	415 020 200	RED - RED	6.17	0.243	132	5.2
280 - 510	415 020 300	BLUE - BLUE	6.35	0.250	121	4.8
310 - 460	415 020 400	PINK - PINK	5.94	0.234	148	5.8
310 - 510	415 020 500	ORANGE - ORANGE (OR) GOLD - GOLD	6.17	0.243	132	5.2

Part numbers with a 486 prefix must be ordered from the Valcourt Race Dept. All others must be ordered from your local Ski-Doo dealer.

TITANIUM CLUTCH SPRINGS	
TENSION	PART NUMBER
180 - 410	486 103 200
200 - 290	487 103 300
220 - 320	488 103 400
220 - 384	489 103 500
240 - 380	490 103 600
260 - 380	491 103 700
260 - 410	492 103 800
280 - 410	493 103 900

EFFECTS OF THE DRIVEN PULLEY SPRING

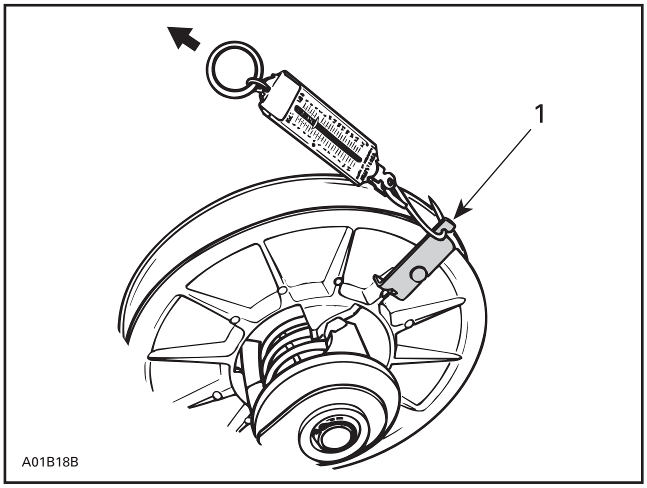
The driven pulley spring is needed to keep the plastic slider buttons in contact with the cam and to provide enough side force on the belt in the low gear position to allow initial acceleration while the torque rises to a point where the torque sensing cam begins to take over. At full load, the driven pulley spring has much less effect on the driven pulley shifting sequence than does the cam, especially at low shift ratios. At the part throttle loads at low ratios, the spring has the main effect on the shift characteristics of driven pulley.

Increases in the driven pulley spring preload will bring the engine speed up before the pulley starts shifting and will help backshift the clutch quicker. Decreasing the preload will allow a faster upshift but a slower backshift thus lowering the engine RPM.

NOTE: Control of the engine speed is done by calibrating the engine pulley not by adjusting the driven pulley spring preload. An attempt to lower the engine RPM by decreasing the spring preload in the driven pulley will result in belt slippage on acceleration. An attempt to increase engine RPM by increasing the preload will result in excessive drive belt wear and decreased efficiency in the transmission.

The driven pulley spring preload is listed in the basic specifications for all our machines. This preload tension will vary from 4 kg (9 lb) to 7.5 kg (17 lb) on models equipped with the TRA clutch.

The preload figure given in our specifications is quoted in kg (lb) of force for each machine, not in inch-pounds or foot-pounds of torque. A figure given in units of torque would require multiplying the radius of the pulley by the pull recorded on the scale. Our figures are quoted for each pulley size and it is only necessary to record the pull of the spring by attaching a scale to the rim of the pulley. The scale must be positioned at 90° to the radius of the pulley. Holding the fixed half of the pulley still, pull until the sliding half just begins to rotate. At this point, read the scale.



TYPICAL
1. Spring scale hook (P/N 529 030 900)

To change the spring tension, relocate the spring end in the sliding pulley half or reposition the spring end in the cam.

There are six holes available on a Formula cam. They are numbered 1-6. Most Formula driven pulleys have three adjustment holes in the sliding half. They are lettered A, B, C. When adjusting driven pulley tension, always refer to the tension in kg (lb) — not B-6 or A-5 hole positions for accuracy and repeatability. Moving the spring from one numbered hole to a hole adjacent will change the preload by 1.35 -1.8 kg (3-4 lb). Remember, use the number and letters as references — measure the tension for accuracy. By using various combinations, the preload is adjustable from 5 to 35 pounds (depending on spring type).

The charts below will give an approximate reference for each spring position. It will vary with different springs and cam angles.

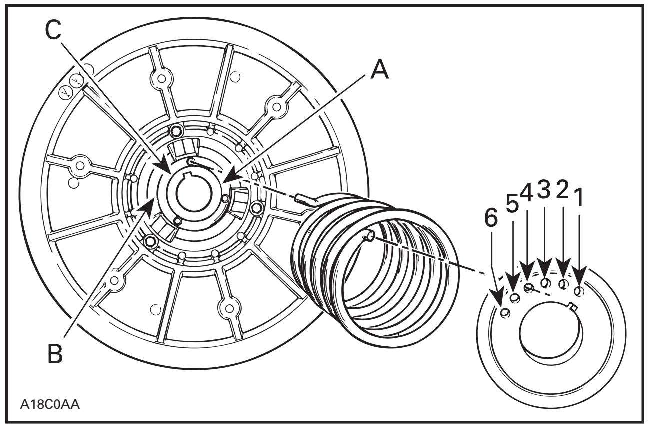
DRIVEN CLUTCH PRELOAD

WHITE SPRING/LBS			
POSITION	A	B	C
1	26	29	24
2	21	23	20
3	16	19	15
4	11	14	10
5	7	10	6
6	3	5	1

BEIGE SPRING/LBS			
POSITION	A	B	C
1	14	16	12
2	9	11	7
3	4	6	2
4	28	30	26
5	23	25	21
6	18.5	20.5	16.5

Our procedure is as follows:

- Remove the drive belt and lock the parking brake.
- Using a reliable fish scale and our spring scale hook (P/N 529 030 900) pull perpendicular to the rim of the pulley until the moveable sheave begins to open. Record the reading on the fishscale.
- Next while the pulley is still being pulled open, relax the tension on the fish scale until the moveable pulley begins to close, record the reading.
- **Next add the two readings together and divide by two. This is the number we use as our reference.**
- Recording **only the pull** reading and this will definitely allow the driven pulley tension to be too low. This low tension will lead to a noticeable drop in peak RPM and a loss of top speed.



Letters and numbers shown in illustration are actual letters and numbers embossed on parts

NOTE: Always recheck torsional pre-load after adjusting.

By experimenting with them, you may find a more efficient combination of minimum side pressure yet adequate back shifting for your particular racing application.

COLOR	WIRE DIAMETER	PART NUMBER
BEIGE	.207 in	414 558 900
WHITE	.207 in	504 152 070
YL/BK (titanium)	—	486 104 000

Part numbers with a 486 prefix must be ordered from the Valcourt Race Dept. All others must be ordered from your local Ski-Doo dealer.

EFFECTS OF THE DRIVEN PULLEY CAM

The purpose of the driven pulley cam is to sense the torque requirements of the drive axle and feed a portion of the engine torque, which has been applied to the driven pulley, back to the sliding half of the pulley. It is this side force that signals the downshift and provides side thrust to give traction to the drive belt.

The cam is acting like a screw pushing against the sliding half of the pulley. A large cam angle will act like a coarse thread while a small cam angle will act similar to a fine thread. The smaller the cam angle, the greater the side force on the sliding half of the pulley and the slower the upshift will be. This will result in higher engine RPM.

A larger cam angle will allow the pulley to upshift at a lower engine speed. Less side force will be exerted on the sliding half of the pulley and the pulley will upshift more rapidly.

On downshift, a smaller cam angle will backshift more easily and, again, tend to keep the engine RPM higher. A larger cam angle will be harder to downshift and will load the engine and reduce the RPM.

If all other variables in the pulleys are kept constant, a cam change with a smaller angle will result in a slower upshift and a faster downshift. Engine RPM will remain higher. A change to a cam with a larger angle will result in a faster upshift and the downshift will be slower. Engine RPM will be lower.

Remember the drive pulley signals or controls the upshift of the transmission while the driven pulley signals the downshift largely because of the effect of the cam.

The standard factory cam will probably work well for most **woods** type cross-countries, while a smaller angled cam may prove to be better for high speed lake cross-countries.

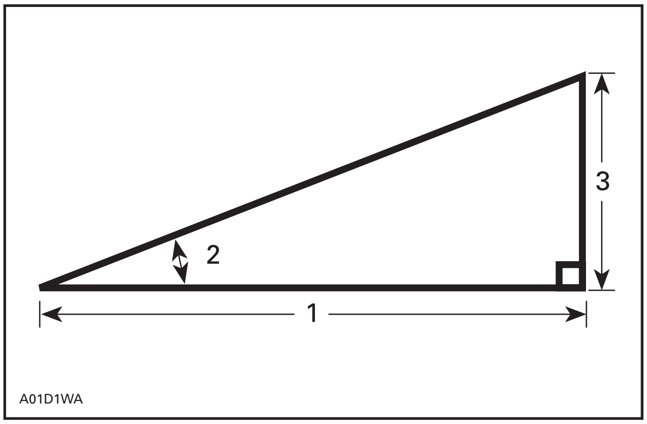
Top speed and low ET's are drag racers' and radar runners' most important concerns. Because backshifting is not at all important in these races, most racers experiment with larger cam angles for the fastest possible upshift.

Multi-angle cams are sometimes used by racers needing a good holeshot. They generally work best on vehicles where no track spin is encountered. As a vehicle idles on the starting line, the exhaust temperature cools thus slightly lowering the optimum HP RPM of the engine. Because of this, a steeper (larger) angle cam can be used to upshift more quickly, and lower the RPM to work with the cooler exhaust. As the exhaust heats up, the optimum HP RPM increases. A multi-angle cam reduces to a shallower (smaller) angle as the clutch shift out and the RPM is increased to match the **hot** HP curve of the engine. This phenomena is more pronounced on engines with narrower powerbands.

Oval and snowcross racers need the best of both worlds. A good holeshot is critical but backshifting must be quick in order to have good response out of the corners. They may have to change cam angles depending on what type of track layout is encountered.

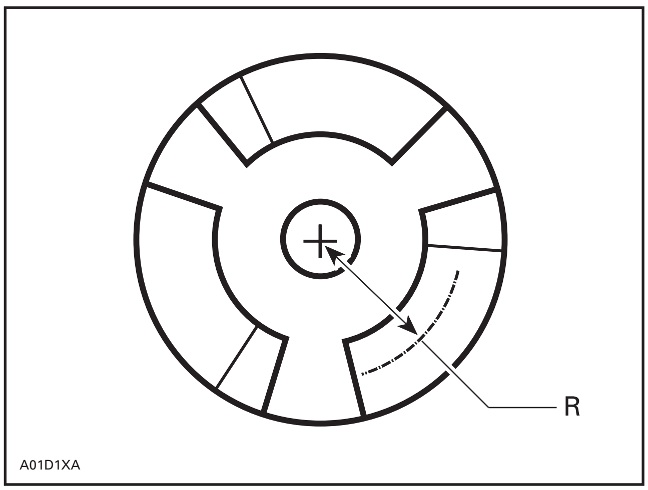
Driven pulley cams are helices. A helix is measured in lead. Lead is the distance a point moves along the axis of rotation in one revolution of the helix. (Screw threads are a helix).

The helix angle is computed from the lead and the circumference of the helix.



1. *Circumference (C)*
2. *Helix angle A*
3. *Lead (L)*

Helix angles for Ski-Doo cams are measured at the mean circumference of the cam. This is at the midpoint of the ramp surface.



Circumference (mean) = 2πR

Measuring a cam on the outside diameter will produce a different angle than on the mean diameter. A cam angle measured on the outside diameter can be converted to the **Ski-Doo spec** mean diameter angle as follows:

To simplify things, just remember that if you measure a Ski-Doo cam at the outside circumference the angle will be about 4° less than the specification (mean circumference).

Many after-market cams are measured at the outside circumference. By adding 4° you can compare them to Ski-Doo cams.

Driven Pulley Cam Specification

NOTE: All 88.9 mm diameter cams are interchangeable.

P/N	MULTI-ANGLE CAM ANGLE	P/N	CAM ANGLE
415 021 100	44° - 40°	415 022 800	30°
415 021 200	46° - 42°	415 022 900	32°
415 021 300	48° - 40°	415 023 000	34°
415 021 400	48° - 44°	415 023 100	36°
415 021 500	50° - 36°	415 022 700	38°
415 021 600	50° - 40°	504 092 100	40°
415 021 700	50° - 44°	415 022 500	42°
417 126 380	53° - 47°	—	—
415 021 800	54° - 40°	504 096 000	44°
415 021 900	54° - 44°	415 023 200	46°
415 022 000	54° - 46°	504 140 900	47°
415 022 100	54° - 48°	415 022 400	48°
415 022 200	58° - 44°	504 096 100	50°
415 023 400	58° - 48°	415 022 300	52°
417 122 200	*40° - 44°	415 021 000	54°
417 125 900	*44° - 40°	415 022 600	56°
417 126 391	*44°	415 023 300	58°

NOTE: 1995 and newer cams have more surface area to support large bushing. *MX Zx all aluminum, 2 key way.

The cams listed below are available through the Racing department in Valcourt only.

P/N	DESCRIPTION
486 074 700	Cam 37
486 074 800	Cam 40
486 074 900	Cam 42
486 075 000	Cam 44
486 075 100	Cam 47
486 075 200	Cam 50
486 075 300	Cam 53
486 075 400	Cam 56-50
486 075 500	Cam 56-47
486 075 600	Cam 56-44
486 075 700	Cam 53-50
486 075 800	Cam 53-47
486 075 900	Cam 53-44
486 076 000	Cam 53-42
486 076 100	Cam 53-40
486 076 200	Cam 50-47
486 076 300	Cam 50-44
486 076 400	Cam 50-42
486 076 500	Cam 50-40
486 076 600	Cam 50-37
486 076 700	Cam 47-44
486 076 800	Cam 47-42
486 076 900	Cam 47-40
486 077 000	Cam 47-37
486 077 100	Cam 44-40
486 077 200	Cam 44-37
486 077 300	Cam 42-37
486 077 400	Cam 40-44
486 077 500	Cam 40-37
486 099 600	Cam 43-47
486 103 100	Cam 47-50

Part numbers with a 486 prefix must be ordered from the Valcourt Race Dept. All others must be ordered from your local Ski-Doo dealer.

BALANCING OF PULLEYS

Each half of Ski-Doo driven pulley is individually balanced. This means that parts can be interchanged and that no alignment marks are needed for assembling for the complete assembly to be in balance.

The TRA clutch is similar to our driven pulleys in the sense that each major component is balanced separately.

However, there are arrows to align when reassembling this clutch. The first one is on the spring cup or cover to the sliding half. The next is between the governor cup and the sliding half. Once these have been indexed properly, the fixed half can be inserted into the clutch assembly and no alignment is needed between the inner pulley and the sliding half on 1994 and older TRA's. 1995 inner pulleys **do** have an alignment mark.

Some 1995 and 1996 models have the new cushion drive, governor cup as standard equipment. This governor cup can't be retro-fitted to other non-cushion drive vehicles due to weight imbalance. Use only complete clutch assemblies on non-cushion drive vehicles.

Truing Pulley Surfaces

The surfaces of a die cast pulley sheave are not always perfectly true. The casting cools in the die at slightly different rates which makes the surface uneven. Truing the surface in a lathe can increase efficiency of the transmission. The driven pulley sheaves have a 13.75° angle while TRA drive pulley sheaves have a 12° angle. Always remove as little material as possible when trueing these surfaces. Pulley halves need to be rebalanced after any machining.

NOTE: On 1996 and newer liquid cooled models, the drive and driven clutch surfaces are machined.

Windage Plates

Windage plates which cover the reinforcing webs on each sheave simply make the pulley more aerodynamic and reduce the amount of energy lost from pumping air. The use of these plates or covers can make a difference of one to two MPH on top end. The down side of the use of these plates is the increase in sheave temperature due to the reduction of air cooling.

Installation

⚠ WARNING

Do not apply anti-seize compound or any lubricant on crankshaft and drive pulley tapers.

⚠ WARNING

Never use any type of impact wrench at drive pulley removal and installation.

Drive Pulley Ass'y

The installation procedure must be strictly adhered to as follows:

Lock crankshaft in position as explained in removal procedure.

Install drive pulley on crankshaft extension.

Install lock washer and screw.

⚠ WARNING

Never substitute lock washer and/or screw with jobber ones. Always use Bombardier genuine parts for this particular case.

Torque screw to 105 N•m (77 lbf•ft).

Install drive belt and pulley guard.

Raise and block rear of vehicle and support it with a mechanical stand.

⚠ WARNING

Ensure that the track is free of particles which could be thrown out while is rotating. Keep hands, tools, feet and clothing clear of track. Ensure nobody is standing near the vehicle.

Accelerate the vehicle at intermediate speed and apply brake. Repeat five times.

Reduce the screw torque to 85 N•m (63 lbf•ft) then, retorque to 95 N•m (70 lbf•ft).

⚠ WARNING

After 10 hours of operation the transmission system of the vehicle must be inspected to ensure the retaining screw is properly torqued.

DRIVE BELTS

The drive belt is the critical link in transmitting power from one clutch to the other. The changes in belt technology and materials have allowed us to take for granted the kind of reliability and efficiency that not many years ago we all only dreamed about.

One of the more important changes in drive belts has been the introduction of Kevlar® Fiber B to replace fiberglass or polyester cord in the tensile layer of modern drive belts. This material is much stronger, more flexible, and allows a better adhesive bond with the various rubber compounds used to build a drive belt.

Another important change in drive belts is the increase in width. The extra width allows us to add more Kevlar cords in the tensile layer for strength with today's high output sleds.

Use only the specific Bombardier drive belt listed for your application. The drive belt is a calibrated part of the transmission system. Different belts with different compounds or angles will change how your transmission shifts.

Drive belts can vary ± 6 mm (1/4 in) length from belt to belt. Because of this manufacturing tolerance, we recommend measuring your drive belts and marking their length on the outer cover. Try to use only belts that are the same length while racing to keep your clutch set up as consistent as possible.

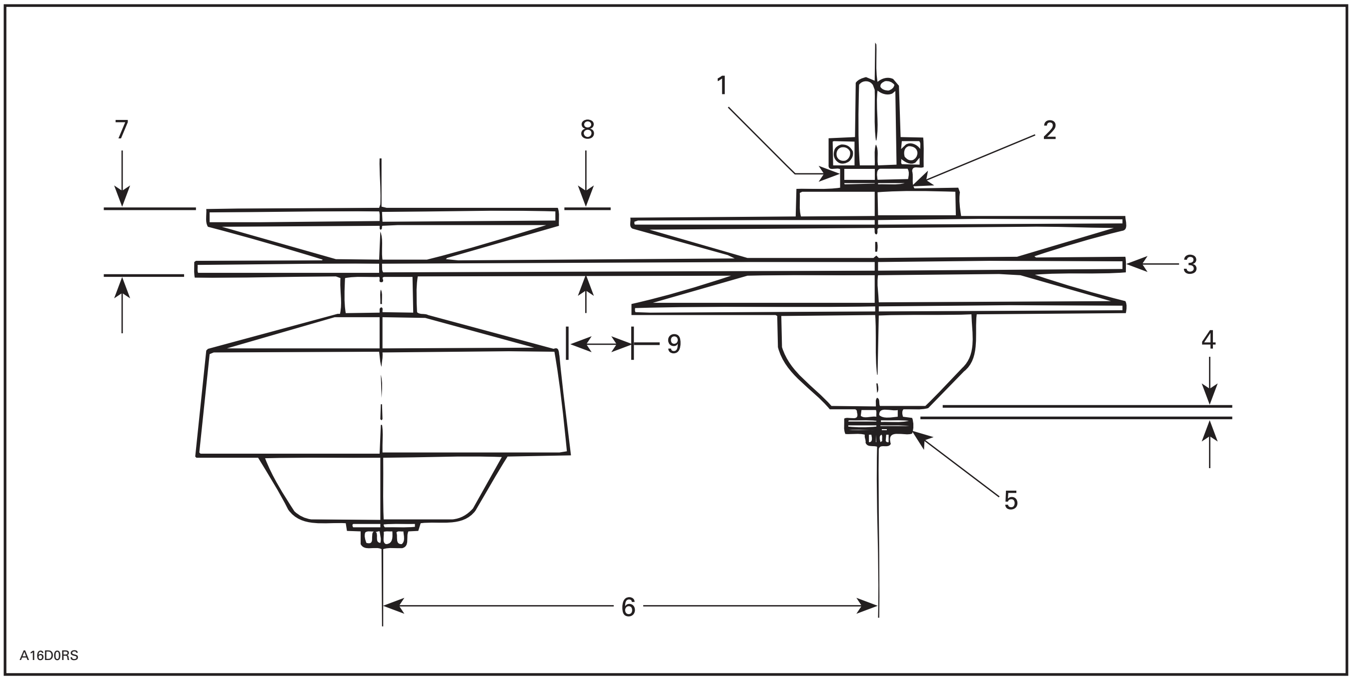
Always break in a new belt by running it easy for 10-15 miles. Vary the vehicle speed and throttle setting without going over 2/3 throttle. It is also a good idea to mark the direction of rotation on the belt. Once the belt has been used, always run it in the same direction.

Be careful not to bend sharply or coil up these new hard compound drive belts since they are much more prone to cracking in cold weather than earlier belts.

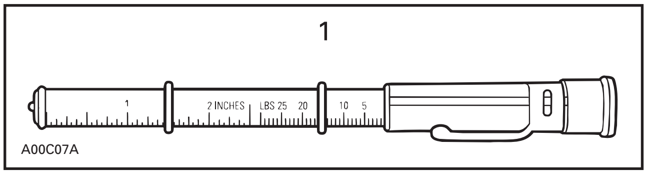
Proper deflection, setup, alignment, and break-in will help insure maximum performance and longevity from the drive belt.

PART NUMBER	WIDTH (new)	MINIMUM WIDTH (wear limit)
415 060 600	34.7 mm	32.30 mm
414 860 700	34.90 mm	32.50 mm
417 300 067	35.00 mm	33.00 mm
417 300 066	35.10 mm	33.00 mm
417 300 127	35.10 mm	32.10 mm
414 827 600	33.33 mm	30.00 mm

Proper Alignment of the TRA Clutch



1. *Sleeve (Note: no clearance to this side of driven pulley)*
2. *2 shims (504-108 -200)*
3. *Use straight bar (.375 in x 19 in)*
4. *DSA/ZX platform: 0 - 1 mm (0 - .040 in)*
5. *Shim as required to achieve clearance*
6. *PRS: 268.3 (10-9/16 in) — DSA/ZX platform: 257.5 (10-9/64 in) — CK3: 361.0 (14-7/32 in)*
7. ***Y** = X + 1.5 mm (.060 in)*
8. ***X** = PRS: 36.0 mm (1.460 in) — DSA/ZX platform: 35.0 mm (1.380 in) — CK3: 35.5 (1.398 in)*
9. ***Z** = PRS: 27.0 mm (1.060 in) — DSA/ZX platform: 16.5 mm (.650 in) — CK3: 3 pipe 123.0 mm (4.842 in) — CK3: 120.0 (4.724 in)*

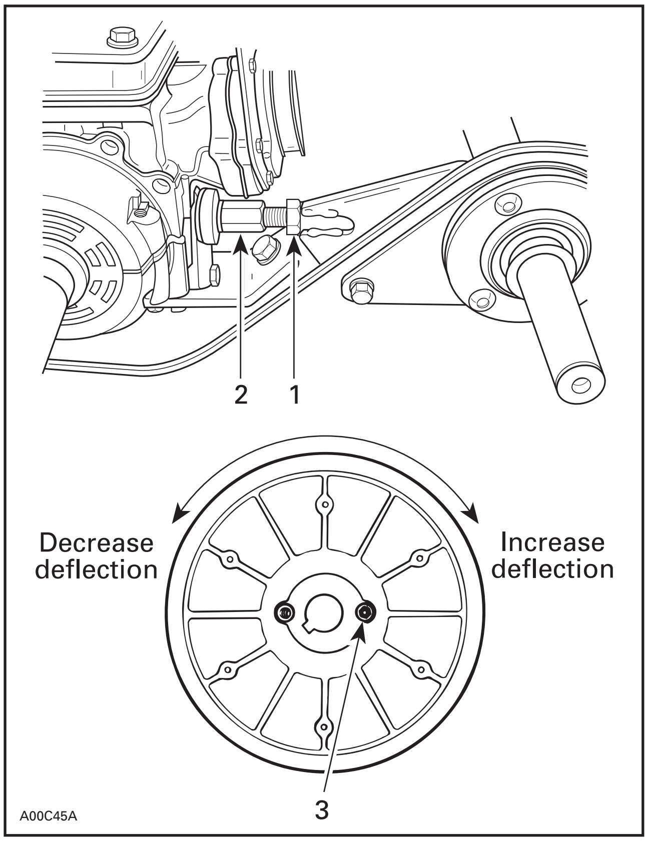


1. Use Ski-Doo tool (P/N 414 348 200)

Proper belt deflection and alignment are extremely important. Included is a page on proper alignment procedures and deflection measurement methods for your use.

Do not forget about the torque limiter rod on most models. This bolt is located between the jackshaft and the engine on the left side. It should be lightly snugged **after** the proper alignment and center to center distances have been set.

NOTE: Do not overtighten, it will misalign pulleys.



TYPICAL
1. Jam nut
2. Adjuster
3. Allen screw with jam nut

The driven pulley has one, two or three (depending upon the year) set screws on the fixed half that are used for setting belt deflection. These 3 mm Allen screws can be moved in or out to open or close the sheaves to lower or raise the drive belt in the driven pulley to achieve the correct deflection.

It is best to accurately align the pulleys and then shim the driven clutch tight. Some feel it is better to let it float and align itself. But this doesn’t happen in a dynamic situation when there is load on the belt. If you have a lot of float in the driven and you back off the throttle and the pulley misaligns, when power is applied again, the pulley will stay misaligned because of the force on the countershaft. Shimming the driven pulley tightly to the jackshaft bearing also helps to positively position the jackshaft and its left side bearing.

CHAINCASE GEARING

Contrary to popular belief, small gear changes do not directly affect top speed as long as the clutches are functioning properly. Gearing one or two teeth taller on the top will not generally make the vehicle any faster on top end unless the clutches are fully shifted out and the engine is starting to overrev.

With the TRA clutch, we have about 20 percent more shift ratio available compared to other designs. Because of this, we have been able to lower the gearing in our chaincase considerably. Yet, we still have the same overall top gear ratio because of the 0.8:1 top ratio of the TRA clutch.

This gives us better belt life by allowing our clutches to **slip** for a shorter period of time at engagement. It also provides more torque to the drive axle for acceleration.

Most snowmobiles are geared on the **high** side from the factory. They are usually geared for 8 -16 km/h (5-10 MPH) more than they would reach in average conditions. Because of this, the belt does not seem to go all the way to the top of the drive clutch. This is a normal situation. Snowmobiles run under widely varying conditions. If all snowmobiles were geared to attain a full shift under average conditions and then the vehicle were run on a perfectly smooth frozen surface, it would easily shift out to its geared top speed. Since the drag is so low under these conditions, the engine would begin to over-rev, eventually lose power, possibly damage the engine, and you will not achieve top speed.

There are other factors involved here also. As clutches shift through their range, the efficiency with which they transmit power decreases as the clutch ratio exceeds about 1.5:1. Efficiency also drops as belt speed (RPM) increases. For optimum chaincase performance ensure that you use the synthetic chaincase oil.

Because newer clutch designs shift beyond a 1:1 ratio, belt speed increases dramatically and the diameter that the belt follows around the driven pulley decreases considerably. This wastes energy and efficiency as the belt is being bent around a smaller diameter and centrifugal force is trying to pull the belt into a circular path instead of following the pulleys.

This is why for years manufacturers kept their clutch ratios around 1:1 to keep belt speeds down.

Now with the advent of larger displacement, high torque, lower RPM engines, we can use overdrive transmissions and still keep our belt speeds within reason.

As we mentioned, as belt speeds go up, efficiency drops. This is one reason many radar runners gear extremely high sometimes even approaching 1:1 in the chaincase. They have found through diligent testing that they can achieve a higher top speed without shifting their clutches all the way out because of a decrease in belt speed which means an increase in transmission efficiency. That is their bottom line.

For oval racing, the small benefit you may achieve in top end speed would probably be lost by the loss of acceleration on the start and out of the corners on a tight oval circuit.

This holds true for cross-country and snow crossers also. Top speed is not as important as quick acceleration out of the corners and ditches.

You can easily check your gearing selection by marking your drive clutch with a black marker with straight lines from bottom to top on the belt surfaces of the clutch. Go out and ride your sled under your normal conditions and stop to see how far the belt has rubbed the marker off the clutch surfaces. If it has shifted the belt all the way to the top, you may be able to pull one or two more teeth on the top sprocket. Experiment!

If it is down about 1/2 in or more from the top, you could consider trying a one tooth smaller top gear depending upon your type of racing.

The best combination of gearing for speed and acceleration you can achieve is far more important than shifting the belt **all the way to the top** of the clutches.

The following formula can be used to calculate the theoretical top speed of your Ski-Doo. The formula assumes the transmission is shifted out to its top gear ratio. Make sure you use the correct track pitch and transmission ratio for your machine.

Square shaft clutch top ratio = 1

TRA clutch top ratio = .83

Pitch of internal drive track = 2.52 in

Number of teeth on internal drive sprocket = 9

NOTE: Some Summit and long track models use 8 tooth drive sprockets.

$$\text{top speed in MPH} = \frac{\text{engine RPM}}{\text{clutch ratio}} \times \frac{\text{teeth, top sprocket}}{\text{teeth, bottom sprocket}} \times \frac{(\text{pitch of track} \times \text{No. of teeth on drive sprocket})}{12} \times \frac{60}{5280}$$

Example: 1995 Formula Z — gearing 25/44 peak power at 7800 RPM

$$\frac{7800}{.83} \times \frac{25}{44} \times \frac{(2.52 \times 9)}{12} \times \frac{60}{5280} = 115 \text{ MPH}$$

For quick reference, use the gear ratio charts provided.

A little known fact that can seriously impair a racer's performance is the misconception that the factory stated peak horsepower RPM or the peak power point you find on a dyno is the correct figure to clutch your race sled to.

Generally, this is not the case. The figures that are printed by the factory are determined on a dynamometer in clinical test conditions.

CHAINS BOMBARDIER P/N			
LINKS	11 WIDE	13 WIDE	15 WIDE
68	412 106 600	—	—
70	412 105 900	412 106 800	486 093 100
72	412 105 500	412 106 700	486 074 300
74	412 105 800	412 106 900	504 151 910
76	—	412 107 600	—

GEARS						
	11 WIDE		13 WIDE		15 WIDE	
TEETH	STEEL	POWDER	STEEL	POWDER	STEEL	ALUMINUM
TOP						
17	504 071 800	—	486 070 400	—	—	—
18	—	504 070 100	486 070 500	—	—	—
19	—	414 680 500	486 070 600	—	486 092 600	—
20	504 074 800	—	486 070 700	—	486 092 700	—
21	504 084 000	—	504 139 300	—	486 092 800	—
22	504 074 700	504 056 000	504 083 500	504 091 100	486 074 600	—
23	504 078 400	504 087 800	504 085 400	504 091 000	486 093 000	—
24	504 078 600	504 056 100	503 139 700	504 090 900	—	—
25	504 084 100	504 085 200	—	504 084 300	—	—
26	—	504 055 900	—	504 085 300	—	—
27	—	—	—	—	—	—

	11 WIDE		13 WIDE		15 WIDE	
BOTTOM						
38	504 056 400	—	—	—	—	—
39	—	—	—	—	—	—
40	414 339 600	504 056 200	—	504 089 000	—	—
41	—	—	—	—	—	—
42	—	—	—	—	—	—
43	—	504 748 500	—	—	—	489 104 600
44	—	504 057 300	—	504 085 500	486 074 400	—
44R	504 076 500	504 088 200	—	504 084 400	—	—

Part numbers with a 486 prefix must be ordered from the Valcourt Race Dept. All others must be ordered from your local Ski-Doo dealer.

TRANSMISSION CALIBRATION PROCEDURE

1. A new vehicle should be broken-in before fine tuning the transmission. 200 — 300 miles will allow things like bearings and the track to loosen-up. This will allow the sled to roll much freer which may slightly change the clutch calibration.
2. Set up the chassis configuration (lowering, weight transfer, traction).
3. Adjust the carburetor calibration to match the condition of the day.
4. Pick the chain case ratio.
5. Define the driven pulley calibration. Stock is a good starting point. Drag racers may consider trying a larger cam angle. Use multi-angle cams only for fine tuning after working with the drive clutch.
6. Choose the drive belt (compound, length, width).
7. Define the TRA calibration.
   - Start with the stock ramp in position #3.
   - For most forms of racing, a higher engagement RPM can be utilized. The better the traction, the higher the engagement that can be used. Most stock grass drag rules limit engagement to 5500 RPM. That's 5500 RPM on the technical inspector's tachometer and it may not agree with your dash tachometer. If in doubt, get the tech. man to verify your engagement. The easiest way to raise engagement is to use a spring with a higher start load and a similar finish load. Remember, the stiffer spring at start will also affect the shift curve at 0 to 1/2 ratio.
   - If the stiffer spring slowed down the shift at low ratios, try more roller pin weight. The pin weight will not change engagement much but will shift faster. Utilize the threaded roller pins to achieve pin weights in between the hollow steel and solid steel pin.
   - Fine tune the shift curve by trying different adjuster positions. Use the lowest adjuster number that still allows you to maintain RPM.
   - Pin weight and ramp angle are interrelated, but can be varied to achieve certain results. A 16.5 gram pin and the adjuster set in #5 may produce the same full throttle RPM as a 14.5 gram pin with the adjuster set in #3, but the lighter pin will be revving higher at part throttle setting at low ratios. This may work better for snowcross or woods racing whereas the heavier pin may be better in a drag race. Some ramp profiles will achieve better top speed with the adjusters set in lower numbers (1-4). If you are in position 5 or 6, try a slightly lighter pin weight (1.5 to 2 grams) and lower the adjuster position.

NOTE: Never use adjuster position #6 with the FZ ramp. The tip of the ramp may touch the lever arm.

   - If your shift curve is perfect but the engagement is too low, a flat or notch can be ground in the ramp right where the roller sits at neutral position. This is a touchy procedure and should only be attempted as a last resort. Be prepared to scrap some ramps during the learning procedure.
8. The best way to test clutching is with a set of timing lights or side by side comparison with a similar vehicle. Leave one machine as a base line reference while tuning the test vehicle. Don't change things on both vehicles at the same time or you won't know if you are gaining or losing. Also, only change one parameter at time on your test vehicle so you know exactly what results from the change.
9. For drag racers, try running the engine down to several hundred RPM below the stated power peak. When the exhaust is cold, the peak power RPM drops. How much lower depends on the engine type, exhaust type, jetting and underhood temperature. Summer and fall grass draggers should especially try lower RPM.
10. This is where the winners become winners. Test, test, test and then go test some more.
11. KEEP DETAILED NOTES OF ALL YOUR TESTINGS!!! No matter how good you think your memory is, after you test your hundredth combination, things can get overwhelming.

Transmission Tuning Test Sheet

DATE: ______________________ VEHICLE: ________________________ SHEET NO.: __________

TEST SITE: __________________ TEMPERATURE:___________________ SURFACE COND.: ______

		TEST 1	TEST 2	TEST 3	TEST 4	TEST 5
	Cam angle					
	Spring color code					
	Spring preload, lb					
	Spring position ex.: (A-4)					
	Chaincase gearing					
	Lever arm and pin type					
	Weight each assembly					
	Ramp identification					
	No. of set screws added (if used)					
	Spring color code/tension					
	TRA adjuster position					
	Belt part number					
	Width					
	Length					
	Engagement RPM					
	Shift RPM					
	Top speed					
	Time for run/measured distance					
	Variation min./max.					
	Special notes					

Racers Log

VEHICLE:		DATE:		SHEET NUMBER:
LOCATION:		SURFACE CONDITIONS:		
TEMPERATURE:		BAROMETRIC PRESSURE:		HUMIDITY:
CARBURETOR SIZE:		FUEL:		C.R.A.D.:
	PTO	MAG	Carburetion notes:	
Main jet				
Needle jet				
Jet needle				
E-clip position				
Slide cut-away				
Pilot jet				
Drive pulley			Clutching notes:	
Lever arm/pin type				
Pin weight				
Ramp identification				
TRA adjuster position				
Spring identification				
Spring pressure @ engagement				
Spring pressure @ full shift				
Engagement RPM				
Shift RPM				
Drive belt identification				
Driven pulley				
Cam identification				
Spring identification				
Spring preload and location				
Chaincase gearing				
	LH	RH	Chassis notes:	
Inches of carbide/ski				
Camber				
Front spring identification				
Ride height				
Center spring identification				
Limiter adjustment				
Rear spring identification				
Ride height				
Stud quantity and type				

TABLE OF CONTENTS

USEFUL PUBLICATIONS

DESCRIPTION	P/N
2002 Shop Manual Volume 3 – Zx Series	484 200 036
Specification Booklet 1998-2002	484 300 207

TECHNICAL DATA

Supplement for model: MX Z 600 2001

MODEL: MX Z 600 2001						
	RACING TYPE	*-GRASS DRAGS-*				
	Maximum horsepower *	RPM		*7700*		
CARBURETOR	Carburetor type					
				PTO	*CENTER*	*MAG*
	Main jet	P/N 504 108 200 no air box with filters		*500*		*500*
	Needle					
	Needle clip position					
	Slide cut-away					
	Pilot screw			*1.0*		*1.0*
	Needle jet					
	Air screw adjustment	± 1/16 turn				
	Needle valve					
	Fuel			*Super unleaded*		
DRIVE RATIO	Drive ratio	21 - P/N 504 139 300	43 - P/N 504 148 500	*21-43*		
	Chain			*74 links* *P/N 412 106 900*		
	Drive pulley	Type of drive pulley		*TRA*		
		Ramp identification		*287* *P/N 417 005 287*		
		Calibration screw position		*3*		
		Spring		*250/380* *P/N 417 222 004*		
		Clutch engagement	RPM	*5000*		
		Pin		*std*		
		Lever		*std*		
	Driven pulley	Spring	Beige	*P/N 414 558 900*		
			Preload kg (lb)	*18 lb*		
		Cam	Angle	*50°* *P/N 486 075 200*		
	Drive belt		Part number	*std*		
	Spring rave		Part number	*std*		

Calibration done at a temperature of 15° Celcius

* The maximum horsepower RPM is applicable on the vehicle. It may be different under certain circumstances and BOMBARDIER INC. reserves the right to modify it without obligation.

Supplement for model: 1999 MX Zx 440/2000 MX Zx 440

<table>
<tr><th colspan="7">MODEL: MX Zx 440 1999 and 2000</th></tr>
<tr><th></th><th colspan="3">RACING TYPE</th><th colspan="3">-GRASS DRAGS-</th></tr>
<tr><td></td><td>Maximum horsepower *</td><td colspan="2">RPM</td><td colspan="3">8200</td></tr>
<tr><td rowspan="12">CARBURETOR</td><td colspan="3">Calibration done at temperature of 30°C</td><td colspan="3"></td></tr>
<tr><td colspan="3">Carburetor type</td><td colspan="3">TMX</td></tr>
<tr><td colspan="3"></td><td>PTO</td><td>CENTER</td><td>MAG</td></tr>
<tr><td colspan="3">Main jet</td><td>220</td><td></td><td>220</td></tr>
<tr><td colspan="3">Needle</td><td></td><td></td><td></td></tr>
<tr><td colspan="3">Needle clip position</td><td>4°</td><td></td><td>4°</td></tr>
<tr><td colspan="3">Slide cut-away</td><td></td><td></td><td></td></tr>
<tr><td colspan="3">Pilot jet</td><td>45</td><td></td><td>45</td></tr>
<tr><td colspan="3">Needle jet</td><td></td><td></td><td></td></tr>
<tr><td colspan="2">Air screw adjustment</td><td>± 1/16 turn</td><td>0.5 (1/2)</td><td></td><td>0.5 (1/2)</td></tr>
<tr><td colspan="3">Needle valve</td><td></td><td></td><td></td></tr>
<tr><td colspan="3">Fuel</td><td colspan="3">Racing fuel</td></tr>
<tr><td rowspan="14">DRIVE RATIO</td><td colspan="3">Drive ratio</td><td colspan="3"></td></tr>
<tr><td colspan="3">Chain</td><td colspan="3">72 links
20-43</td></tr>
<tr><td rowspan="4">Drive pulley</td><td colspan="2">Type of drive pulley</td><td colspan="3">TRA</td></tr>
<tr><td colspan="2">Ramp identification</td><td colspan="3">CF-1</td></tr>
<tr><td colspan="2">Calibration screw position</td><td colspan="3">5</td></tr>
<tr><td colspan="2">Spring color</td><td colspan="3">250/380</td></tr>
<tr><td rowspan="3"></td><td>Clutch engagement</td><td>RPM</td><td colspan="3">5400</td></tr>
<tr><td colspan="2">Pin</td><td colspan="3">Steel thr. + 3 set screws</td></tr>
<tr><td colspan="2">Lever</td><td colspan="3"></td></tr>
<tr><td rowspan="3">Driven pulley</td><td rowspan="2">Spring</td><td>Color</td><td colspan="3"></td></tr>
<tr><td>Preload kg (lb)</td><td colspan="3">20 lb (B-6)</td></tr>
<tr><td>Cam</td><td>Angle</td><td colspan="3">47° - 42°</td></tr>
<tr><td colspan="2">Drive belt</td><td>Part number</td><td colspan="3">486 076 800</td></tr>
<tr><td colspan="2">Spring rave</td><td>Part number</td><td colspan="3">414 860 700</td></tr>
<tr><td></td><td colspan="6">* The maximum horsepower RPM is applicable on the vehicle. It may be different under certain circumstances and BOMBARDIER INC. reserves the right to modify it without obligation.</td></tr>
</table>

Supplement for model: 1999 MX Z 670 H.O.

MODEL: 1999 MX Z 670 H.O.				*PRELIMINARY*		
	RACING TYPE	*-GRASS DRAGS-*		*500'*		
	Maximum horsepower *	RPM		*7900*		
C A R B U R E T O R						
	Carburetor type			*VM 44*		
				PTO	*CENTER*	*MAG*
	Main jet			*350*	*N.A.*	*320*
	Needle			*7ECY1*		*7ECY1*
	Needle clip position			*4*		*4*
	Slide cut-away			*2.5*		*2.5*
	Pilot jet			*60*		*60*
	Needle jet			*AA4*		*AA4*
	Air screw adjustment		± 1/16 turn	*0.5 (1/2)*		*0.5 (1/2)*
	Needle valve			*1.5*	*1.5*	*1.5*
	Fuel			*Super unleaded*		
D R I V E R A T I O	Drive ratio			*23-43*		
	Chain			*Links*		
	Drive pulley	Type of drive pulley		*TRA*		
		Ramp identification		*280 P/N 417 005 280*		
		Calibration screw position		*no. 3*		
		Spring color		*230/320 Pink/Purple P/N 414 754 200*		
		Clutch engagement	RPM			
		Pin		*Solid (16 gr)*		
		Lever		*Std Aluminum*		
	Driven pulley	Spring	Color	*Beige*		
			Preload kg (lb)	*(B6)*		
		Cam	Angle	*50° P/N 504 096 100*		
	Drive belt		Part number	*414 860 700*		
	Spring rave		Part number			
	Calibration done at temperature of			*80°F*		

* The maximum horsepower RPM is applicable on the vehicle. It may be different under certain circumstances and BOMBARDIER INC. reserves the right to modify it without obligation.

TABLE OF CONTENTS

These are general guide lines for preparing a stock DSA chassis for various forms of competition. Refer to the appropriate section of the book for more detailed information.

HILL CLIMBING

Front Suspension

- Use soft springs. You want the skis to compress very easily and not transmit any upward force into the chassis.
- Use minimal rebound dampening in the shock absorbers and on HPG T/A shocks, the gas pressure can be reduced to 200 PSI.

Center

- Use medium spring pressure. You need some track pressure for traction but the front arm must be able to compress easily to absorb bumps.
- The limiter strap should be fairly short to keep front end lift to a minimum. Two to three inches of lift is plenty. A balance must be maintained between having enough traction and keeping the front end down for steering.

Rear Suspension

- Spring pressure should be kept firm in order to reduce weight transfer and help keep the front end down on the ground.
- When rules allow, use rebuildable shocks. This will allow you to calibrate compression and rebound dampening. This is necessary when changing spring rates.

Track

- Use the highest profile track available.
- On sleds with less than 80 horsepower use a 121 inch track. A deep profile long track might actually give you too much traction and the lower HP won't be able to spin the track in certain conditions.
- Bigger HP sleds should use the 136 inch paddle track. This track has 1.5 inch tall paddles molded into the track. This is standard on the Summit.
- 570 208 600 15 × 136 × 1.5 Paddle track
- 570 208 900 15 × 121 × 1.5 Paddle track
- 570 021 200 15 x 136 x 1.75 Paddle track
- 861 759 800 15 x 136 x 2 Paddle track (kit includes drive axle ass'y)
- 570 210 200 15 x 136 x 2 Paddle track
- 860 304 500 Ski stance widening kit 1996-98 Summit

Transmission

- Good backshifting is important. Use a few pounds more than normal preload on the driven pulley.
- Adjust the TRA to maintain optimum RPM.

Driving Style

- Contrary to popular belief, constant full throttle is not always the fastest way to the top. Use your thumb to adjust for the conditions. Sometimes you need to back out of it to keep the track from spinning excessively. You need to keep your momentum up but you must keep the sled on the ground so your track is hooked up and the skis can steer you around any obstacles.

DRAG RACING (ice and grass)

Special Rules

- Snow flap must be retained by 1/8 inch diameter cable.
- Double limiter straps are required by many organizations.

Front Suspension

- Lower the ride height as far as possible but maintain the legal travel requirement of two inches. Shorter springs are available.
- 415 020 600 DSA front spring 125 lb/in 8 inch free length.
- Trim the rubber blocks under the ski legs to reduce and adjust the amount of heel pressure on the ski.
- Use steel runners on the grass and stock trail carbide runners on the ice.

Center

- Use fairly stiff springs and preload.
- Shorter limiter straps will be required (414 955 300). On grass, more weight transfer can be used to keep the weight off the skis. On ice, run the limiter very short to keep ski lift to a minimum.

Rear Suspension

- Lower the ride height to the two inch minimum.
- Grass: Soften preload to help weight transfer and keep the skis from dragging.
- Ice: Use a lot of preload to help keep the front end down for better top speed at the end of the chute.
- Add two pairs of additional idler wheels and replace the 135 mm diameter wheels with 141 mm diameter wheels.
- Shave the slider shoes down to a 3 mm (1/8 inch) thickness.

Traction

- Most rules limit maximum stud height to 3/4 inch over the tallest part of the track. Taller tunnel protectors will be required.
- Generally, fewer studs are required on grass than on ice. Also, less studs are needed on good, thick sod or hard clay. More studs will be needed on loose grass, dirt and sand.
- Grass: Four steel picks per bar (4 × 48 pitches on 121 inch track = 192 studs). Large horsepower machines may need more studs. Exchange some picks for grass hooks on looser track surfaces. Use "chisel" style studs. They have a wider profile but are still sharp on the ends.
- Ice: Stud quantity is directly related to horsepower on the ice. Up to about 80 HP, 4 to 5 ice picks per pitch should be used for a total of 200-250 studs. 80 to 105 HP should need 6 to 7 picks per pitch for a total of 300-350 studs. Over 110 HP will require 7 to 8 picks per pitch and possibly hooker plates welded to the track guides.

NOTE: The installation of hooker plates will require modification to the tunnel protection system and should be approached with caution.

- Two inch, two hole angled aluminum backer plates should be used when many studs are required. They should form the basis of your stud pattern with single, square, flat or angled backer plates used in between.
- Studs should be placed so the pattern does not repeat itself for 4 to 6 pitches.

Transmission

- Gear for about 10% over the actual speed you will run in the race. On grass, your upper sprocket should be about two teeth smaller than on the ice.
- Always stay with the same belt type and size, belt deflection, and center to center distance. Have several belts of the same size broken in and ready to race. Don't test with one belt and then throw on a new one for race day.
- Use a ramp and spring combination to achieve a 5500 RPM engagement. It is best to stay around 5300-5400 unless you know how your tachometer compares to the tech. inspectors tach.
- Keep the clutches clean! The pulley faces and belt should be wiped down with acetone before every run. Excessive pulley heat indicates belt slippage and you may need to recalibrate your clutch to squeeze the belt harder.
- Torque is what overcomes resistance to rolling. Normally peak torque is about 200 to 300 RPM below peak horsepower. Try to clutch to the peak torque RPM.
- Tune your clutches so that you run best for the final which means everything will be heat soaked. If your sled requires different set ups between early runs when everything is cold and later runs, know what to change and when to change it. Test under a variety of conditions so you are prepared for any track and race conditions.

Cooling

- Install a pair of hydraulic quick couplers in the coolant hoses at a convenient location on the sled. Make a cooling cart using a cooler filled with ice and several winds of copper tubing inside (or another type of heat exchanger) connected to an electric pump and another set of quick couplers. Connect your sled to this mobile refrigerator between runs to circulate coolant through the system and cool the engine down. Cool the engine to the same temperature every time so your runs are consistent.

Fore more drag racing information contact Racing Dept. by fax at (715) 847-6869, phone (715) 847-6884.

SPEED RUNS

Generally, a speed run sled will be set up very similar to an ice drag sled with the following differences.

- Some organizations do not allow lowering for stock class sleds. Check your rules. Shorter springs may be an option to try.
- Because holeshots are not important, engagement speed does not have to be set at 5000 RPM. Top speed at the end of the course is the only concern.
- Chaincase gearing can be set for high theoretical top speeds. Use the largest top and smallest bottom sprocket available. This will keep the belt low in the drive pulley which lowers the belt and countershaft speed which makes the transmission more efficient.
- As few studs as possible should be used. It takes energy to push a stud into the ice and pull it back out again. Since holeshots are not important, use only enough studs to maintain control at top speed.
- Use standard trail carbide runners with the sharp edge worn down a bit. This way you will have steering control without sacrificing speed.
- Run with a very short limiter strap and soft center spring. This will reduce the track approach angle which helps top speed.

For more speed run information contact Racing Dept. by fax at (715) 847-6869, phone (715) 847-6884.

OVAL RACING

Special Rules

- Rear of tunnel must be enclosed per specifications in the I.S.R rulebook.
- Snowflap must be retained by chains or 1/8 inch diameter cable.
- Tail light AND brake light element must be on at all times! Add a jumper wire inside the taillight assembly.
- Any glass lenses must be taped over with clear tape.

Front Suspension

- Lower the ride height to the two inch minimum travel requirement. Shorter springs are available.

P/N 415 020 600	DSA front spring	125 lb/in	8 in free length
P/N 415 020 700	DSA front spring	150 lb/in	8 in free length

- Camber: Left = 0 degrees
  Right = Negative 2 to 4 degrees
- Verify ski toe out at the carbide edge.
- Another trick is to fill the swing arms with spray foam insulation. When the foam hardens it helps the swing arms resist bending without adding much weight.
- Steering ball joints should have as many jam nuts added as will fit between the tie rod and the ball joint. This helps prevent bending of the threaded portion of the ball joint.

Center

- Use spring P/N 415 020 800 (70 lb/inch, 6 inch free length) and soft preload.

Rear Suspension

- Lower the ride height to the two inch minimum travel requirement.
- Install a 4th idler wheel on the rear axle.
- Stiffer springs and firm preload may be required to reduce weight transfer and help keep the skis on the ice. If the handling is generally good but the inside ski is lifting, increase the right rear spring preload.
- Remove non guide clips and install taller track guides on the right side of the track or use designated oval track.

Traction

- Most rules limit maximum stud height to 3/8 inch over the tallest part of the track. Track cutting is illegal. A camoplast oval track is available P/N 679 9844, it has 3/4 inch lug height and tall guide clips for oval racing.
- Use a thin profile, sharp tipped stud for hard ice conditions. If the track conditions get sloppy, exchange some picks for a chisel or wedge type stud.
- Seven picks per bar for a total of 336 studs will be required for all sleds up to about 100 HP. Bigger sleds may require more picks and/or hooker plates.
- Use 2 inch, 2 hole angled aluminum backer plates for the majority of your pattern, especially on the outside belts. The right hand belt will need a 2 inch plate on every pitch. Fill in the pattern with 1 inch square backer plates. The pattern should not repeat itself for at least 5 pitches.
- Use a good quality square bar carbide runner with 10 inches of carbide for starters. As you gain experience, try 14 inches of carbide for more front end bite.
- Studs and carbides need to be SHARP! The carbide must shave your fingernail when scraped across and studs must prick your finger.

Controls

- You will probably be more comfortable in the corners if you make a curved extension for the left side of the handlebars. Many drivers make a new set of bars from the same size tubing and custom bend it to fit their preference. (Check your rule book for requirements on handlebars).
- You may also want to fabricate a stirrup for your right foot.

Transmission

- You need aggressive shifting to get a good hole-shot but you also need good backshifting. Here again, testing is the key to success.
- Use the lowest TRA setting that still allows you to maintain correct RPM when exiting the corners.
- Gear for the speed you will go on the course.
- Break in several belts of the same type and size and set up your pulleys to work with these belts.
- Maintain your clutches on a weekly basis. A clean, free moving driven pulley is important to good backshifting. Clean the pulley faces with acetone on a regular basis.

For more Oval Racing information contact Racing Dept. by fax at (715) 847-6869, phone (715) 847-6884.

Physical Conditioning

- While a well set up sled will be easier to drive than a poor one, it still takes good arm strength to turn a stocker with aggressive carbide. Train your upper body for strength and endurance. A good overall conditioning program that also works your legs and respiratory system is a smart idea. While it may not seem like 3 lap heats are very long, 10 lap finals on a short track with tight corners can really wear you down.

CROSS-COUNTRY/SNOW-CROSS RACING

Your team should be organized well in advance and hold regular meetings to cover key information. It is very important that all team members be familiar with each others duties and be prepared to assist one another as required. Remember situations develop with little or no notice and a well organized team can turn negatives into positives and increase the team's chance of winning!

Recommended Team Structure

IT IS RECOMMENDED THAT THE MINIMUM TEAM STRUCTURE BE AS FOLLOWS;

1. RACE DRIVER
2. CHIEF MECHANIC
3. ASSISTANT MECHANIC
4. TEAM MANAGER

Duties of the Mechanic and Team Manager

THE MECHANIC(S)

1. PRE RACE PREPARATION — To ensure that they are familiar with all aspects of the Ski-Doo snowmobile and capable of doing the worst case scenarios, which are track changes and motor repairs. These and other repairs such as those to suspensions must be practiced enough times to ensure perfection. Remember power tools are seldom accessible when working at the start line therefore get used to hand tools and operating in the cold.
2. ON RACE DAY — Each morning it is recommended that the mechanic(s) warm up, refuel and move the sled to the start line as directed by the race officials and as early as possible to get a good spot. The mechanics should take a warm up stand and cover with them to the start line. Take a spark plug wrench and spare plugs so the driver's spares don't have to be used.
3. AT THE FINISH LINE — Intercept the driver and ask what has to be done to the machine to get ready for the next heat or day and start planning the work session. You may have to really question your driver closely for feedback on the sled's requirements as he may be too tired to recall or too busy bench racing with the other drivers. Remember you may be working outside in the open and must be prepared to operate in rain or snow.
4. DAILY WORK PERIOD — Use the maintenance checklist as a guide line and add on must-doo items resulting from day's ride.

Post this list on the tool box and check off items as they are completed so that one mechanic doesn't repeat the other's work in error.

THE FIRST ITEM CHECKED SHOULD BE THE TRACK, AS DAMAGE TO IT OR SUSPENSION PARTS MAY NOT HAVE BEEN NOTED BY THE DRIVER. THE TRACK MUST BE ROTATED FOR ONE COMPLETE REVOLUTION TO PROPERLY CHECK. BOTH MECHANICS SHOULD OBSERVE AT THE SAME TIME.THIS IS THE IDEAL OPPORTUNITY TO INSPECT THE FRONT END, INCLUDING SKIS AND THEIR CARBIDES.

Make sure that you have a parts runner(s) at the fence closest to your area and use them to bring the parts from your race trailer. I-500 type events have regulations to control parts delivery and usage so make sure you check with race officials before doing something which could penalize your driver.

5. POST RACE PERIOD — Make sure you have all your own tools back and replace or re-order parts used and be ready for the next day. Go over your work with the other mechanic and driver to compare notes and things to watch for during the next day's ride. Get ready for the crew/driver meetings and maybe fit in some dinner.

DUTIES OF THE TEAM MANAGER

1. PRE RACE PREPARATION — The team manager has an important job to do and must pull everyone and everything together in an organized fashion. Time spent in preparation is seldom wasted. He/she must assemble all the documentation and paperwork for the whole team and maintain a master file. All snowmobile registration, insurance, hotel arrangements, entry information, etc., and back up copies must be available quickly. It is a good idea to confirm your hotel reservations one week before and ask for a fax map if you are not sure of the location. File everything in your driver's race binder for easy access.

2. DAILY START LINE — Get up first and make sure all mechanics are up and getting ready to leave. Let your driver sleep in as long as possible but make sure your vehicle (the second one) starts before the mechanics leave for the impound area. Ensure all rooms are checked out of and paid for. Phone ahead to confirm the next hotel's reservations. Get your driver up on time and get him to the start line at least 15 minutes before his flight leaves. Make sure that you have an overcoat for your driver to wear at the start line to keep warm until he leaves. Wait until your driver(s) leave the start and then make your way to the finish line and work area for that night.
3. DAILY FINISH LINE — Get on the road as soon as possible leaving the mechanic(s) and the registered support vehicle to follow along the official route and the various checkpoints. Make sure you have your drivers warm up coat and gear bag with his post race clothing. Check in to the next hotel and get all the room keys before going to the finish line. Get any parts or support organized that couldn't be done by the mechanics and try to intercept your driver as soon as he gets in. Ask him for sled feedback as soon as possible so that the work plan can be initiated even before the mechanics arrive. Remember on multi day events the sled may be impounded at this point and therefore may not be inspected prior to work period.
4. WORK PERIOD — You may not be able to get inside the work area but should position yourself along the fence closest to your mechanic's area. Be ready to run for parts and assist as required. Keep track of the parts used, borrowed or given away to your driver and other teams. Make sure the warm up stand and cover are available for overnight storage.
5. POST WORK PERIOD — Help sort out the parts and get ready for the next day's routine. Look for a convenient place to eat and make sure everyone is on time for the crew/driver meetings. The team manager must attend the crew meeting with the mechanics while the driver attends his separate meeting. Make sure all keys are handed out prior to the meetings as the drivers normally meet longer and it would be nice to get the support crew back to the hotel first. Make sure wake up calls are in and backup alarms on. Make a list of room numbers for quick use.

CROSS BORDER INFORMATION

1. **IF YOU ARE A CANADIAN OR US CITIZEN** — You will need valid ID at both borders. This would include a birth certificate or a drivers license or a passport for all team members. The team manager should double check all members for ID before leaving the home town.
2. **OTHER COUNTRIES** — You will need a valid passport for all team members from countries other than the US or Canada.
3. **BORDER CONFIRMATION** — It is better to be safe than sorry, so if you have any doubt contact a border official directly and do it well before race time.
4. **SNOWMOBILES AND SUPPORT VEHICLES** — Ensure that all support vehicles and snowmobiles have valid ownerships, registrations and insurance for the state or province of origin. Do not forget about your trailer!
5. **PARTS AND EQUIPMENT** — As a general rule the border officials will let race teams pass with little difficulty but large inventories of parts that appear to have a retail use may be subject to a temporary bond.
6. **HEALTH INSURANCE** — Check your personal health insurance plan to see what coverage is in effect while in another country. You may want to supplement your existing policy with temporary Blue Cross or equivalent for the driver and all team members.

Team Press Coverage and Sponsor Recognition

You should make sure that all current and future potential sponsors are looked after in a professional manner. Here are a few tips;

1. PRE RACE COVERAGE
   – press articles and newsletters
2. SLED AND TEAM IDENTIFICATION
   – jackets, hats, trailer graphics
3. RACE REPORT
   – phone back home daily to a central contact
4. POST RACE TEAM PHOTO AND REPORT
   – take a camera
5. THANK YOU LETTERS AND PRESENTATIONS
   – remember your crew

RACE CIRCUIT RULES

Remember it is the driver and team's responsibility to have the sled race-ready in accordance with the rules of the circuit you race in. All races approved for Ski-Doo's Winners Circle contingency awards are governed by the general rules laid out in the ISR annual handbook. It is common practise for the various race associations across North America to modify the ISR rules for local use. This does result in conflicting standards and therefore every driver must carefully check the rules.

Contact the following circuits for detailed race rules.

ISR	International Snowmobile Racing	262-335-2401 PH 262-335-9440 Fax
WSA	World Snowmobile Association	763-493-9900 PH 763-493-9910 Fax
CSRA	Canadian Snowcross Racing Association	905-476-7182 905-476-7157 Fax
ASRA	American Snowcross Racing Association	905-476-7182 PH 905-476-7157 Fax
RMR	Rock Maple Racing	802-368-2747 PH
USSA	United States Snowmobile Association	920-732-3563 PH 920-732-3900 Fax
MRPPI	Motorsports Racing Plus Pro Ice	612-428-3800 PH 612-428-3897 Fax
SCM	Super Competition Motorsport	450-794-2298 PH 450-794-2450 Fax
PRO	Power Sled Racing Organization	315-827-4849
FANS	First American North Star Series	218-222-3810 PH 218-222-3809 Fax
MSDRA	Michigan Snowmobile Drag Racing Association	734-995-6995
CSRC	Colorado Snowmobile Racing Club	970-663-2296
CCC	Colorado Cross Country	907-468-4839
MIRA	Midwest International Racing Association	517-736-6784
RMSHA	Rocky Mountain Snowmobile Hillclimb	435-752-1892

PARTS SUPPORT

The **Ski-Doo** factory support trucks will be on hand at most major Snowcross, grass drag and oval events across the U.S. and Canada. The purpose of these trucks is to provide parts, and technical support for all racers racing Ski–Doo snowmobiles.

The Ski-Doo race support trucks carry an extensive inventory of parts, however it is always best to be self contained and not to count on anyone but himself for parts support.

Below is a list of Base Gasket part numbers and thickness for the 453 Rotax.

BASE GASKET P/N	THICKNESS	
	mm	(in)
420 931 580	0.3	(.012)
420 931 582	0.6	(.024)
420 931 583	0.5	(.019)
420 931 584	0.8	(.031)

2001 MX Zx 440 SPRINGS

FRONT SHOCK SPRING			
P/N	SPRING RATE	FREE LENGTH mm	COLOR
505 070 692	55-85	320	BL/GN/RD
CENTER SHOCK SPRING			
503 189 325 (standard)	150	242	YL/SI/YL
415 070 500 (softer)	135	242	BL/YL/YL
REAR TORSION SPRING			
P/N	WIRE DIAMETER mm	OPENING ANGLE	COLOR
503 189 443 RH (std)	11.11	95°	GN/GN/GN
503 189 445 LH (std)	11.11	95°	GN/GN/GN
503 189 627 RH (softer)	10.6	90°	YL/WH
503 189 629 LH (softer)	10.6	90°	YL/WH
503 189 522 RH (harder)	11.11	90°	GN/GN/YL
503 189 524 LH (harder)	11.11	90°	GN/GN/YL

2002 MX Zx 440 SPRINGS

FRONT SHOCK SPRING		
P/N	SPRING RATE	FREE LENGTH mm
505 070 575	293	45
505 070 941	150	315
CENTER SHOCK SPRING		
503 189 990	215	189
503 189 988	215	64
503 189 999 (option)	325	189
REAR TORSION SPRING		
P/N	WIRE DIAMETER mm	OPENING ANGLE
503 189 992 503 189 994	—	—

SUGGESTED SPARE PARTS

You should have a self-contained parts supply. The factory parts truck won't always be there to back you up.

TEAM SPARE PARTS:

- parts book
- piston assembly and circlips
- rotary valve disc
- tuned pipe
- radiator cap
- gas cap
- drive belts
- carb. inlet needle and seat
- drive and driven clutch springs
- drive and driven slider buttons
- TRA adjuster screws and nuts
- drive clutch retainer bolt
- brake fluid
- steering tie rods and ball joints
- ski shock assembly
- skis and carbide runners
- ski bolt and nut
- track guides
- speedometer cable
- idler/rear axle wheels with bearings
- track adjuster bolts
- light bulbs
- high windshield and O-rings
- tether cord and switch
- injection oil studs
- handle bars and grips
- shop manual/specification booklet
- engine gaskets, seals and O-rings
- rewind assembly and components
- exhaust springs
- spark plugs
- spark plug caps and wires
- primer line fuel line and filters
- primer
- main jets
- chaincase chain and sprockets
- TRA clutch puller and forks
- TRA clutch rollers
- driven pulley circlip and keys
- brake lever
- radius rods and rod ends
- brake pads
- steering arms
- padding and tape for ski loops
- front swing arms
- throttle cable
- throttle lever and housing
- rear axle spacers, washers, bolts
- rubber suspension bump stops
- tail light assembly
- hood latch rubbers
- synthetic chaincase oil.

SUGGESTED SPARE PARTS ON BOARD SLED

Enough tools to perform all maintenance period requirements in the event that your crew is delayed enroute to the impound.

- spark plugs
- drive belts
- rear idler wheel and bolt
- long rubber bungees
- small hatchet and hammer
- shop rags
- tie rod ends
- small flashlight
- small container of injection oil
- throttle cable and lever
- windshield O-rings
- safety wire, tie wraps and duct tape
- de-icer
- pry bar
- emergency starter rope
- bolt and nut assortment
- small tape measure
- camping knife.

Maintenance Check List

Driver: ______________________ Mechanic(s): ______________________

Problems observed/reported: (double check with driver) ______________________

____

____

Parts needed for work period/pit area: (fuel and lubes) ______________________

____

____

Tools/Equipment Needed for Work Period/Pit Area:

- cover and jackstand
- pieces of carpet to lay on
- 3 flashlights
- one magnet
- pop riveter
- WD40
- shop rags
- contact gloves
- tie wraps
- brake fluid
- antifreeze
- large hammer and pry bar
- clip board, checklist and markers
- other:
- toboggan/cart for tools and parts
- 1 tool set per mechanic
- clutch tools including alignment bar
- hand drill and bits
- devcon
- contact cleaner or acetone
- silicone seal
- duct and electrical tape
- injection and chaincase oil
- deicer
- tape measures
- grease gun
- safety wire

Things to DOO During Work Period or Between Heats:

- carefully remove ice and snow build up
- front and rear suspension
- inspect suspension components
- check/replace studs
- check camber
- check tightness of all suspension
- bolts
- check all idler wheels for missing
- rubber and condition of bearings
- lube steering and front suspension
- ball joints
- check chain tension and oil level
- check clutch alignment and clean
- pulley faces
- check carb. and air box tightness
- coolant hose condition/routing
- check electrical connections
- other work:
- inspect track for damage and
- missing guide clips
- check skis and carbides
- check ski toe out
- check drive axle seal
- check brake disc and pad condition
- grease all zerk fittings
- check track tension and alignment

– check brake fluid and operation
– inspect drive belt
– check exhaust system and springs
– check throttle and oil cable and
– check light bulbs.

Replace any tools or parts used from race vehicle supply.

Shut off fuel before impound.

FAX HOTLINE SERVICE

Up to date snowcross technical information is available from the Ski-Doo Racing Department by way of a tip sheet.

If you have a designated fax line and wish to receive the tip sheets. Please contact the Racing Department at (715) 848-4971.

We also encourage your feed back and would like to hear about any problems or possible solutions you may have.

Some Ideas

1. Consume a high carbohydrate diet (see nutrition tips). These foods will nourish your muscles with muscle sugars (glycogens) the better your muscles are "fueled" the less fatigued you will be during and after training and on race day. The less time you have for training the more important it is to eat properly and lets face it, we all have jobs that get in the way of your sport so plan accordingly.
2. Right after training or a race, start consuming carbos such as fig bars, fruit, etc., to start replacing depleted stores.
3. Drink lots of fluids to maintain hydration and make sure you "warm down" after training to bring your heart rate down slowly and to gently work out the by-products of exercise.
4. A small cup of caffeine coffee might be consumed just prior to race. It may enhance your performance by making you more alert. This should be experimented first in training to ensure there are only positive effects.
5. For XC and SNOW CROSS racing, endurance type training activities that enhance your stamina and breathing control are best. Running for periods exceeding 30 minutes is the best way to improve stamina. The more and faster you run the better your breathing control will become. These abilities will pay off in short burst, SNOW CROSS events and long distance events like the I-500. When you lose breathing control and start hyper-ventilating you quickly lose concentration and then 2 things generally happen; you slow down and get passed or you suddenly become part of the landscape adjacent to the trail!
6. A good daily routine should involve a cheap and highly portable format that relies on no equipment and can be done just about anywhere therefore making it **excuse proof**. Try this one;
   a. 8 chin-ups — full arm extension.
   b. 25 push-ups — chest [not belly] touching the floor.
   c. 32 sit-ups — knees bent, hands locked behind head.

As you start training, quality is more important than quantity therefore do 1 good chin-up at a time if that is all you are capable of completing. The next day try 2 and so on until you are up to 8. The secret to improving is not quantity of exercise but frequency and quality; in other words you will see more progress by doing 1 good chin-up 8 times daily than doing 8 poor ones once a day. You must place pace yourself or you are inviting muscle damage that will prevent you from riding.

7. As mentioned previously, running is one of the best ways to improve stamina and cardiovascular efficiency. Try running a 4 mile distance in 32 minutes. Concentrate on finishing the distance first before looking at the watch. The real mental test and training opportunity will come around the 2 mile mark when your brain is trying to tell you to quit. You must fight these thoughts and concentrate on positive things like how you are going to spend Ski-Doo's contingency money!

8. It is very important that you become very familiar with all of your personal riding gear and how it works for you. All combinations of clothing must be tested well before race day and in all weather conditions so that you know how they will affect your riding style. There should be no surprises on the start line such as goggles fogging because you taped up a different way than normal. You have to develop and follow standard operating procedures that work for you; the biggest mistake made by new drivers is to overdress. At the start line you should only be able to maintain warmth by wearing an overcoat which is handed over to your mechanic as you start.
9. It also important to know your sled and it's systems very intimately. Even if you have the best mechanics for your wrench sessions, the driver is ultimately responsible for any failures. The driver must be able to conduct all trail side repairs to get across the finish line. The driver and team must train together regularly to get to know the sled intimately. Do not test any setup during competition, this is the quickest way out of the winner's circle. Test one change at the time and verify against an untouched reference sled. Keep detailed notes on all tests or you are doomed to repeat past mistakes and waste valuable time.

You must first finish before you can finish in first place.

TABLE OF CONTENTS

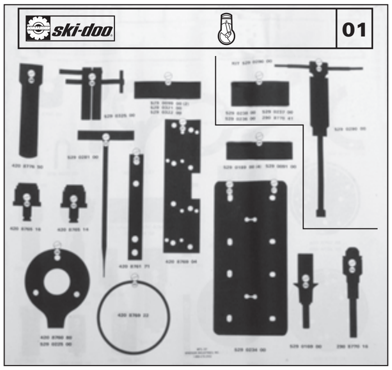
SERVICE TOOLS

This is a list of tools to properly service Ski-Doo snowmobiles. The list includes both the mandatory tools included in a kit (P/N 861 743 700) and the optional tools that are ordered separately. The list of Service Products, both mandatory and optional, are not part of any kit and must all be ordered separately. If you need to replace or add to your tool inventory these items can be ordered through the regular parts channel.

Following mention points out new tool and product: NEW

WORKSHOP — MANDATORY SERVICE TOOLS

Tool board
(P/N 529 034 000)

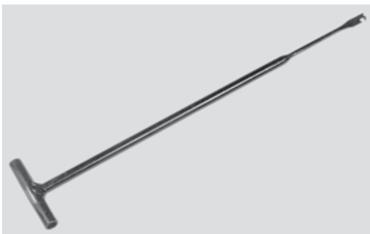


A00A3X4

APPLICATION
All models.

ENGINE — MANDATORY SERVICE TOOLS

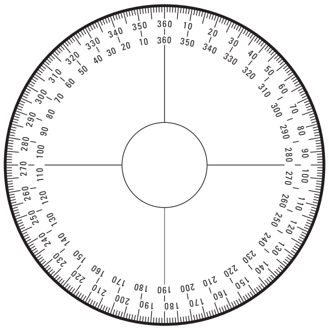
Exhaust spring installer/remover
(P/N 529 035 400)



A01B584

APPLICATION
CK3 series.

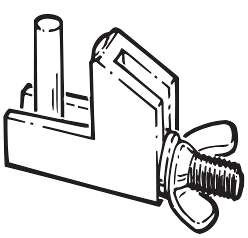
Degree wheel
(P/N 529 035 607)



A00B514

APPLICATION
All rotary valve engines.
NOTE: This tool replaces degree wheel (P/N 295 000 007).

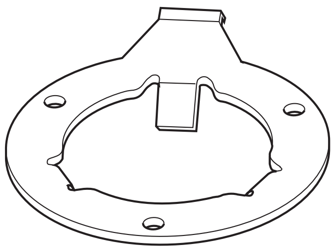
Hose pincher (2)
(P/N 295 000 076)



A01B2I4

APPLICATION
All vehicles.
NOTE: Only the P/N has been changed. This hose pincher is identical to the P/N 529 009 900.

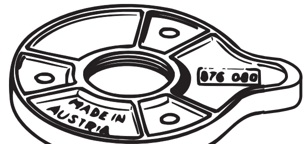
Holder wrench
(P/N 420 876 357)



A00C0Q4

APPLICATION
377, 443 and 503 engines.

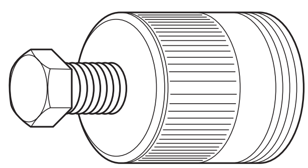
Magneto puller ring
(P/N 420 876 080)



A00C1R4

APPLICATION
All engines except 247.

Magneto puller
(P/N 529 035 547)



A00C1A4

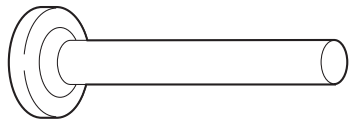
APPLICATION
All engines except 247.
NOTE: The previous extractor (P/N 529 022 500) can be upgraded by replacing the screw with the new one (P/N 529 035 549).

Aligning pin (4)
(P/N 529 018 900)

A00A1D4

APPLICATION
467, 494 and 582 engines.

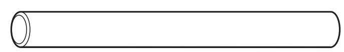
Pusher
(washer behind the impeller)
(P/N 529 020 700)



A00C3H4

APPLICATION
Rotary valve engines.

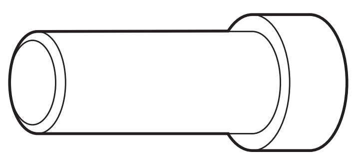
Rotary valve shaft pusher
(P/N 420 876 612)



A00C0F4

APPLICATION
Rotary valve engines with a 10 mm impeller shaft.

Rotary valve seal pusher
(valve side)
(P/N 420 876 607)



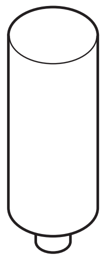
A00C0Y4

APPLICATION
Rotary valve engines.

ENGINE (continued) — MANDATORY SERVICE TOOLS

Rotary valve shaft seal pusher (inner, water pump side)

(P/N 420 876 512)



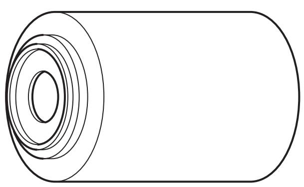
A00C374

APPLICATION

Rotary valve engines, 1991 and newer with a 10 mm impeller shaft.

Rotary valve shaft seal pusher (outer, water pump side)

(P/N 420 877 050)



A00C0X4

APPLICATION

Rotary valve engines.

Bearing pusher (rotary valve)

(P/N 420 876 500)

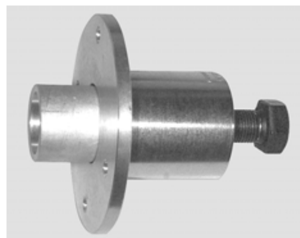
A00B2J4

APPLICATION

Rotary valve engines.

Ceramic seal pusher

(P/N 420 877 820)



A00B524

APPLICATION

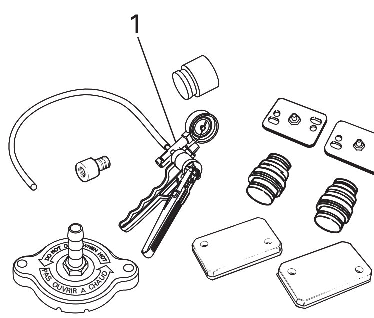
494 and 670 engines with ceramic seal on water pump side.

Engine leak tester kit

(P/N 861 749 100)

1) Hand pump

(P/N 529 021 800)



A01B5F5

APPLICATION

All engines.

Fuel and oil system leak tester kit

(P/N 529 033 100)

A01B5E4

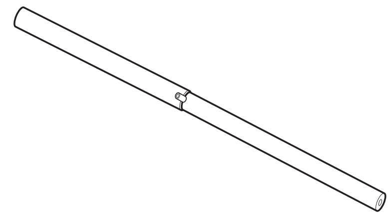
APPLICATION

All models.

Choke plunger tool

A) (P/N 529 032 100)

B) (P/N 529 035 602)



A01C5D4

APPLICATION

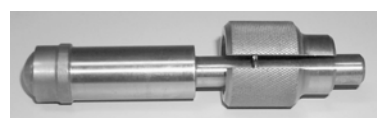
A) All models equipped with chokes except ZX series (small end for 30, 32 and 34 mm carburetor and big end for 38 mm carburetor).

B) VM type carburetor on ZX series.

NEW

Piston circlip installer

(P/N 529 035 686) 20 mm



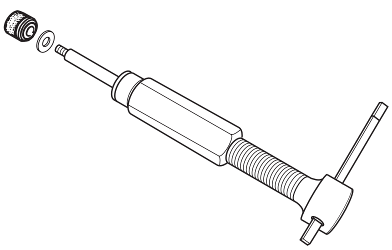
A32B0C4

APPLICATION

Engines with tab type circlip.

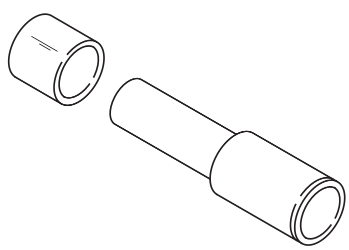
ENGINE (continued) — MANDATORY SERVICE TOOLS

1) Piston pin puller
(P/N 529 035 503)



A02B094

2) Sleeve kit 18 mm
(P/N 529 035 541)
3) Sleeve kit 20 mm
(P/N 529 035 542)



A01B5A4

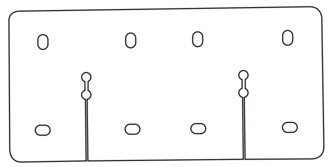
NOTE: 18 mm sleeve kit contains 1 shouldered sleeve and 3 sleeves. 20 mm sleeve kit contains 1 shouldered sleeve and 2 sleeves.

APPLICATION

1) All engines.
2) 277, 443, 503 and 809 engine.
3) 593, 670 and 693 engines.

NOTE: The previous piston pin puller (P/N 529 029 000) can be upgraded by adding protector (P/N 529 035 513) and replacing the expansion sleeve with appropriate sleeve kit.

Rubber pad
(P/N 529 023 400)

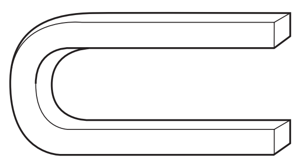


A01B4C4

APPLICATION

All cageless bearing engines.

Rotary valve circlip tool
A) (P/N 529 029 100)
B) (P/N 529 020 800)

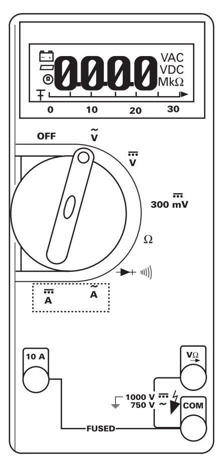


A00C3I4

APPLICATION

A) 1994 and on rotary valve engines.
B) Up to 1993 rotary valve engines.

Multimeter
(P/N 529 035 788)

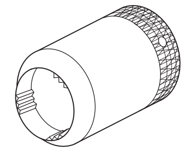


F01B1O4

APPLICATION

All models.

Choke/DESS nut tool
(P/N 529 034 600)



A01B554

APPLICATION

All models equipped with a choke and/or a DESS.

NOTE: This tool replaces choke nut tool (P/N 529 032 200).

9-volt adaptor
(P/N 529 035 675)

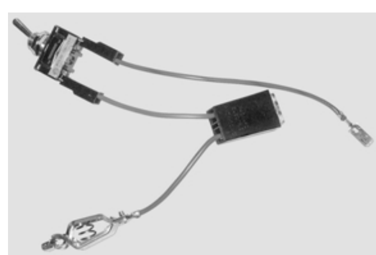
A00B5G4

APPLICATION

All models equipped with a DESS.

NEW

Bypass wire kit
(P/N 861 780 600)



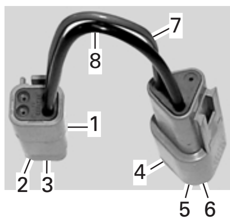
A32B0F4

APPLICATION

2002 ZX with 360 W magneto.

ENGINE (continued) — MANDATORY SERVICE TOOLS

Homemade adaptor



A00B5J4

Required parts:

1) Female housing (P/N 515 175 245)
2) Female terminal (2) (P/N 409 015 100)
3) Female lock (P/N 515 175 246)
4) Male housing (P/N 409 207 000)
5) Male terminal (2) (P/N 278 000 631)
6) Male lock (P/N 409 207 600)
7) RED wire in position 1 (4-wire connector) and B (3-wire connector)
8) BLACK wire in position 2 (4-wire connector) and C (3-wire connector)

APPLICATION

2001and 2002 Mach Z TECH PLUS.

1-2) Programmer kit (P/N 529 035 718)

2) Communication cables (P/N 529 001 052)

A01B5B5

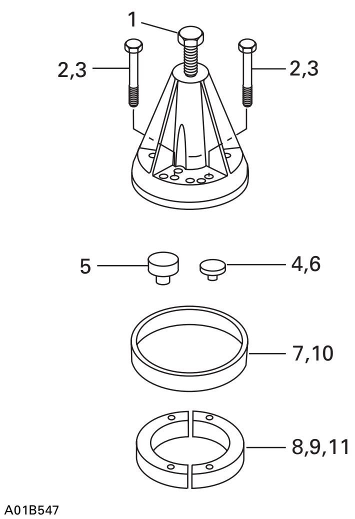
APPLICATION

All models equipped with a DESS.

ENGINE (continued) — RECOMMENDED SERVICE TOOLS

The following tools are highly recommended to optimize your basic tool kit and reduce repair time.

1-2) Crankshaft bearing puller with screw
(P/N 420 877 635)



APPLICATION
All engines.

1)	Screw M16 x 1.5 x 150	(P/N 420 940 755)
2)	Screw M8 x 40 (4)	(P/N 420 840 681)
3)	Screw M8 x 70 (4)	(P/N 420 841 201)
4)	Crankshaft protector 247 engine.	(P/N 420 976 890)
5)	Crankshaft protector PTO All engines except 247.	(P/N 420 876 552)
6)	Crankshaft protector MAG All engines except 247.	(P/N 420 876 557)
7)	Puller ring Use with half rings (P/N 420 977 475 or 420 276 025).	(P/N 420 977 490)
8)	Half ring (2) For 72 mm O.D. bearings.	(P/N 420 977 475)
9)	Half ring (2) For 62 mm O.D. bearings.	(P/N 420 276 025)
10)	Puller ring For half rings (P/N 420 977 479).	(P/N 420 977 494)
11)	Half ring (2) For 80 mm O.D. bearings.	(P/N 420 977 479)

ENGINE (continued) — RECOMMENDED SERVICE TOOLS

Piston circlip installer

A) (P/N 529 035 561) 18 mm

B) (P/N 529 035 562) 20 mm

A00B4Y4

APPLICATION

A) All engines except 593, 670, 693 and 793.

NOTE: This tool replaces circlip installer (P/N 529 016 900).

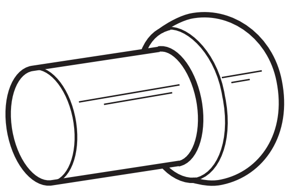
B) 2001 and older 593, 670 and 693 engines.

NOTE: This tool replaces circlip installer (P/N 290 877 016).

Piston pin/connecting rod bearing centering tool

(P/N 529 009 100)

NOTE: New diameter is 9.65 mm (0.380 in).



A01B1R4

APPLICATION

All engines except cageless and 670 engines.

Ring compressor

A) (P/N 420 876 090) (62 mm)

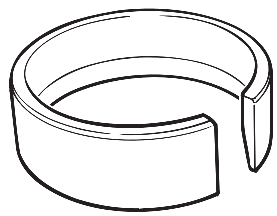
B) (P/N 420 876 974) (69.5 mm)

C) (P/N 420 876 970) (72 mm)

D) (P/N 420 876 972) (76 mm)

E) (P/N 420 876 975) (67.5 mm)

F) (P/N 529 030 800) (78 mm)



A01B1T4

APPLICATION

A) 377 engine.

B) 467 and 494 engines.

C) 503, 253 and 536 engines.

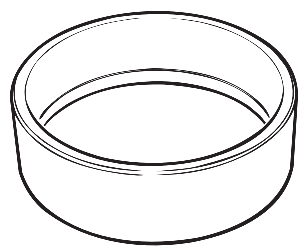
D) 582, 583 and 643 engines.

E) 443 and 447 engines.

F) 670 engine.

Magneto coil centering ring

(P/N 420 876 922)



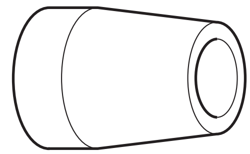
A01B1V4

APPLICATION

All engines with Nippondenso CDI (160 W).

Seal protector sleeve

(P/N 420 276 900) (MAG)



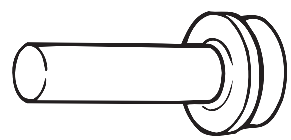
A00C0D4

APPLICATION

247 engine.

Polyamid ring pusher

(P/N 420 276 930)



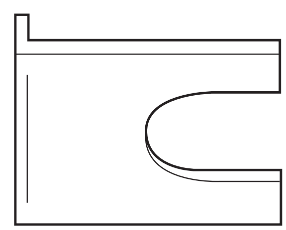
A00C0Z4

APPLICATION

247 engine.

Crankshaft feeler gauge

(P/N 420 876 620)



A00C114

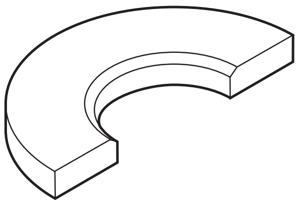
APPLICATION

377, 443, 447 and 503 engines.

ENGINE (continued) — RECOMMENDED SERVICE TOOLS

Crankshaft distance gauge (5.7 mm)

(P/N 420 876 822)



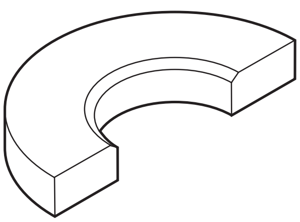
A00C294

APPLICATION

377, 443 and 447 engines.

Crankshaft distance gauge (12.7 mm)

(P/N 420 876 824)



A00C3A4

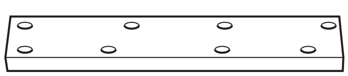
APPLICATION

503 engine.

Cylinder aligning tool

A) (P/N 420 876 904) (on exhaust side)

B) (P/N 420 876 171) (on intake side)



A00B084

APPLICATION

A) 2-cylinder liquid cooled engines.

B) 2-cylinder fan cooled engines.

Driver tool

(P/N 529 035 521)

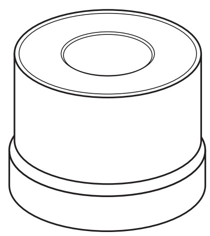
A00B4O4

APPLICATION

Mini Z.

Attachment

(P/N 529 035 522)



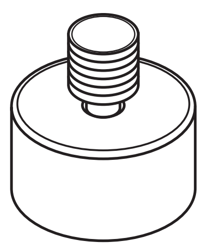
A00B4P4

APPLICATION

Mini Z.

Pilot 22 mm

(P/N 529 035 523)



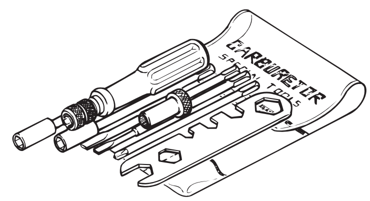
A00B4Q4

APPLICATION

Mini Z.

Carburetor tool kit

(P/N 404 112 000)



A00B2F4

APPLICATION

All models.

Adaptor

(P/N 529 033 800)

(TYPICAL)

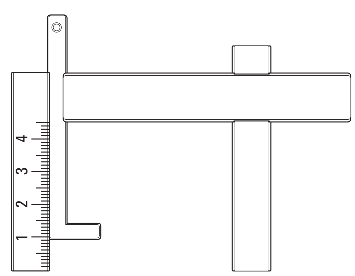
A00B4H4

APPLICATION

1997 and 1998 Grand Touring SE 1998 Summit x 670.

Float level gauge

(P/N 529 035 520)



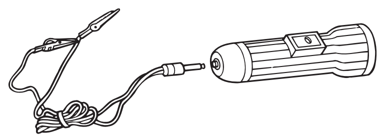
A00B4N4

APPLICATION

All models.

ENGINE (continued) — RECOMMENDED SERVICE TOOLS

Circuit tester
(continuity light)
(P/N 414 012 200)



A00C214

APPLICATION
All vehicles.

Stroboscopic timing light
(P/N 529 031 900)

A00B4F4

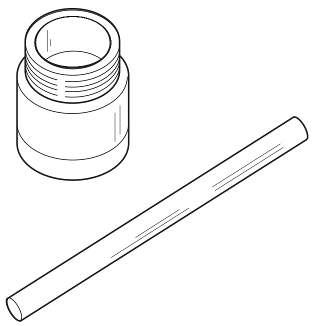
APPLICATION
All engines.

Bypass wires
(P/N 529 033 300)

A00I094

APPLICATION
F and CK3 Grand Touring 700/SE with 360 W magneto.

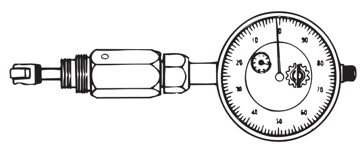
RAVE movement indicator
(P/N 861 725 800)



A18B014

APPLICATION
All RAVE equipped engines.

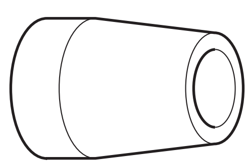
Dial indicator
(TDC gauge)
(P/N 414 104 700)



A00B4E4

APPLICATION
All engines.

Seal protector sleeve
A) (P/N 420 876 980)
B) (P/N 420 876 490)



A00C0D4

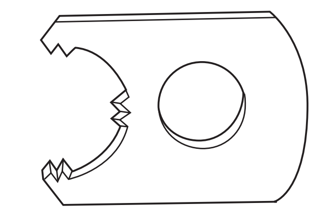
APPLICATION
A) Rotary valve engines with 10 mm shaft.
B) Rotary valve engines with 12 mm shaft.

Magneto puller
(P/N 420 976 235)

F01B294

APPLICATION
247 engine.

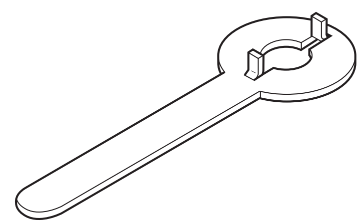
Injection pump gear holder
(P/N 420 876 695)



A00B314

APPLICATION
253, 377, 447 and 503 engines.

Injection pump gear holder
(P/N 420 277 905)

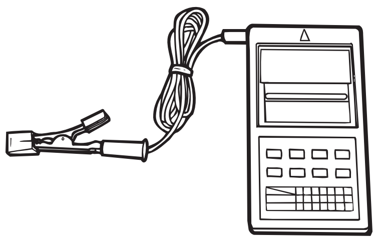


A00C164

APPLICATION
All liquid cooled engines.

ENGINE (continued) — RECOMMENDED SERVICE TOOLS

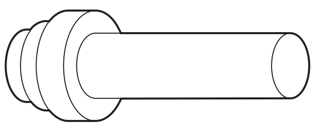
Digital/induction type tachometer
(P/N 529 014 500)



F01B1G4

APPLICATION
All engines.

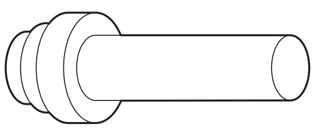
MAG seal pusher
(P/N 420 277 875)



A00C0V4

APPLICATION
277 engine.

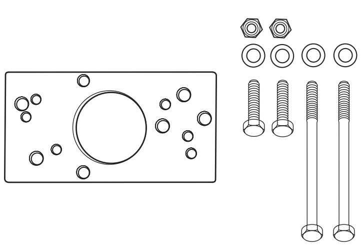
PTO seal pusher
(P/N 420 876 660)



A00C0V4

APPLICATION
277 engine.

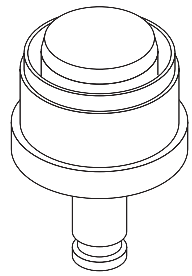
Base puller plate kit
(P/N 529 024 900)



A05C0M4

APPLICATION
277 engine.

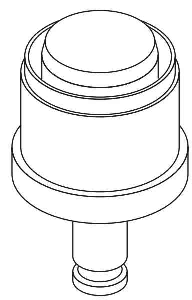
Insertion jig
(magneto side seal)
(P/N 420 876 516)



A00C3T4

APPLICATION
779 engine.

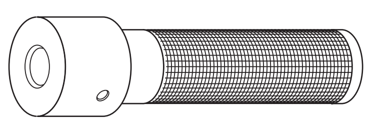
Insertion jig
(magneto seal)
(P/N 420 876 514)



A00C3U4

APPLICATION
454, 494, 599, 670, 699 and 809 engines.

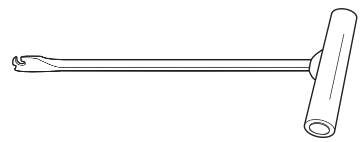
Handle for insertion jig
(P/N 420 877 650)



A00C3V4

APPLICATION
454, 494, 599, 670, 699, 779 and 809 engines.

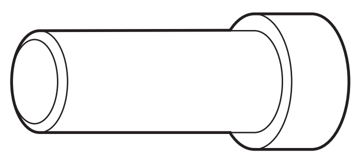
Exhaust spring installer/remover
(P/N 529 035 559)



A00C3S4

APPLICATION
All models except CK3 series.
NOTE: This tool replaces exhaust spring installer/remover (P/N 529 028 100).

Rotary valve seal and
shaft pusher
(P/N 420 876 605)

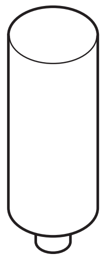


A00C0Y4

APPLICATION
Rotary valve engines 1990 models and older.

ENGINE (continued) — RECOMMENDED SERVICE TOOLS

Seal pusher (rotary valve)
(P/N 420 876 510)

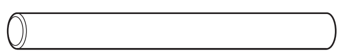


A00C374

APPLICATION

All rotary valve shaft seals with a 12 mm I.D.

Rotary valve shaft pusher
(P/N 420 876 610)



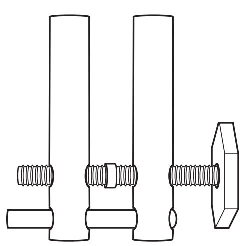
A00C0F4

APPLICATION

All rotary valve engines with 12 mm shaft.

Large hose pincher
(P/N 529 032 500)

(TYPICAL)



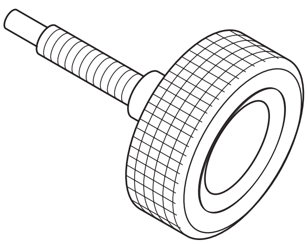
F01B234

APPLICATION

All vehicles.

TRANSMISSION — MANDATORY SERVICE TOOLS

Driven pulley opening tool
(P/N 529 017 200)



A00A1A4

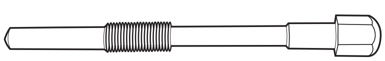
APPLICATION
All non-RER models.

Clutch holder
(P/N 529 006 400)

A01B154

APPLICATION
All TRA drive pulleys.

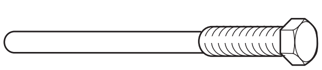
TRA drive pulley puller
(P/N 529 022 400)



A06B014

APPLICATION
TRA drive pulley for the 454, 494, 599, 670, 699, 779 and 809 engines.

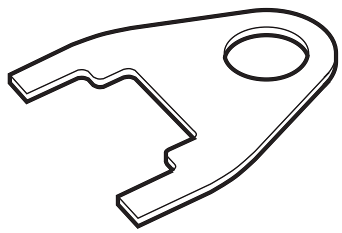
TRA drive pulley puller
(P/N 529 007 900) (25 mm)



A18B044

APPLICATION
TRA drive pulley for 443, 467, 503, 536 and 537 engines.

Forks (3)
(P/N 529 005 500)



A16B014

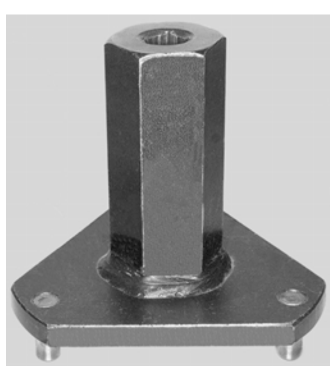
APPLICATION
All vehicles equipped with a TRA drive pulley.

Tapered tool
(P/N 529 025 300)

A32B0M4

APPLICATION
Skandic LT 2001-2002.

Spider tool
(P/N 529 025 200)



A32B0N4

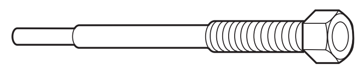
APPLICATION
Skandic LT 2001-2002.

Drive pulley puller
(P/N 529 025 000)

A29B034

APPLICATION
Skandic LT 2001-2002.

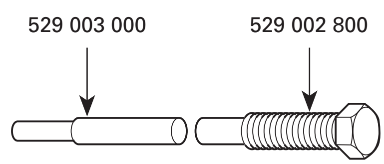
Drive pulley puller
(P/N 529 002 100)
(standard threads)



A00C084

APPLICATION
Square shaft, standard (SAE) threads.

Drive pulley puller
(P/N 860 414 200)
(square shaft metric)
Consists of:



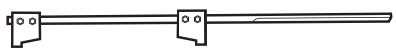
A00C095

APPLICATION
Square shaft, metric threads drive pulley.

TRANSMISSION (continued) — MANDATORY SERVICE TOOLS

Transmission alignment bar

A) (P/N 529 026 900)
B) (P/N 529 030 000)
C) (P/N 529 035 586)
D) (P/N 529 026 700)
E) (P/N 529 035 530)
F) (P/N 529 031 000)
G) (P/N 529 035 527)
H) (P/N 529 035 572)
I) (P/N 529 035 594)



A01B4D4

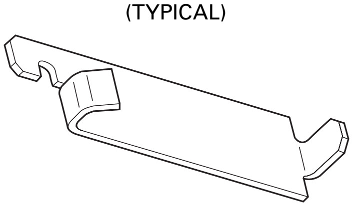
APPLICATION

A) Tundra II LT/R.
B) S-Series with Bombardier Lite.
C) S-Series with Bombardier Lite and RER.
D) F-Series, S-Series and ZX series with TRA.
E) S-Series with TRA and RER.
F) Skandic WT LC/SWT.
G) CK3 series except 1998 Mach Z series.
H) 1998 Mach Z series.
I) CK3 series with RER.

Spring scale hook (long)

A) (P/N 529 006 500)
B) (P/N 529 030 900)
C) (P/N 529 035 557)

(TYPICAL)

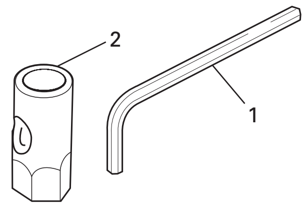


A00B4A4

APPLICATION

A) Tundra II LT.
B) F-Series and S-Series (1995 and newer).
C) CK3 without RER.

Drive belt tension adjuster tool
(P/N 529 008 700)



A15B044

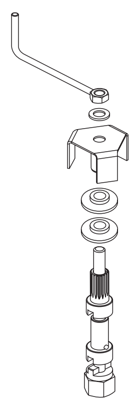
Parts included:

1) Hexagonal wrench (P/N 420 876 730).
2) Socket wrench (P/N 529 015 000).

APPLICATION

All vehicles except Élan, Tundra II and Skandic WT.

Pulley spring compressor
(P/N 529 035 524)



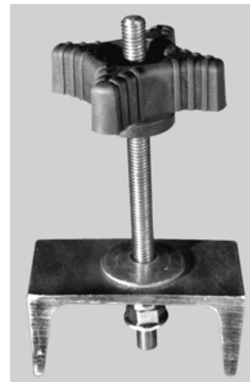
A02D1P4

APPLICATION

All models.

NOTE: This tool has Acme threads and replaces spring compressor (P/N 529 018 600).

Driven pulley spring compressor
(P/N 529 035 300)

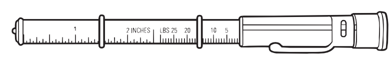


A05B034

APPLICATION

Tundra R.

Tension tester
(P/N 414 348 200)

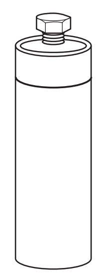


A00C074

APPLICATION

All models.

Countershaft bearing installer
(P/N 529 030 200)



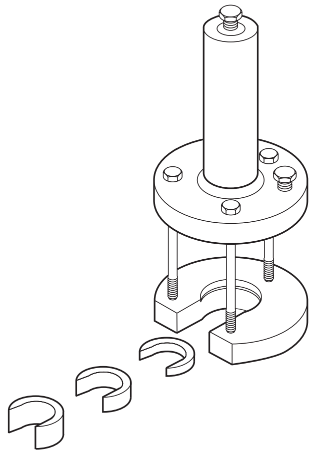
A00A194

APPLICATION

S-Series and F-Series.

TRANSMISSION (continued) — MANDATORY SERVICE TOOLS

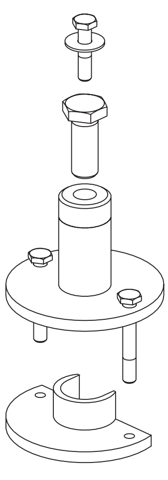
Countershaft bearing remover
(P/N 529 030 100)



A00A274

APPLICATION
S-Series and F-Series.

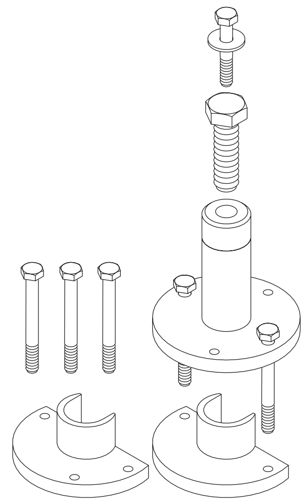
Countershaft bearing remover/installer
(P/N 529 035 554)



A01B5C4

APPLICATION
CK3 series.

Countershaft bearing remover/installer
(P/N 529 035 699)

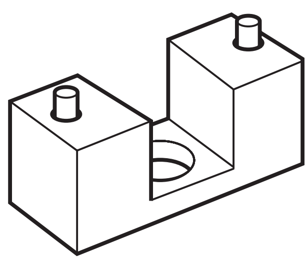


A00B5K4

APPLICATION
ZX and CK3 Series.

NOTE: This tool replaces CK3 series countershaft bearing remover/installer (P/N 529 035 554).

Spring cover tool
(P/N 529 027 300)



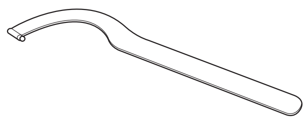
A01B4M4

APPLICATION
Bombardier Lite drive pulley.

TRANSMISSION (continued) — RECOMMENDED SERVICE TOOLS

The following tools are highly recommended to optimize your basic tool kit and reduce repair time.

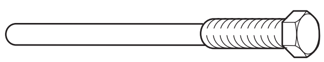
Clutch holder
(P/N 529 027 600)



A02B034

APPLICATION
Bombardier Lite drive pulley.

Drive pulley puller
(P/N 529 031 400)



A18B044

APPLICATION
Bombardier Lite drive pulley, except Élan.

Driven pulley opening tool
(P/N 529 035 501)

A03D2P4

APPLICATION
S and CK3 series with RER.

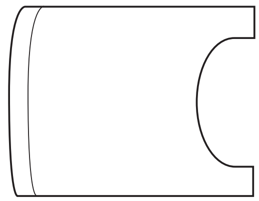
NOTE: This tool replaces driven pulley opening tool (P/N 529 019 500).

Driven pulley opening tool
(P/N 529 034 200)

A05B044

APPLICATION
Tundra R.

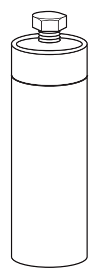
Alignment tool
(P/N 420 476 010)



A00C1D4

APPLICATION
Skandic WT and Alpine II gearbox.

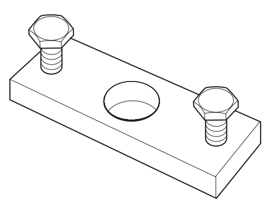
Countershaft bearing installer
(P/N 529 018 800)



A00A194

APPLICATION
PRS chassis.

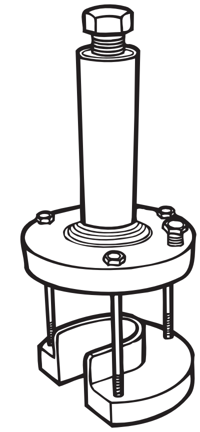
Cam pusher
(P/N 529 012 900)



A18B064

APPLICATION
Tundra II LT.

Countershaft bearing remover
(P/N 529 018 700)

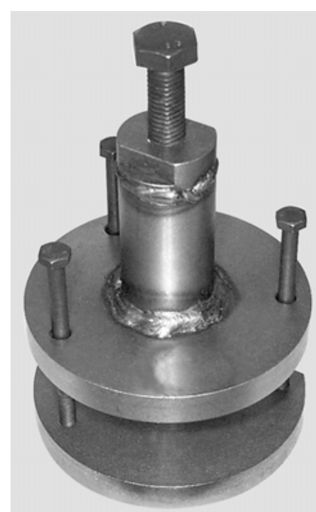


A00A164

APPLICATION
PRS chassis.

NEW

Countershaft bearing remover
(P/N 529 035 812)



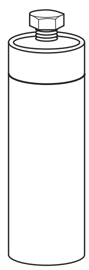
A29B024

APPLICATION
Skandic LT.

TRANSMISSION (continued) — RECOMMENDED SERVICE TOOLS

NEW

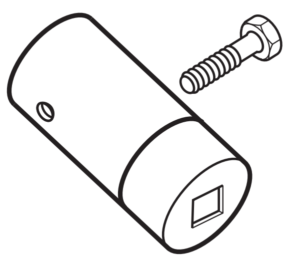
Countershaft bearing installer
(P/N 529 035 815)



A00A194

APPLICATION
Skandic LT.

Drive pulley puller
(P/N 529 023 100)



A00C3J4

APPLICATION
Élan.

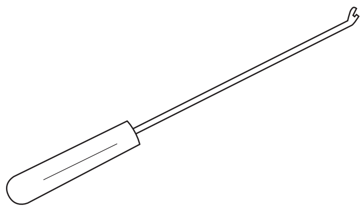
Transmission ball mounting pin
(P/N 420 476 020)

A00C1C4

APPLICATION
Alpine II 3-speed gearbox.

TRANSMISSION (continued) — RECOMMENDED SERVICE TOOLS

Transmission adjuster
(P/N 529 028 500)

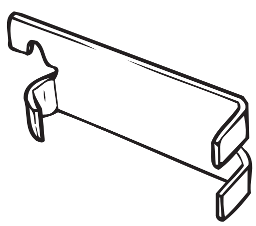


A00D0X4

APPLICATION

F-Series equipped with "twist shifter" reverse transmission.

Spring scale hook (long)
(P/N 529 015 200)

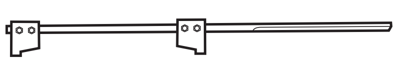


A01B514

APPLICATION

1994 models and older except Alpine II.

Alignment bar
A) (P/N 529 025 600)
B) (P/N 529 028 200)
C) (P/N 529 028 300)
D) (P/N 529 026 800)
E) (P/N 529 031 000)
F) (P/N 529 035 808)

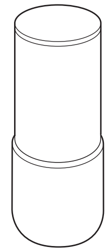


A01B4D4

APPLICATION

A) PRS chassis.
B) Alpine II.
C) Élan.
D) Safari L.
E) Skandic WT 1996.
F) Skandic LT.

Burnishing bar
(P/N 529 026 402)

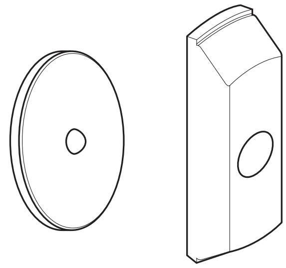


A00B464

APPLICATION

Tundra II LT, Safari L and Skandic.

Large bushing extractor
(P/N 529 031 100)



A00B4I4

APPLICATION

Formula type driven pulley.

NOTE: Use this tool only with former puller (P/N 529 018 600) that has regular threads.

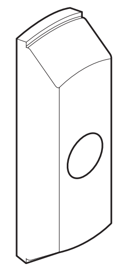
Bushing extractor/installer
(P/N 529 031 300)

A01B5G4

APPLICATION

TRA drive pulley spring cover with repleacable bushing

Large bushing extractor
(P/N 529 035 576)



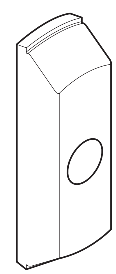
A02D1Q4

APPLICATION

Formula type driven pulley.

NOTE: Use this tool only with new puller (P/N 529 035 524) that has Acme threads and support plate included with extractor (P/N 529 031 100).

Large bushing extractor
(P/N 529 035 575)



A02D1Q4

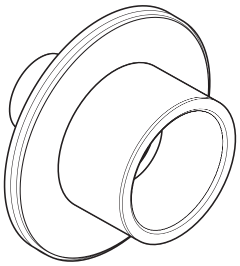
APPLICATION

LPV 27 driven pulley.

NOTE: Use this tool only with new puller (P/N 529 035 524) that has Acme threads and support plate included with extractor (P/N 529 031 100).

TRANSMISSION (continued) — RECOMMENDED SERVICE TOOLS

Large bushing installer and small bushing extractor
(P/N 529 031 200)

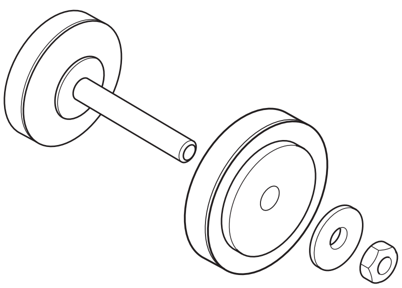


A00B4J4

APPLICATION

All models except Tundra/R, Skandic WT/SWT/WT LC and S-Series with RER.

Chaincase seal pusher
(P/N 529 035 584)



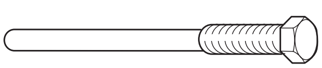
A00B504

APPLICATION

S, F, CK3 and ZX series.

NOTE: This tool replaces chaincase upper seal pusher (P/N 529 032 300).

TRA drive pulley puller (27 mm)
(P/N 529 010 100)

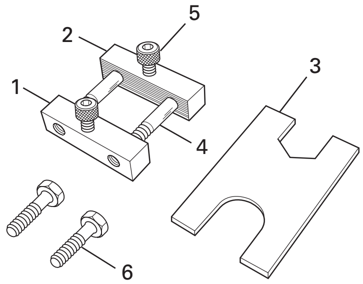


A18B044

APPLICATION

TRA drive pulley (27 mm) shaft except 454, 670 and 779 engines.

Drive axle sprocket adjuster
(P/N 861 725 700)



A01B2O4

Parts included in the kit:

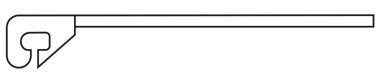
1) Block with threads
   (P/N 529 010 700)
2) Block without threads
   (P/N 529 010 800)
3) Plate
   (P/N 529 010 600)
4) Bolt M10 (2)
   (P/N 222 007 565)
5) Allen screw M8 (2)
   (P/N 222 983 065)
6) Screw M8 (2)
   (P/N 222 082 565)

NOTE: When the tool is to be used between tunnel and sprocket use screws M8.

APPLICATION

All vehicles except Élan.

Transmission adjuster
(P/N 529 030 300)

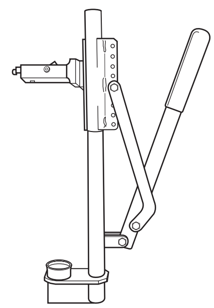


A03D1T4

APPLICATION

Vehicles equipped with “push-pull shifter” reverse transmission.

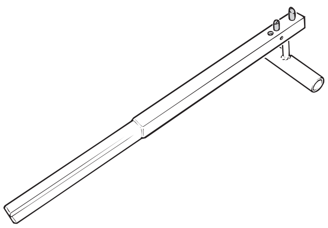
SUSPENSION — MANDATORY SERVICE TOOLS

Shock spring removal kit (P/N 529 035 504) Replacement clevis pin: (P/N 414 528 400)  A01B4O4
APPLICATION All suspensions with coil spring. NOTE: The previous shock spring removal kit (P/N 529 027 100) can be upgraded by replacing the stopper with a wider stopper (P/N 529 035 551).

SUSPENSION (continued) — RECOMMENDED SERVICE TOOLS

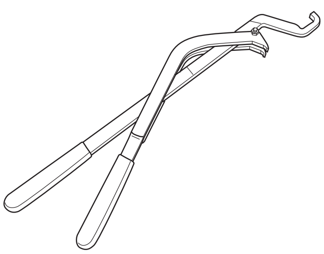
A) Track cleat remover
(P/N 529 008 200)
Pins
(P/N 529 008 204)

NOTE: Pins can be rotated 180° depending on whether the tool is used by a left-hander or right-hander.



A01B1J4

B) Track cleat remover
(P/N 529 028 700)



A01F224

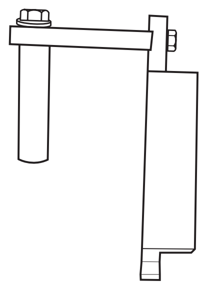
APPLICATION

A) 1993 and older.
B) 1994 and newer except Élan and Tundra II.

Camber angle tool
(P/N 529 021 600)

NOTE: Angle finder with a magnetic base must be used.

Suggestion: K-D tool no. 2968

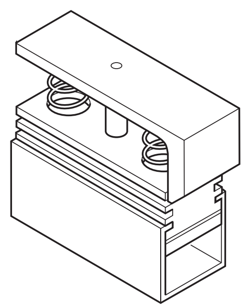


A06B024

APPLICATION

All DSA front suspensions.

Track tension gauge
(P/N 529 021 500)

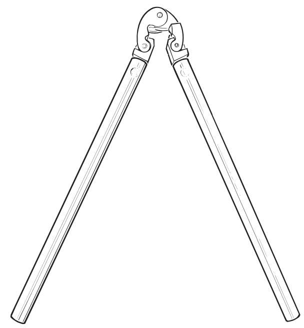


A00B3X4

APPLICATION

All models except Élan.

Track cleat installer
A) (P/N 529 008 500)
Narrow
B) (P/N 529 028 800)
Narrow
C) (P/N 529 007 700)
Wide

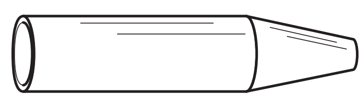


A01B1M4

APPLICATION

A) 1993 and older.
B) 1994 and newer.
C) 1992 and older with wide cleat opening.

Dome guide
A) (P/N 529 026 500)
B) (P/N 529 035 728)



A06F1B4

APPLICATION

A) C-36 T/A shocks.
B) C-46 T/A shocks.

SUSPENSION (continued) — RECOMMENDED SERVICE TOOLS

Shock wrench
(P/N 529 035 727)

A00F224

All T/A shocks

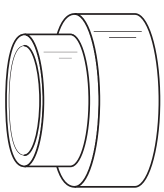
NEW

HPG shock holding tool
(P/N 529 035 769)

A01B5H4

All HPG shocks

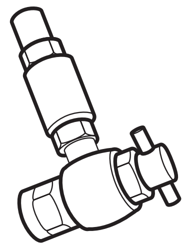
Piston guide
A) (P/N 529 026 600)
B) (P/N 529 035 608)



A06F1C4

APPLICATION
A) C-36 T/A shocks.
B) C-46 T/A shocks.

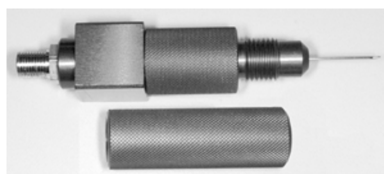
Gas shock valve tool
(tire valve type)
(P/N 529 035 570)



A02F134

APPLICATION
1999 and older T/A shocks and some 2000 and up T/A shocks.

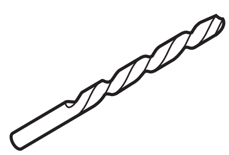
Tool for shock (needle type)
(P/N 529 035 614)



A00B5I4

APPLICATION
Most 2000 and up T/A shocks.

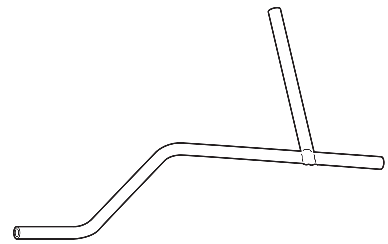
Drill bit
(P/N 529 031 800)



A01B564

APPLICATION
All 3/16 inch rivets.

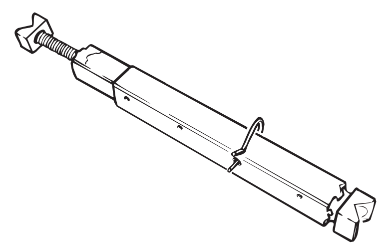
Spring installer (bar)
(P/N 529 005 000)



A00C1I4

APPLICATION
Tundra II LT, Scout and all SC-10 suspensions.

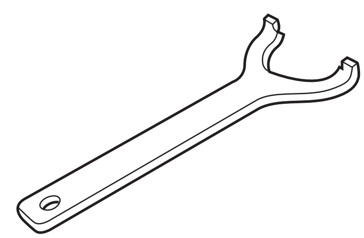
Drive axle holder
(P/N 529 007 200)



A01B1E4

APPLICATION
All models.

Kayaba shock adjustment tool
(P/N 529 035 582)

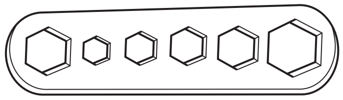


A00A1K4

APPLICATION
C-7 suspension.

SUSPENSION (continued) — RECOMMENDED SERVICE TOOLS

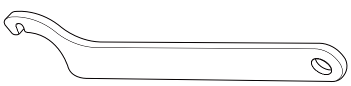
Hexagonal wrench
(P/N 529 014 700)



A19B024

APPLICATION
All SC-10 suspensions, Safari and Skandic prior to 1995.

Suspension adjustment wrench
(P/N 529 017 100)



A15B094

APPLICATION
1992 and old Formula C-7.

Suspension adjustment wrench
(P/N 529 032 900)

A02F114

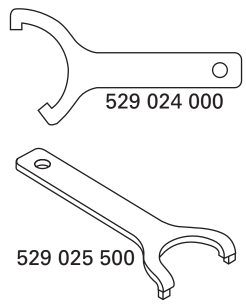
APPLICATION
ARM and SC 10 II suspensions.

Suspension adjustment wrench
(P/N 529 034 100)

A02F124

APPLICATION
CK3 series.

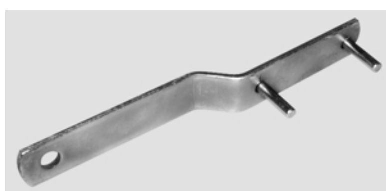
Adjustment wrench
(P/N 861 743 900)
Consists of:



A00B4B4

APPLICATION
1998 and older models with T/A shock.

Adjustment wrench
(P/N 520 000 126)



A00B5H4

APPLICATION
SC-10 II (coupling blocks).

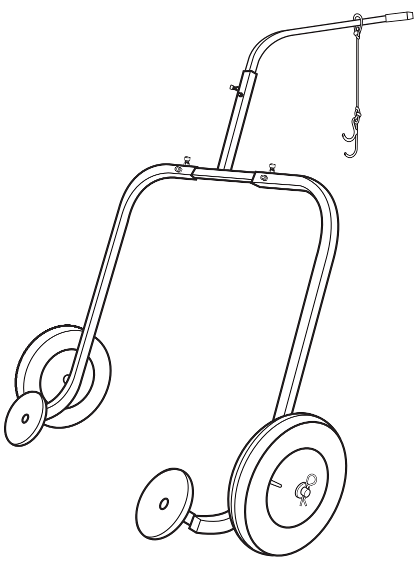
VEHICLES — RECOMMENDED SERVICE TOOLS

Protective mat
(P/N 529 030 600)

A01B45W

APPLICATION
All vehicles.

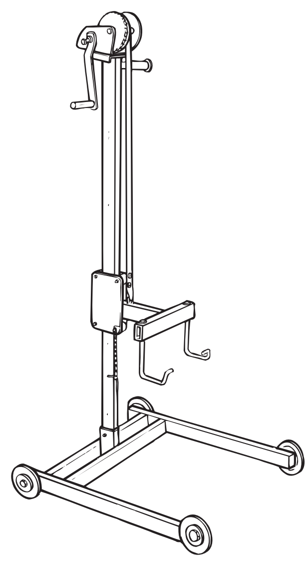
Dolly
(P/N 529 029 900)



A00B4CJ

APPLICATION
All models.

Snowmobile jack
(P/N 529 020 000)



A01A1JJ

APPLICATION
All models.

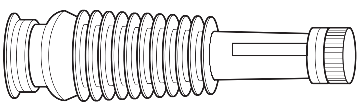
VEHICLES (continued) — RECOMMENDED SERVICE TOOLS

Template for hood drilling
(P/N 529 034 400)

A02H154

APPLICATION
S-Series.
NOTE: To drill new hood prior to install meters.

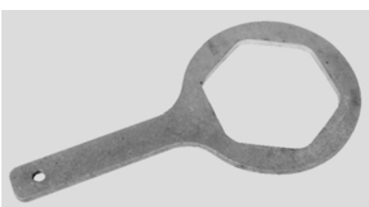
Flexible spout for oil container
(P/N 414 837 300)



F04B044

APPLICATION
All models.

Adjustment wrench
(P/N 529 035 603)

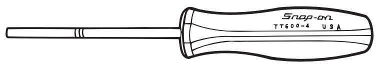


A32B044

APPLICATION
To remove and install fuel tank nut on ZX series.

Terminal (Packard) remover
Not sold by Bombardier

Snap-on
TT 600-4



F01B1J4

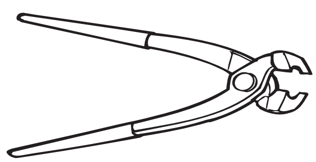
APPLICATION
Models with Packard connectors.

Crimping tool
(P/N 295 100 164)

F00B0E4

APPLICATION
Models with AMP connectors.

Hose clamp pliers
(P/N 295 000 070)



F01D174

APPLICATION
Some models.

NOTE